DOC NO.

TWR-17546 Vol. III L623-FY91-M020

REV A '

-----

Flight Set 360L007 (STS-33)
Insulation Component Final Report
Volume III
Final Release

August 1990

Prepared by:

S. Hicken

Thermal Insulation Design

Approved by:

F. Baugh, Supervisor

Thermal Insulation Design

S. Marsh

Insulation Program Manager

Larry Wille

L. Allred

Integration Engineer

Polores Mills 9-26-90

Kelease ECS SS-1015

Thickol CORPORATION

SPACE OPERATIONS

P.O. Box 707, Brigham City, UT 84302-0707 (801) 863-3511

(NASA-CR-104001) FLIGHT SLT 360L007 (STS-33) INSULATION COMPONENT. VOLUME 3: FINAL RELEASE Final Report (Thickol Corp.) 204 p. CSCL 218

N91-21230

Unclas

G3/20 0330392

# · ACTIVE PAGE RECORD

PAGE NO.	REVISION						
A	All		·				
						·	
		·					
							•

A	TWR-17546	DOC III NO.		VOL
	······································	SEC	PAGE	i

# REVISION DESCRIPTION

REV LTR	DATE	DESCRIPTION
A	Aug 1990	This revision adds the thermal safety factor analysis, factory joint inspections, and edge separation evaluation to the interim report.
	·	

EVISION A_	DOC NO.	TWR-1754	5	<b>45</b> 4	
	SEC		PAGE		_



### **ABSTRACT**

Volume III of this postfire report deals with the insulation component of the RSRM. The report is released twice for each flight set. The interim release contract date is on or before 60 days after the last field joint or nozzle to case joint is disassembled at KSC and contains the results of the KSC visual evaluation. The data contained in the Volume III interim release supersedes the insulation data presented in the KSC 10 day report. The final release contract date is on or before 60 days after the last factory joint is disassembled at the Clearfield H-7 facility and contains the results of all visual evaluations and a thermal safety factor analysis. The data contained in the Volume III final release supersedes the interim release and the insulation data presented in the Clearfield 10 day report.



# CONTENTS

Section			Page
1.0	INTROD	DUCTION	1
2.0	OBJECT	TIVES	1
3.0	SUMMAR	Ϋ́	2
	3	EXTERNAL INSULATION 3.1.1 Factory Joint Weatherseals 3.1.2 Stiffener Stubs and Rings	2 2 3
	3.2 N	OZZLE TO CASE JOINTS	3
•	3.3 F	PIELD JOINTS	3
	3.4 I	GNITER JOINTS AND INSULATION	4
	3	NTERNAL ACREAGE INSULATION 1.5.1 Aft Segments 1.5.2 Center Segments 1.5.3 Forward Segments	4 5 5 6
	3.6 I	NSULATION THERMAL PERFORMANCE	6
4.0	CONCLU	ISIONS	6
	4.1 K	SC EVALUATION CLASSIFICATIONS	7
	4.2 H	I-7 EVALUATION CLASSIFICATIONS	8
5.0	RECOMM	ENDATIONS	8
	5.1 K	SC EVALUATION RECOMMENDATIONS	8
	5.2 H	I-7 EVALUATION RECOMMENDATIONS	8
6.0	RSRM-7	'A VISUAL EVALUATIONS	8
	6	RSRM-7A EXTERNAL INSULATION 5.1.1 RSRM-7A Factory Joint Weatherseals 5.1.2 RSRM-7A Stiffener Stub and Rings	9 9 10
	6.2 R	RSRM-7A NOZZLE TO CASE JOINT	10
	6	RSRM-7A FIELD JOINTS 5.3.1 RSRM-7A Aft Field Joint 5.3.2 RSRM-7A Center Field Joint 5.3.3 RSRM-7A Forward Field Joint	11 11 12 13

DOC NO. TWR-17546 VOL III
SEC PAGE



# CONTENTS (Cont)

Section			Page
	6.4	RSRM-7A IGNITER JOINTS AND INSULATION	14
	6.5	RSRM-7A ACREAGE INSULATION 6.5.1 RSRM-7A Aft Segment Acreage Insulation	14 14
		6.5.2 RSRM-7A Aft Center Segment Acreage Insulation 6.5.3 RSRM-7A Forward Center Segment Acreage	15
		Insulation 6.5.4 RSRM-7A Forward Segment Acreage	16
		Insulation	17
	6.6	POSTFIRE EVALUATION OF RSRM-7A PREFIRE DISCREPANCIES	18
7.0	RSRM	-7A INSULATION PERFORMANCE EVALUATION	19
	7.1	RSRM-7A NOZZLE TO CASE JOINT	22
	7.2	RSRM-7A FIELD JOINTS	22
	,	7.2.1 RSRM-7A Aft Field Joint	23
		7.2.2 RSRM-7A Center Field Joint	24
		7.2.3 RSRM-7A Forward Field Joint	24
	7.3	RSRM-7A AFT SEGMENT	24
		7.3.1 RSRM-7A Aft Dome	24
		7.3.2 RSRM-7A Aft Cylinder	25
	7.4	RSRM-7A AFT CENTER SEGMENT	26
	7.5	RSRM-7A FORWARD CENTER SEGMENT	26
	7.6	RSRM-7A FORWARD SEGMENT 7.6.1 RSRM-7A Forward Segment Star Tip	27
		Planes	27
		7.6.2 RSRM-7A Forward Segment Non-Star Tip	21
		Planes	28
8.0	RSRM	-7B VISUAL EVALUATIONS	29
	8.1	RSRM-7B EXTERNAL INSULATION	29
		8.1.1 RSRM-7B Factory Joint Weatherseals	29
		8.1.2 RSRM-7B Stiffener Stub and Rings	30
	8.2	RSRM-7B NOZZLE TO CASE JOINT	31
	8.3		32
		8.3.1 RSRM-7B Aft Field Joint	32
		8.3.2 RSRM-7B Center Field Joint	33
		8.3.3 RSRM-7B Forward Field Joint	34
<u>A</u>		DOC NO. TWR-17546	vor III
		SEC PAGE	

REVISION FORM TC 7994-310 (REV 2-88)



# CONTENTS (Cont)

Section		<u> 1</u>	Page
	8.4	RSRM-7B IGNITER JOINTS AND INSULATION	34
	8.5	RSRM-7B ACREAGE INSULATION 8.5.1 RSRM-7B Aft Segment Acreage Insulation 8.5.2 RSRM-7B Aft Center Segment Acreage	35 35
		Insulation	36
		8.5.3 RSRM-7B Forward Center Segment Acreage Insulation	37
		8.5.4 RSRM-7B Forward Segment Acreage Insulation	38
	8.6	POSTFIRE EVALUATION OF RSRM-7B PREFIRE DISCREPANCIES	39
9.0	RSRM-	-7B INSULATION PERFORMANCE EVALUATION	4Ó
	9.1	RSRM-7B NOZZLE TO CASE JOINT	40
	9.2		40
		9.2.1 RSRM-7B Aft Field Joint	40
		9.2.2 RSRM-7B Center Field Joint	41
		9.2.3 RSRM-7B Forward Field Joint	41
	9.3	RSRM-7B AFT SEGMENT	41
		9.3.1 RSRM-7B Aft Dome	41
		9.3.2 RSRM-7B Aft Cylinder	42
	9.4	RSRM-7B AFT CENTER SEGMENT	42
	9.5	RSRM-7B FORWARD CENTER SEGMENT	43
	9.6	RSRM-7B FORWARD SEGMENT	43
		9.6.1 RSRM-7B Forward Segment Star Tip Planes	43
		9.6.2 RSRM-7B Forward Segment Non-Star Tip Planes	44
REFERE	ENCES		46
DISTRI	BUTIO	ON 1	188



# **FIGURES**

Figure		Page
1	RSRM Motor Configuration	47
2	RSRM-7A Igniter to Case Joint Putty Configuration	48
3	RSRM-7A Aft Center Segment Liner Pattern	49
4	RSRM-7A Forward Center Segment Liner Pattern	50
5	RSRM-7A Forward Segment Liner Pattern	51
6	RSRM Insulation Performance Stations	52
7	Nozzle to Case Joint Safety Factor Measurement	53
8	Field Joint (Clevis) Safety Factor Measurement	54
9	RSRM-7A Aft Dome Insulation Performance	55
10	RSRM-7A Aft Cylinder Insulation Performance	56
11	RSRM-7A Aft Center Segment Insulation Performance	57
12	RSRM-7A Forward Center Segment Insulation Performance	58
13	RSRM-7A Forward Segment Star Tip Insulation Performance	- 59
14	RSRM-7A Forward Segment Non-Star Tip Insulation Performance	60
15	RSRM-7B Igniter to Case Joint Putty Configuration	61
16	RSRM-7B Aft Center Segment Liner Pattern	62
17	RSRM-7B Forward Center Segment Liner Pattern	63
18	RSRM-7B Forward Segment Liner Pattern	64
19	RSRM-7B Aft Dome Insulation Performance	65
20	RSRM-7B Aft Cylinder Insulation Performance	66
21	RSRM-7B Aft Center Segment Insulation Performance	67



# FIGURES (CONT'D)

Figure		Page
22	RSRM-7B Forward Center Segment Insulation Performance	68
23	RSRM-7B Forward Segment Star Tip Insulation Performance	69 <sup>.</sup>
24	RSRM-7B Forward Segment Non-Star Tip Insulation Performance	70



# TABLES

Table		Page	1	
1	Summary of Nozzle to Case Joint and Field Joint Safety Factors	71		
2	Summary of Factory Joint Safety Factors	72		
3	Summary of Case Insulation Safety Factors	73		
4	Criteria for Classifying Potential Anomalies	74		
5	RSRM-7 Final Clevis Edge Separation Conditions	75		
6	RSRM-7 Final Tang Edge Separation Conditions	76		
7	RSRM-7A Nozzle to Case Joint Performance	77		
8	RSRM-7A Aft Field Joint Performance	78		
9	RSRM-7A Center Field Joint Performance	79		
10	RSRM-7A Forward Field Joint Performance	80		
11	RSRM-7A Aft Dome Insulation Performance	81		
12	RSRM-7A Aft Cylinder Insulation Performance	84		
13	RSRM-7A Aft Center Segment Insulation Performance	90		
14	RSRM-7A Forward Center Segment Insulation Performance	93		
15	RSRM-7A Forward Segment Star Tip Insulation Performance	96	•	
16	RSRM-7A Forward Segment Non-Star Tip Insulation Performance	99		
17	RSRM-7B Nozzle to Case Joint Performance	102		
18	RSRM-7B Aft Field Joint Performance	103		
19	RSRM-7B Center Field Joint Performance	104		
20	RSRM-7B Forward Field Joint Performance	105		
21	RSRM-7B Aft Dome Insulation Performance	106		
22	RSRM-7B Aft Cylinder Insulation Performance	109		
23	RSRM-7B Aft Center Segment Insulation Performance	115		
REVISION <u>A</u>	DOC NO. TWR-17546		/OL	III
FORM TC 7994-310 (REV 2		-	,	

ix



# TABLES (CONT'D)

Table		Page
24	RSRM-7B Forward Center Segment Insulation Performance	118
25	RSRM-7B Forward Segment Star Tip Insulation Performance	121
26	RSRM-7B Forward Segment Non-Star Tip Insulation Performance	124



# Appendix A

Table		Page
A-1	RSRM-7A Aft Dome Factory Joint Weatherseal Evaluation	128
A-2	RSRM-7A Aft Segment Stiffener to Stiffener Factory Joint Weatherseal Evaluation	129
A-3	RSRM-7A Aft Segment ET Attach to Stiffener Factory Joint Weatherseal Evaluation	130
A-4	RSRM-7A Aft Center Segment Factory Joint Weatherseal Evaluation	130
A-5	RSRM-7A Forward Center Segment Factory Joint Weatherseal Evaluation	131
A-6	RSRM-7A Forward Segment Cylinder to Cylinder Factory Joint Weatherseal Evaluation	131
A-7	RSRM-7A Forward Dome Factory Joint Weatherseal Evaluation	132
A-8	RSRM-7A Aft Stiffener Ring TPS Evaluation	132
A-9	RSRM-7A Center Stiffener Ring TPS Evaluation	133
A-10	RSRM-7A Forward Stiffener Ring TPS Evaluation	133
A-11	RSRM-7A Forward Stiffener Stub TPS Evaluation	134
A-12	RSRM-7A Nozzle to Case Joint Insulation Evaluation	135
A-13	RSRM-7A Nozzle to Case Joint Vent Slot Fill	136
A-14	RSRM-7A Aft Field Joint Insulation Evaluation	137
A-15	RSRM-7A Center Field Joint Insulation Evaluation	138
A-16	RSRM-7A Forward Field Joint Insulation Evaluation	139
A-17	RSRM-7A Igniter Boss Insulation Evaluation	140
A-18	RSRM-7A Igniter Chamber Insulation Evaluation	140
A-19	RSRM-7A Igniter Adapter to Forward Dome Putty Evaluation	141
A-20	RSRM-7A Igniter Adapter to Igniter Chamber Putty Evaluation	142



# Appendix A (Cont'd)

Table	Page
A-21 RSRM-7A Aft Segment Internal Insulation Evaluation	143
A-22 RSRM-7A Aft Segment NBR Inhibitor Height Evaluation	144
A-23 RSRM-7A Aft Segment NBR Inhibitor Tear Evaluation	145
A-24 RSRM-7A Aft Center Segment Internal Insulation Evaluation	146
A-25 RSRM-7A Aft Center Segment NBR Inhibitor Height Evaluation	146
A-26 RSRM-7A Aft Center Segment NBR Inhibitor Tear Evaluation	147
A-27 RSRM-7A Aft Center Segment Stress Relief Flap Evaluation	148
A-28 RSRM-7A Forward Center Segment Internal Insulation Evaluation	149
A-29 RSRM-7A Forward Center Segment NBR Inhibitor Height Evaluation	149
A-30 RSRM-7A Forward Center Segment NBR Inhibitor Tear Evaluation	150
A-31 RSRM-7A Forward Center Segment Stress Relief Flap Evaluation	151
A-32 RSRM-7A Forward Segment Internal Insulation Evaluation	152
A-33 RSRM-7A Forward Segment Stress Relief Flap Evaluation	153
A-34 RSRM-7A Insulation Postfire Photograph List	154



# Appendix B

Table		Page
B-1	RSRM-7B Aft Dome Factory Joint Weatherseal Evaluation	158
B-2	RSRM-7B Aft Segment Stiffener to Stiffener Factory Joint Weatherseal Evaluation	159
B-3	RSRM-7B Aft Segment ET Attach to Stiffener Factory Joint Weatherseal Evaluation	160
B-4	RSRM-7B Aft Center Segment Factory Joint Weatherseal Evaluation	160
B-5	RSRM-7B Forward Center Segment Factory Joint Weatherseal Evaluation	161
B-6	RSRM-7B Forward Segment Cylinder to Cylinder Factory Joint Weatherseal Evaluation	162
B-7	RSRM-7B Forward Dome Factory Joint Weatherseal Evaluation	163
B-8	RSRM-7B Aft Stiffener Ring TPS Evaluation	163
B-9	RSRM-7B Center Stiffener Ring TPS Evaluation	164
B-10	RSRM-7B Forward Stiffener Ring TPS Evaluation	164
B-11	RSRM-7B Forward Stiffener Stub TPS Evaluation	165
B-12	RSRM-7B Nozzle to Case Joint Insulation Evaluation	166
B-13	RSRM-7B Nozzle to Case Joint Vent Slot Fill	167
B-14	RSRM-7B Aft Field Joint Insulation Evaluation	168
B-15	RSRM-7B Center Field Joint Insulation Evaluation	169
B-16	RSRM-7B Forward Field Joint Insulation Evaluation	170
B-17	RSRM-7B Igniter Boss Insulation Evaluation	171
B-18	RSRM-7B Igniter Chamber Insulation Evaluation	171
B-19	RSRM-7B Igniter Adapter to Forward Dome Putty Evaluation	172
B-20	RSRM-7B Igniter Adapter to Igniter Chamber Putty Evaluation	173



# Appendix B (Cont'd)

<u>Table</u>		Page
B-21	RSRM-7B Aft Segment Internal Insulation Evaluation	174
B-22	RSRM-7B Aft Segment NBR Inhibitor Height Evaluation	175
B-23	RSRM-7B Aft Segment NBR Inhibitor Tear Evaluation	176
B-24	RSRM-7B Aft Center Segment Internal Insulation Evaluation	177
B-25	RSRM-7B Aft Center Segment NBR Inhibitor Height Evaluation	177
B-26	RSRM-7B Aft Center Segment NBR Inhibitor Tear Evaluation	178
B-27	RSRM-7B Aft Center Segment Stress Relief Flap Evaluation	179
B-28	RSRM-7B Forward Center Segment Internal Insulation Evaluation	180
B-29	RSRM-7B Forward Center Segment NBR Inhibitor Height Evaluation	180
B-30	RSRM-7B Forward Center Segment NBR Inhibitor Tear Evaluation	181
B-31	RSRM-7B Forward Center Segment Stress Relief Flap Evaluation	182
B-32	RSRM-7B Forward Segment Internal Insulation Evaluation	183
B-33	RSRM-7B Forward Segment Stress Relief Flap Evaluation	184
B-34	RSRM-7B Insulation Postfire Photograph List	185



### ACRONYM LIST

**ASF** Actual Safety Factor CEI Contract End Item CF/EPDM - Carbon Fiber Filled EPDM CSF - Compliance Safety Factor DFI Development Flight Instrumentation DR Discrepancy Report EMT Engineering Management Team EPDM Ethylene Propylene Diene Monomer ET - External Tank E.T. - Exposure Time FRR - Flight Readiness Review HPM High Performance Motor

I.D. - Inside Diameter
IFA - In Flight Anomaly
KSC - Kennedy Space Center

 $M + 3\sigma$  - Median Plus Three Times The Standard Deviation

MDD - Material Decomposition Depth MDR - Material Decomposition Rate MDT - Minimum Design Thickness

NBR - Acrylonitrile Butadiene Rubber

PEEP - Postfire Engineering Evaluation Plan

PFAR - Postfire Anomaly Record

PR - Problem Report

PSI - Pounds Per Square Inch

RPRB - Redesign Program Review Board RSRM - Redesigned Solid Rocket Motor

SRB - Solid Rocket Booster SRM - Solid Rocket Motor

STS - Space Transportation System
TPS - Thermal Protection System

DOC NO. TWR-17546 VOL III
SEC PAGE

REVISIO



#### 1.0 INTRODUCTION

STS-33 was launched from KSC pad 39B on 22 November 1989. Two of the Redesigned Solid Rocket Motors were part of the launch system and were designated RSRM-7A (360L007A) and RSRM-7B (360L007B). Both motors incorporated the redesigned nozzle to case joint and case field joint as shown on Figure 1. Following booster separation and splashdown, the motors were recovered and returned to Cape Canaveral Hangar AF for disassembly and inspection.

Following the inspection at Hangar AF, the segments were returned to the Thiokol Corporation H-7 refurbishment facility. There, the insulation thicknesses were measured, and the factory joints were disassembled. The documentation of these inspections and the insulation thermal performance evaluation (material decomposition safety factor) have been added to this final release of the report.

In an attempt to standardize and document the evaluation of flight RSRMs, a Postflight Engineering Evaluation Plan has been written (References 1 and 2). The PEEP outlines the basic evaluations to be performed. Appropriate procedures contained in this plan were used to evaluate the internal and external insulation. Addendums to the PEEP were written which outline additional evaluations to be performed on the RSRM-7A and RSRM-7B motors to assess conditions documented on prefire discrepancy reports (References 3 and 4). The intent of these procedures was to insure that all pertinent evaluation points were examined and documented in a consistent and complete manner.

#### 2.0 OBJECTIVES

The objective of this report is to document the postflight condition of the internal and external insulation and evaluate the material decomposition safety factors of the RSRM-7A and RSRM-7B internal insulation. An additional objective of this document is to discuss the Insulation Component Program Team assessment of the observations.



# 3.0 SUMMARY

A summary of the RSRM-7A and RSRM-7B external and internal insulation condition is found below. A detailed description of the results can be found in Sections 6.0 through 9.0.

#### 3.1 EXTERNAL INSULATION

### 3.1.1 Factory Joint Weatherseals

Two of the fourteen weatherseals on this flight set exhibited unbonds.

The RSRM-7A aft segment stiffener to stiffener factory joint weatherseal was unbonded on the aft edge for approximately 70% of the circumference. The depth of the unbond measured from 0.8 to 0.9 inch which was to the pin retainer band. The unbond exhibited Chemlok 205 to case failure. Water was dripping from the unbond, and corrosion was evident under the unbond. There was no evidence of soot or heat effects on the unbonds. Paint was peeled up from the case and attached to the edge of the weatherseal intermittently along the unbond. Corrosion was evident on the case under the peeled paint. A small forward edge unbond was also noted near 310° and measured 0.5 inch longitudinally by approximately 0.75 inch circumferentially.

Two insulation to case unbonds were identified on the forward edge of the RSRM-7B forward segment cylinder to cylinder weatherseal. The weatherseal was unbonded centered at 160° for 14 inches to a depth ranging from 1.0 to 1.5 inches. The paint was also peeled and missing from the case in the area forward of the weatherseal in two places. The occurrences measured 2.4 inches longitudinally by 5 inches circumferentially and 3.25 inches longitudinally by 7 inches circumferentially. The forward edge of the weatherseal was also unbonded centered at 135° for 11 inches to a depth of 0.1 inch. An aft edge unbond was noted at 210° and measured 0.6 inch longitudinally by approximately 1 inch, circumferentially. All unbonds were at the Chemlok 205 to case interface.

The other factory joint weatherseals appeared to be in excellent condition. Normal heat effects and discoloration were evident on the weatherseals of both aft segments, and normal debris impact damage from re-entry was evident intermittently on the aft edges of the weatherseals.

REVISIO A	DOC NO.	TWR-17546	46   VOL III	
	SEC	PAGE		
FORM TC 7994-310 (REV 2-88)			_	

2

U (REV 2-88)



No significant areas of missing EPDM insulation were noted. The K5NA closeouts over the thermocouple wires were in good condition, with no evidence of water leaking from any of the these locations.

# 3.1.2 Stiffener Stubs and Rings

The insulation over the stiffener stubs and rings was in good condition. Normal heat effects and discoloration were evident on all surfaces in the 220°-270°-320° region. There were no significant areas of missing material. The EPDM was well bonded to the stiffener stubs and appeared to be well bonded to the stiffener rings. There was very little stiffener ring damage since the sea state was high at splashdown. The K5NA repair on the outboard edge of both forward stiffener stubs showed normal erosion and some small missing chunks intermittently around the circumference.

#### 3.2 NOZZLE TO CASE JOINTS

Based on the visual evaluation, both nozzle to case joints performed well. No gas paths through the polysulfide adhesive were identified. The RSRM-7A polysulfide bondline failed 83% cohesively at disassembly while the RSRM-7B bondline failed 89% cohesively at disassembly.

One small void in the polysulfide was identified on the RSRM-7A joint at 109° and measured 1.6 inches longitudinally by 0.25 wide. The void extended across the step but did not extend to the wiper 0-ring and was not penetrated by hot gas. Porosity was evident on both joints in the step region. The average polysulfide vent slot fill was 32% on RSRM-7A and 84% on RSRM-7B.

#### 3.3 FIELD JOINTS

The internal insulation in all six of the case field joints performed as designed, and no anoralous conditions were identified. J-leg tip contact was evident full circumference at each joint. Wet soot deposits extending down the bondline were noted on all of the RSRM-7 field joints, generally to a depth of 0.2 to 0.7 inch radially into the bondline (outboard from the remaining material). The maximum depth of the wet soot was 1.35 inches on the RSRM-7B center field joint. No heat

REVISIONA DOC NO. TWR-17546 VOL III

3

FORM TC 7994-310 (REV 2-88)



effects were evident under the soot. Similar wet sooting has been noted on previous RSRM joints and is believed to occur at re-entry or splashdown during joint flexing.

There were no clevis edge separations that were recordable (over 0.10 inch depth). Some tang edge separations were visible on the field joints. The tang insulation edge separations were probed during postflight inspection at Clearfield H-7. The deepest postfire tang edge separation had a depth of 0.25 inch as compared with no prefire separation. These separations are documented in Tables 5 and 6.

Clevis insulation cracks were noted on the radius region insulation on four of the six field joints. Some cracks were noted on prefire Problem Reports. The cracks did not have any effect on the function of the joint.

# 3.4 IGNITER JOINTS AND INSULATION

The condition of the igniter boss insulation was excellent. An evaluation of both RSRM-7A and RSRM-7B igniter boss insulation to case interfaces revealed no edge separations. The molded insulation surface was in good condition, and both joints exhibited normal erosion on the inboard surface. One blowhole through the putty was present on the RSRM-7A igniter to case joint at 332°. The putty in the RSRM-7B joint had no blowholes, however, putty was extruded up to the adapter full circumference and onto the aft face of the adapter intermittently around the circumference.

The RSRM-7A igniter adapter to igniter chamber joint was in good condition with no blowholes. The igniter adapter to igniter chamber joint on the RSRM-7B had a blowhole through the putty at 340°. Soot was in the putty from 315° to 350° but did not extend to the gasket. No adverse effects on the performance of the joint resulted from either of the blowholes.

#### 3.5 INTERNAL ACREAGE INSULATION

The acreage insulation, including the internal insulation over each of the factory joints, was in good condition. No evidence of hot gas penetration through the insulation was identified.

REVISION A	DOC NO.	TWR-17546	VOL	III
<del></del>	SEC	PAGE		
FORM TC 7994-310 (REV 2-88)		+	,	



### 3.5.1 Aft Segments

Four to six small blisters were identified in the CF/EPDM in the RSRM-7A aft dome. The largest blister measured 1.75 inches axially by 0.25 inches circumferentially. This was significantly less than was seen on the previous flight set and is considered a normal condition.

The aft segment NBR inhibitor stubs exhibited scalloped erosion around the circumference. These areas had a very short inhibitor stub with intermittent inhibitor pieces taller than adjacent areas. This condition has been noted on all previous flight RSRM aft segments. This uneven erosion was not typically seen to this extent on HPM motors, but it does not appear to be a problem. There were no tears in either inhibitor.

The aft segment acreage insulation was in normal condition. There were no gouges, separations, cuts, missing material, excessive erosion, or other areas of blisters.

### 3.5.2 Center Segments

Only two inhibitor tears greater than 3 inches radially were noted in either aft center segment inhibitor stub. Both were noted on the RSRM-7B aft center segment and measured 4.0 and 4.5 inches in length.

Some radial tears were noted in the forward center segment NBR inhibitor stubs (nine on RSRM-7A and eight on RSRM-7B). The tears in the forward center segments ranged from 5.0 to 11.75 inches radially. The radial extent and frequency of the tears identified in the inhibitor stubs are within the range of tears noted on past flight motors. The edges of the tears demonstrated no material loss or erosion. This indicated that the tears occurred after motor burn.

The acreage insulation exhibited normal ercsion. The castable inhibitor was completely missing on all four center segments. The flap and CF/EPDM was completely eroded to the flap bulb on the aft center segments and partially eroded on the forward center segments.

DOC NO.	TWR-17546	VOL	III
SEC	PAGE		
	l	5	



### 3.5.3 Forward Segments

The stress relief flap was present full circumference on both forward segments but was heat affected and eroded. The castable inhibitors were completely missing full circumference. The flaps had a scalloped appearance similar to that seen on previous RSRM flight forward segment flaps. The acreage insulation was in normal condition. The eleven point star pattern was easily distinguishable in the liner.

A detailed examination was performed on the insulation in both forward domes near the igniter boss to inspect for evidence of voids or thin insulation. No gas paths or areas of abnormal erosion were identified. The insulation in this area was also removed, and no indications of folds or voids at the insulation to case interface were noted. Dissection and evaluation of the two RSRM-7 igniter boss forward dome samples were completed and thickness measurements, void mapping, and photographs of the samples were done. In general, these insulation lay-ups looked very good. Inspection by Process Engineering showed there were only 6 to 10 small voids (typically 0.10 inch with 0.17 inch maximum diameter) and several small folds at the case surface for each layup.

#### 3.6 INSULATION THERMAL PERFORMANCE

No unacceptable conditions were found in the thermal safety factor evaluation of the nozzle to case joints, field joints, factory joints, and case wall acreage areas. All safety factors exceeded the minimum requirements. A summary of minimum safety factors can be found in Tables 1 through 3.

#### 4.0 CONCLUSIONS

During the KSC evaluation, Squawk forms were generated to report and track observations which violated the Postflight Engineering Evaluation Limits (Reference 1). The Squawks were reviewed by the SRB/SRM Postflight Assessment Team, and some of the Squawks were elevated to PRs.

All observations presented in this document were reviewed by the Insulation Component Program Team to determine which observations were potential anomalies. The observations documented on PRs and Squawks

DOC NO.	TWR-17546	VOL	III
SEC	PAGE		



were automatically termed potential anomalies. The Insulation Component Program Team then classified each of the potential anomalies as 'critical', 'major', or 'minor' anomaly or 'remains observation' as defined per the Table 4 Redesign Program Review Board (RPRB) criteria.

#### 4.1 KSC EVALUATION CLASSIFICATIONS

The Insulation Component Program Team identified two conditions observed at KSC which were considered potential anomalies:
'MINOR ANOMALY'

1. The RSRM-7A aft segment stiffener to stiffener factory joint weatherseal was unbonded on the aft edge for approximately 70% of the circumference. The unbond exhibited Chemlok 205 to case failure. A small forward edge unbond was also noted near 310°. The following documentation was written against these conditions:

KSC Squawk I.D. number 33-026 KSC PR PV6-146111 PFAR 360L007A-04

Two insulation to case unbonds were identified on the forward edge of the RSRM-7B forward segment cylinder to cylinder weatherseal. The weatherseal was unbonded at 160° for 14 inches and at 135° for 11 inches. A small aft edge unbond was noted at 210°. All unbonds were at the Chemlok 205 to case interface. The following documentation was written against these conditions:

KSC Squawk I.D. number 33-024 KSC PR PV6-145966 PFAR 360L007B-01

These unbonds are believed to be a result of surface contamination and do not represent a flight debris concern. A team has been established to evaluate weatherseal unbonds. The condition was classified as a 'minor' anomaly.

#### 'REMAINS OBSERVATION'

2. Repair adhesive from a prefire clevis insulation separation repair was noted on the clevis ramp insulation of the RSRM-7A aft segment and on the tip of the clevis insulation of the RSRM-7B aft center segment. The following documentation was written against this condition:

PFAR 360L007A-14 PFAR 360L007B-26

DOC NO.	TWR-17	546	VOL	III
SEC		PAGE	-	
	ľ			



Since the adhesive did not extend into the bonding region of the joint and did not affect the function of the joint, it was classified as 'remains observation'.

The Insulation Component Program Team presented their assessment of the observations shown in this document to the RPRB on 13 December 1989. The RPRB accepted the insulation team's classifications as presented.

#### 4.2 H-7 EVALUATION CLASSIFICATIONS

The Insulation Component Program Team identified no conditions observed at Clearfield H-7 which were considered potential anomalies.

The Insulation Component Program Team presented their assessment of the Clearfield H-7 observations to the RPRB on 29 August 1990.

Insulation Design has concluded that the RSRM-7A and RSRM-7B insulation systems performed as designed.

#### 5.0 RECOMMENDATIONS

The following recommendations are based on the results of the RSRM-7 postflight inspection.

#### 5.1 KSC EVALUATION RECOMMENDATIONS

- 1. Increased controls should be implemented in the processing of the factory joint weatherseals to eliminate contamination and ensure adequate bond strengths are achieved.
- M-111 planning should be reviewed to insure adequate precautions and inspections are made in conjunction with clevis insulation edge separation repairs.

# 5.2 H-7 EVALUATION RECOMMENDATIONS

 Insulation thickness measurements need to continue to be screened and all outlying data re-measured and verified or corrected to ensure that safety factor violations do not occur due to bad data.

#### 6.0 RSRM-7A VISUAL EVALUATIONS

During the postflight evaluation, Insulation Design documented the condition of the external factory joint weatherseals, stiffener rings, stiffener stubs, nozzle to case joint, case field joints, igniter to case

REVISION	DOC NO.	TWR-17546	VOL	III
	SEC	PAGE		
FORM TC 7994-310 (REV 2-88)		1	_	

8

P310 (NEA 5-99)



joint, segment acreage insulation, NBR inhibitors, and stress relief flap regions. A copy of this documentation for RSRM-7A can be found in Appendix A. The condition of the RSRM-7A insulation components is discussed in the following subsections.

#### 6.1 RSRM-7A EXTERNAL INSULATION

### 6.1.1 RSRM-7A Factory Joint Weatherseals

Each factory joint weatherseal was visually inspected, and the results are recorded in Tables A-1 through A-7. No significant areas of missing EPDM insulation were noted on any factory joint weatherseal.

The weatherseals on all three aft segment factory joints were slightly heat affected from 220°-270°-320° due to the plume radiation from the solid rocket motors and shuttle main engines. The heaviest heat effects occurred near 270°. This is a normal occurrence that had no effect on the performance of the weatherseals.

The RSRM-7A aft segment stiffener to stiffener factory joint weatherseal was unbonded on the aft edge for approximately 70% of the circumference. The depth of the unbond measured from 0.8 to 0.9 inch which was to the pin retainer band. The unbond exhibited Chemlok 205 to case failure. There was no evidence of soot or heat effects on the unbonds. Paint was peeled up from the case and attached to the edge of the weatherseal intermittently along the unbond. Corrosion was evident on the case under the peeled paint and under the unbonded weatherseal. A small forward edge unbond was also noted near 310° and measured 0.5 inch longitudinally by approximately 0.75 inch circumferentially. This was the only joint which showed any moisture under the weatherseal.

Research of the manufacturing logs for the RSRM-7 factory joint weatherseals revealed that the Conscan readings for the RSRM-7A aft segment stiffener to stiffener weatherseal aft bonding surface were above current planning requirements. Results of the swab sample taken at KSC in the unbond revealed no measurable contamination.

A team has been established to evaluate the occurrence of weatherseal unbonds. Until this evaluation is completed and corrective action is taken, weatherseal unbonds are expected to continue to occur. It has

DOC NO. TWR-17546 VOL III
SEC PAGE
9



been analyzed and determined that the unbonds do not represent a flight concern; however, the resulting case corrosion problems are being dealt with by removing the weatherseals at Hangar AF.

The remainder of the RSRM-7A weatherseals were in excellent condition.

# 6.1.2 RSRM-7A Stiffener Stub and Rings

The condition of the insulation over the forward stiffener stub and the stiffener rings is recorded in Tables A-8 through A-11. The insulation was in good condition with normal heat effects and discoloration on all surfaces. The heaviest heat effects occurred from 220°-270°-320° due to the plume radiation from the solid rocket motors and shuttle main engines. No visible damage to any stiffener ring insulation was noted. This was due to the rough sea state at the time of booster splashdown. Some insulation unbonds were noted on the end of the ring segments after removal from the case. These unbonds were a result of the hydrolazing process.

The K5NA repair on the outboard edge of the forward stiffener stub showed normal erosion and some small missing chunks intermittently around the circumference.

#### 6.2 RSRM-7A NOZZLE TO CASE JOINT

The nozzle to case joint insulation condition is recorded in Tables A-12 and A-13. The nozzle to case joint performed as expected with no polysulfide blowholes identified across the bondline. One small void in the polysulfide was identified at 109° and measured 1.6 inches longitudinally by 0.25 wide. The void extended across the step but did not extend to the wiper 0-ring and was not penetrated by hot gas. Polysulfide porosity was evident in the step region full circumference.

The failure mode of the polysulfide bondline at disassembly was approximately 83% cohesive within the polysulfide, 15% adhesive at the NBR to polysulfide interface, and 2% adhesive at the phenolic to polysulfide interface. The vent slots showed an average polysulfide fill of 32% with values ranging from 0% to 100% fill.

REVISIONA	DOC NO.	TWR-17546	VOL III
<del></del>	SEC	PAGE	
FORM TC 7994-310 (REV 2-88)		' :	10



The bondline around the circumference demonstrated erosion similar to that observed on previous RSRM motors. The polysulfide was decomposed further into the joint than the flap erosion. For approximately 0.40 inch aft of the erosion, the polysulfide was partially decomposed and bubbled. Although the material was partially decomposed, no gas flow occurred in the adhesive bondline decomposed region.

The insulation erosion in the joint region was similar to the condition of previous RSRM flight motors. The NBR flap and baffle appeared to be bonded in place and in excellent shape with normal heat effects and erosion.

#### 6.3 RSRM-7A FIELD JOINTS

#### 6.3.1 RSRM-7A Aft Field Joint

The joint insulation configuration performed as designed. The joint insulation surfaces exhibited normal charring and erosion. Measurements of the tang material char depths and bondline contact are provided in Table A-14.

The general appearance of the pressure sensitive adhesive was noted. Contact within the joint was based on the flat appearance and matted texture of the adhesive, and non-contact was based on the glossy appearance of the adhesive. The joint appeared to have made contact full circumference at the tip of the J-leg. The bondline contact was measured at 0°, 90°, 180°, and 270°. The average contact was 0.98 inch.

No evidence of motor chamber gas leakage to the 0-rings or past the J-joint insulation was identified.

Wet sooting into the joint bondline was essentially uniform full circumference to 0.30 to 0.40 inch outboard from the remaining material. Wet sooting similar to this has been seen on previous flight sets and is believed to occur during motor re-entry or splashdown when the joint may flex and allow soot into the bondline.

Cracks and crazing were also noted on the clevis insulation in the radius region at 38°, 82°, 140°, and 310°. Cracks on this segment were noted on a prefire PR. None of the cracks had any effect on the function of the joint.

REVISION	DOC NO.	TWR-17546	vor III
<del></del>	SEC	PAGE	-
FORM TC 7994-310 (REV 2-88)		1	11



Repair adhesive from a prefire clevis insulation separation repair was noted on the clevis ramp insulation at 245°. The adhesive measured approximately 1 inch long by 0.05 inch circumferentially by 0.01 inch thick. The adhesive did not extend into the bonding region of the joint and did not affect the function of the joint. Evaluation of the segment logs indicates that the edge separation repair was performed at Thiokol before shipment to KSC.

No clevis or tang edge separations were identified at KSC. During inspection at Clearfield H-7, no recordable (over 0.10 inch deep) clevis edge separations were identified. Tang edge separations were visible on the aft field joint. The tang insulation edge separations were hard probed during postflight inspection at Clearfield H-7. The deepest postfire tang edge separation had a depth of 0.175 inch as compared with a prefire separation of 0.03 inch. These separations are documented in Tables 5 and 6.

# 6.3.2 RSRM-7A Center Field Joint

The joint insulation configuration performed as designed. The joint insulation surfaces exhibited normal charring and erosion. Measurements of the tang material char depths and bondline contact are provided in Table A-15.

The general appearance of the pressure sensitive adhesive was noted. Contact and non-contact within the joint was based on the flat appearance and matted texture, or the glossy appearance of the adhesive. The joint appeared to have made contact full circumference at the tip of the J-leg. The bondline contact was measured at 0°, 90°, 180°, and 270°. The average contact was 1.16 inches.

No evidence of motor chamber gas leakage to the 0-rings or past the J-joint insulation was identified.

Wet sooting into the joint bondline was noted full circumference ranging from 0.30 to 0.70 inch outboard from the remaining material. Wet sooting is believed to occur during motor re-entry or splashdown when the joint may flex and allow soot into the bondline.

Tape adhesive residue was noted intermittently on the clevis insulation surfaces and had no effect on the joint.

REVISION A	DOC NO.	TWR-17	546	VOL	III
	SEC		PAGE		
FORM TC 7994-310 (REV 2-88)	•		ŀ	12	



A small area of crazing was supposed to be at 158° on the clevis insulation in the radius region as defined on a prefire PR. The condition, however, could not be located.

No clevis or tang edge separations were identified at KSC. During inspection at Clearfield H-7, no recordable (over 0.10 inch deep) clevis edge separations were identified. Tang edge separations were visible on the center field joint. The tang insulation edge separations were hard probed during postflight inspection at Clearfield H-7. The deepest postfire tang edge separation had a depth of 0.150 inch as compared with no prefire separation. These separations are documented in Tables 5 and 6.

# 6.3.3 RSRM-7A Forward Field Joint

The joint insulation configuration performed as designed. The joint insulation surfaces exhibited normal charring and erosion. Measurements of the tang material char depths and bondline contact are provided in Table A-16.

The general appearance of the pressure sensitive adhesive was noted. The joint appeared to have made contact full circumference at the tip of the J-leg. The contact area appeared flat with a matted texture. The bondline contact was measured at 0°, 90°, 180°, and 270°. The average contact was 1.16 inches.

No evidence of motor chamber gas leakage to the O-rings or past the J-joint insulation was identified. No evidence of cracks or crazing was identified on the joint insulation surfaces.

Wet sooting into the joint bondline ranged from 0.30 to 0.60 inch outboard from the remaining material full circumference.

No clevis or tang edge separations were identified at KSC. During inspection at Clearfield H-7, no recordable (over 0.10 inch deep) clevis edge separations were identified. Tang edge separations were visible on the forward field joint. The tang insulation edge separations were hard probed during postflight inspection at Clearfield H-7. The deepest postfire tang edge separation had a depth of 0.210 inch as compared with no prefire separation. These separations are documented in Tables 5 and 6.

DOC NO.	TWR-17546	VOL	III
SEC	PAGE		



#### 6.4 RSRM-7A IGNITER JOINTS AND INSULATION

The condition of the igniter to case joint insulation is recorded in Tables A-17 through A-20. The condition of the igniter boss insulation was excellent. An evaluation of the insulation to case interface revealed no edge separations. There was a small amount of loose flashing on the igniter boss near 60°. This is a fairly typical condition. The boss molded insulation surface was in good condition with normal erosion on the inboard surface.

The overall condition of the putty in the igniter to case joint was good. The color of the putty was a consistent light olive green. The putty exhibited 100% cohesive failure and nominal tack for the full circumference. There was one blowhole present through the putty at 332°. The blowhole was 1.15 inches circumferentially at the aft edge and 0.20 inch circumferentially at the forward edge. The blowhole resulted in soot on the metal surface forward of the putty full circumference. A map of the putty condition is shown in Figure 2.

The condition of the putty in the adapter to chamber joint was good. The color of the putty was a consistent light olive green. The putty exhibited 100% cohesive failure and good tack for the full circumference. No blowholes were noted in the putty of this joint.

The igniter internal and external insulation was in normal condition. No areas of blistering or abnormal erosion were present.

#### 6.5 RSRM-7A ACREAGE INSULATION

#### 6.5.1 RSRM-7A Aft Segment Acreage Insulation

The aft segment internal insulation was in excellent condition and is recorded in Tables A-21 through A-23.

The forward facing NBR inhibitor stub exhibited scalloped erosion intermittently around the circumference. These areas had a very short inhibitor stub with intermittent inhibitor pieces taller than adjacent areas. A similar condition has been noted on all previous RSRM flight aft segments. Measurements of the remaining inhibitor stub were taken every 30° and are contained in Table A-22. The inhibitor height ranged from 4.5 to 8.5 inches. Although the erosion was uneven, the remaining inhibitor stub heights for this segment were within the expected

DOC NO. TWR-17546 VOL III
SEC PAGE



tolerance band for past flight motors based on a statistical analysis of the historical database (Reference 5). There were no inhibitor tears greater than 3 inches in length noted on this inhibitor.

The segment had no liner remaining. This condition is common for an aft segment.

The erosion in the aft dome was similar to past flight motors. NBR under the CF/EPDM was exposed intermittently in the area roughly 20 inches forward of the nozzle boss. This is a common condition in the aft dome. Four to six small blisters were identified in the CF/EPDM in the aft dome. The largest blister was near 300° and measured 1.75 inches axially by 0.25 inches circumferentially. All blisters were in an area approximately 13 inches forward of the nozzle boss. The size and frequency of the blisters were significantly less than was seen on the previous flight set and are considered a normal condition.

The aft segment acreage insulation was in normal condition. There were no gouges, separations, cuts, missing material, excessive erosion, or other areas of blisters.

# 6.5.2 RSRM-7A Aft Center Segment Acreage Insulation

The condition of the aft center segment internal insulation is recorded in Tables A-24 through A-27.

The forward facing NBR inhibitor stub exhibited uniform erosion full circumference. Measurements of the remaining NBR inhibitor stub were taken every 30° and are contained in Table A-25. The inhibitor stub heights ranged from 11.5 to 14.5 inches for this segment, which is within the expected tolerance band. There were no inhibitor tears greater than 3 inches in length noted on this segment. Three areas of missing material were noted on the heat affected edge of the inhibitor between 45° and 90°. These appeared to be the result of splashdown debris.

Liner coverage in the aft center segment was heavy near the clevis end and generally missing aft of the factory joint. The diagram of the liner pattern is shown in Figure 3.

The condition of the flap region is recorded in Table A-27. The castable inhibitor was completely missing full circumference, and the stress relief flap was eroded back to the flap bulb full circumference.

REVISION DOC NO. TWR-17546 VOL III
FORM TC 7994-310 (REV 2-88)

15

310 (REV 2-88)



Both of these conditions are typical of an aft center segment. The CF/EPDM under the flap was eroded away full circumference. The exposed NBR under the flap appeared to be heat affected.

No evidence of blisters, separations, gouges, cuts, missing material, or excessive erosion was identified in the aft center segment.

# 6.5.3 RSRM-7A Forward Center Segment Acreage Insulation

The condition of the forward center segment internal insulation is recorded in Tables A-28 through A-31.

The forward facing NBR inhibitor stub exhibited uniform erosion full circumference. Measurements of the remaining NBR inhibitor stub were taken every 30° and are contained in Table A-29. The inhibitor stub heights for this segment ranged from 23.75 to 27.5 inches for this segment, which is within the expected tolerance band.

Nine radial tears greater than 3 inches long were noted. The longest tear was 11.75 inches and extended radially outward to approximately 12.5 inches inboard of the clevis I.D. surface. The edges of the tears demonstrated no material loss or erosion. This indicated that the tears occurred after motor burn. The location and length of the tears are contained in Table A-30. The tears are believed to be a result of re-entry or splashdown loads.

Liner coverage for the forward center segment was heavy near the clevis end and mostly missing aft of the factory joint. The diagram of the liner pattern is shown in Figure 4.

The castable inhibitor was completely missing full circumference, which is typical of a forward center segment. The end of the stress relief flap measured from 6.5 to 11.5 inches forward of the tip of the tang. Axial measurements were taken every 90° and are shown in Table A-31. There were no flap tears. The CF/EPDM under the flap was present but slightly eroded and hear affected full circumference. A number of small blisters (approximately 0.25 by 0.50 inch) were noted in the CF/EPDM between 54° and 80°. These were noted between 4 and 9 inches forward of the tip of the tang. Only one of the blisters was opened. The condition appeared to be the result of normal heat effects.

DOC NO.	TWR-17546	VOL	III	
SEC	PAGE			
	ı	16		



No other evidence of blisters, separations, gouges, cuts, missing material, or excessive erosion was identified in the forward center segment.

# 6.5.4 RSRM-7A Forward Segment Acreage Insulation

The condition of the forward segment internal insulation is recorded in Tables A-32 and A-33.

The eleven point star pattern in the liner was easily distinguishable, and the star and non-star liner termination points were comparable to past flight motors, as shown in Figure 5. The liner remaining under the star tip regions was present from the tip of the tang forward to 142.0 inches. The liner remaining under the non-star tip was present from the tip of the tang forward to 148.5 inches. The liner was light between the tip of the tang and the flap bulb.

The castable inhibitor was completely missing full circumference. The end of the stress relief flap measured from 3.5 (full flap remaining) to 7.0 inches forward of the tip of the tang. Axial measurements were taken every 90° and are shown in Table A-33. The flap was scalloped and curled back. The NBR under the flap was heat affected full circumference as has been seen on all previous RSRM forward segments.

A detailed examination was performed on the insulation in the forward dome near the igniter boss to inspect for excessive erosion, insulation voids, and thin insulation. No gas paths or areas of abnormal erosion were identified. The insulation in this area was removed and evaluated further. No indications of folds or voids at the insulation to case interface were noted. Dissection and evaluation of the RSRM-7A boss forward dome samples were completed and thickness measurements, void mapping, and photographs of the samples were done. Inspection showed there were a few small voids (typically 0.10 inch with 0.17 inch maximum diameter) and one small fold at the case surface. average remaining insulation thickness (postfire) in the 5 inch to 7.5 inch distance from the igniter boss was 0.394 inch. The minimum remaining insulation thickness was 0.299 inch.

No evidence of blisters, separations, gouges, cuts, missing material, or excessive erosion was identified in the forward segment.

DOC NO. TWR-17546 VOL III
SEC PAGE



Table A-34 contains a list of all photographs taken of the RSRM-7A insulation.

#### 6.6 POSTFIRE EVALUATION OF RSRM-7A PREFIRE DISCREPANCIES

The prefire discrepancy reports for the RSRM-7A insulation were evaluated prior to launch to identify significant items. identified in References 3 and 4, and the postfire conditions are discussed below.

DR 157901-01 documented cuts, depressions, and missing material on the aft segment nozzle boss insulation bonding surface at 63°, 153°, 167°, 232°, 270°, and 330°. The condition was the result of a prefire nozzle removal operation. Postfire evaluation of this condition indicated that the surface irregularities had no effect on the function of the nozzle to case joint. The conditions in the bonding area were filled with polysulfide adhesive at joint assembly.

DR 169339-01 documented a depression intermittently around the entire circumference of the nozzle to case joint flap of the aft segment. This area was eroded away during normal motor operation, and no adverse effects were noted.

Cracks existed in the aft segment J-joint clevis insulation radius region at 82°, 95° (0.04 inch deep), 154° through 156°, and 238°. These were documented on PR PV6-136315 and PV6-136320. The cracks were evaluated, and no effects on the function of the joint were noted.

Missing material was noted on the tip of the aft center segment J-leg at 158°, 160°, and 166° as noted on DR 169323-01. This area was eroded away during normal motor operation, and no adverse effects were noted.

Missing material was noted aft of the capture feature 0-ring groove (region E, Reference 6) of the aft center segment tang end from 145° to 152° and from 155° to 158° as noted on DR 169331-01. This condition was inspected during the postfire evaluation, and no effects on the function of the joint were noted.

REVISION	DOC NO.	TWR-17546	AOF III
FORM TC 7994-310 (REV 2-88)	SEC	PAGE	10
			18



Contamination was noted on the insulation surface of the aft center segment 50 inches forward of the tang at 90°. The contamination was 1.1 inches longitudinally by 3.6 inches circumferentially and was cleaned off prior to continuing the manufacturing process. The discrepancy was documented on DR 169331-02. This location was inspected during the postfire evaluation, and no evidence of the condition remained.

A crack was noted in the aft center segment J-joint clevis insulation radius region at 158° measuring 0.09 inch deep by 0.075 inch in length. The condition was documented on PR PV6-134026. The area of the crack was inspected during the postfire evaluation, and the crack could not be located.

Missing material was noted on the molded tang surface of the forward segment in region E (Reference 6) at 251°. This condition was documented on DR 169545-01. This condition was inspected during the postfire evaluation, and no effects on the function of the joint were noted.

Voids were noted in the insulation in the forward segment igniter boss region as noted on DR 171514-01. The insulation in this region was removed for further evaluation. No indications of voids were found at the insulation to case surface.

Dissection and evaluation the RSRM-7A igniter boss forward dome samples were completed. Thickness measurements, void mapping, and photographs of the samples were done as discussed in Section 6.5.4.

# 7.0 RSRM-7A INSULATION PERFORMANCE EVALUATION

The RSRM-7A segments were insulated to meet the RSRM design drawing requirements. The internal insulation was designed to meet a 2.0 material decomposition safety factor in the nozzle to case joint, case field joint, and factory joint areas, and a 1.5 material decomposition safety factor for the acreage insulation for all segments. All safety factor analyses discussed in this report will deal with the above mentioned material decomposition safety factors.

The insulation was designed using M +  $3\sigma$  material decomposition depths established from the HPM database. References 7 and 8 explain the database analysis and the design methodology, respectively.

REVISION	DOC NO.	TWR-17546	VOL	III
FORM TC 7994-310 (REV 2-88)	SEC	PAGE		
		i	19	



The nozzle to case joint, field joints, factory joints, and case wall insulation were evaluated based on the actual safety factor and compliance safety factor as required by the CEI specification. This evaluation was done by the use of prefire and postfire measurements.

Prefire insulation thickness measurements were taken in the aft dome up to the 24.3 inch station by means of a template that was bolted to the nozzle boss. A depth gage was used to measure the distance from the template to the bare metal dome before insulation layup. The measurement was repeated after insulation cure to determine the distance from the template to the insulation surface. The two measurements were then subtracted to determine the prefire insulation thickness. This measurement process was performed a third time after firing and char removal to determine the postfire thickness and material decomposition depth.

Prefire thicknesses at all other locations within the motor were measured using ultrasonic inspection methods.

Postfire insulation thicknesses were determined in the aft segment (forward of the 24.3 inch station), the center segments, and the forward segment by drilling holes in the insulation to the case wall and measuring the insulation thickness with a depth gage.

For the purpose of this report, the nozzle to case joint and the field joints will be dealt with in separate sections. All other areas, including the case acreage, the factory joints, and any other regions requiring a minimum 2.0 safety factor, will be dealt with in the sections devoted to the specific motor segments.

Several axial performance stations previously measured on HPM motors have been moved or eliminated to avoid ply terminations, tapered areas, and other conditions created by the RSRM design. Other locations have been added to provide a more complete database.

Some segment stations had liner material remaining after firing. For analysis purposes, the prefire measurements were used in place of the postfire measurements where liner was remaining, and the MDD was considered to be zero.

Several terms used in this part of the report are defined as follows:

REVISION A	DOC NO.	TWR-17546	VOL	III
<del>-</del>	SEC	PAGE		
FORM TC 7994-310 (REV 2-88)		l	20	



- Safety Factor (ASF): The material decomposition safety factor based on the actual prefire thickness and actual MDD.

  ASF = prefire thickness / MDD.
- Aft Cylinder: That region of the aft segment forward of 55.0 inches from the nozzle boss.
- Aft Dome: That region of the aft segment from the aft face of the nozzle boss to and including 55.0 inches forward of the nozzle boss.
- Compliance Safety Factor (CSF): The material decomposition safety factor based on the MDT and actual MDD. CSF = MDT / MDD.
- Exposure Time (E.T.): That amount of time that a particular station is subjected to the internal motor environment. The time is measured in seconds and determined by ballistic evaluation (Reference 9).
- HPM Database: That set of data derived from static and flight HPM motors and defined in Reference 7.
- HPM Database Maximum MDD: The largest single MDD computed for a given axial station in the HPM database.
- $M + 3\sigma$  MDD: The analytically derived MDD values from the HPM database used as the insulation design basis where:
  - M = the median of the 'within motor' MDD medians
  - $\sigma$  = the root sum square of the 'motor to motor' MDD standard deviation ( $\sigma_{\rm M}$ ) and the median of the 'within motor' standard deviations ( $\sigma_{\rm MED}$ ) Reference 7.

$$\sigma = (\sigma_{M}^{2} + \sigma_{MED}^{2})^{\frac{1}{2}}$$

- Material Decomposition Depth (MDD): The amount of material that is decomposed during firing due to erosion or heat effects measured in inches. MDD = prefire thickness postfire thickness.
- Material Decomposition Rate (MDR): The average rate at which material is decomposed as a result of erosion or heat effect. The value is measured in mils (thousandths of an inch) per second and assumes a constant decomposition rate throughout the exposure time. MDR = 1000 X MDD / E.T.
- Minimum Design Thickness (MDT): The minimum insulation thickness defined on the 1U design drawings. The thicknesses are designed to meet the appropriate safety factor based on an M + 3σ material decomposition and the HPM design thickness (Reference 8).

DOC NO. TWR-17546 | VOL III
SEC | PAGE | 21



Performance Station: An axial location in the segment found by measuring forward from the tang tip (on the forward and center segments) or from the nozzle boss face (on the aft segment). The stations in the forward dome are located by continuing the measurement along the insulation surface contour from the 321.0 inch station. Figure 6 shows the location of the stations within each segment.

### 7.1 RSRM-7A NOZZLE TO CASE JOINT

The 2.0 safety factor region of the nozzle to case joint area is defined as that area 2 inches to either side of the joint insulation interface, measured along the insulation internal surface contour. Safety factors were evaluated by examining the MDDs at two locations: 1) at the base of the joint stress relief flap gap and 2) on the aft dome insulation at the joint interface.

Visual inspection of the flap gap has revealed that no significant heating occurs in this region. In fact, the Teflon tape which is in the gap is visible after firing. For this reason, no further measurements or inspections in the flap gap were necessary.

The MDD at the nozzle to case joint insulation interface was calculated at 16 planes using the prefire and postfire insulation thickness as measured per Figure 7. The MDT used in the CSF calculations at the nozzle to case joint was 4.900 inches based on the MDT at the 7.8 and 9.3 inch stations.

The safety factors for the RSRM-7A nozzle to case joint are shown in Table 7. The minimum CSF for the nozzle to case joint was 4.6 at the 0° plane. The minimum ASF was 5.2 at the 0° plane. The median MDD for the nozzle to case joint was 0.703 inch and ranged from 0.479 to 1.067 inch. The safety factors for the nozzle to case joint exceeded the 2.0 requirement in all areas.

### 7.2 RSRM-7A FIELD JOINTS

The 2.0 safety factor region of the field joint area is defined as that area 2 inches to either side of the joint insulation interface. The joint safety factors were evaluated by examining the MDDs in three areas:

1) in the pressurization gap, 2) at the 3.5 inch station, and 3) at the joint insulation interface.

REVISIONA	DOC NO.	TVR-17546	VOL	III
<del></del>	SEC	PAGE		
FORM TC 7994-310 (REV 2-88)				

22



From a visual inspection of all field joints, it was apparent that no significant material decomposition had occurred in the area of the pressurization gap terminus. For this reason, no further measurements or inspections in the pressurization gaps were necessary.

The safety factor at the 3.5 inch station for each field joint will be dealt with in the discussion of the respective segments.

The safety factors at the joint insulation interface were calculated using the MDD on the clevis joint insulation. The MDD was calculated at 24 planes using the prefire and postfire thicknesses as measured per Figure 8. The MDT used in the CSF calculations was 2.595 inches. This minimum is derived by subtracting the maximum 1U inner clevis leg metal thickness of 0.430 inch from the minimum 1U drawing insulation and case thickness of 3.025 inches.

The clevis side of the joint interface sits approximately 0.150 inch radially inboard of the J-leg tip when the joint is assembled. As a result, the clevis side is exposed to a more severe environment and experiences more material decomposition than the J-leg tip. This tends to inflate the MDD value at the joint. A more realistic approach to calculating the joint safety factors would be to use the tang J-leg insulation. It is not possible, however, to obtain corresponding prefire and postfire measurements because the J-leg does not return to the same position after the joint has been assembled and disassembled. For this reason, the clevis side insulation is used to calculate the joint CSF and ASF and is considered to be quite conservative.

#### 7.2.1 RSRM-7A Aft Field Joint

The safety factors for the RSRM-7A aft field joint insulation interface are shown in Table 8.

The minimum CSF for the joint interface was 5.4 at the 210° plane. The minimum ASF was 5.8, also at the 210° plane. The median MDD for the aft field joint was 0.411 inch and ranged from 0.314 to 0.477 inch. The safety factors for the aft field joint exceeded the 2.0 requirement in all areas.

DOC NO. TWR-17546 VOL III
SEC PAGE
23



### 7.2.2 RSRM-7A Center Field Joint

The safety factors for the RSRM-7A center field joint insulation interface are shown in Table 9.

The minimum CSF for the joint interface was 9.6 at the 90° plane. The minimum ASF was 10.5 at the 90° plane. The median MDD for the center field joint was 0.163 inch and ranged from 0.119 to 0.269 inch. safety factors for the center field joint exceeded the 2.0 requirement in all areas.

### 7.2.3 RSRM-7A Forward Field Joint

The safety factors for the RSRM-7A forward field joint insulation interface are shown in Table 10. The minimum CSF for the interface was 12.7 at the  $166^{\circ}$  and  $180^{\circ}$  planes. The minimum ASF was 13.4, at the  $180^{\circ}$ The median MDD for the forward field joint was 0.165 inch and ranged from 0.078 to 0.204 inch. The safety factors for the forward field joint exceeded the 2.0 safety factor requirement in all areas.

## 7.3 RSRM-7A AFT SEGMENT

For purpose of this analysis, the aft segment is divided into the aft dome region and the aft cylinder region. The aft segment was measured in eight degree planes forward of the 98.0 inch station and at sixteen degree planes at and aft of the 98.0 inch station.

#### 7.3.1 RSRM-7A Aft Dome

The safety factor analysis and the supporting measurement data for the RSRM-7A aft dome are shown in Table 11. All safety factors for the aft dome were acceptable. The minimum CSF was 1.92 at the 18.5 and 19.5 inch stations in the 111.6° plane. The minimum ASF was 2.27 at the 18.5 and 19.5 inch stations in the 111.6° plane.

Figure 9 shows how the RSRM-7A aft dome MDDs compare with the HPM database median MDDs and the M +  $3\sigma$  design MDDs.

The M +  $3\sigma$  design MDD was exceeded at the following aft dome station:

REVISIO	DOC NO.	TWR-17546	AOL III
	SEC	PAGE	
FORM TC 7994-310 (REV 2-88)		1	24



# (All Dimensions in Inches)

STATION	PLANES	HPM MED MDD	HPM MAX MDD	RSRM-7A MED MDD	RSRM-7A MAX MDD	M + 3 σ DES MDD	MIN CSF
17.3	1 of 16	1.027	1.564	1.409	1.802	1.675	1.98
18.5	4 of 16	0.986	1.419	1.331	1.749	1.496	1.92
19.5	1 of 16	0.978	1,352	1.174	1.644	1.617	1.92

The postfire measurement at these locations were retaken and verified. The prefire and postfire measurements at these stations were analyzed, and no apparent problems with the data could be seen. Although the noted maximum MDD at this station exceeded the M +  $3\sigma$  MDD used to design the insulation, the minimum CSF is above the required 1.5 value. This station will be closely monitored in future motors to determine if the measurements indicate a trend.

# 7.3.2 RSRM-7A Aft Cylinder

The safety factor analysis and the supporting measurement data for the RSRM-7A aft cylinder are shown in Table 12. All safety factors for the aft cylinder were acceptable. The minimum CSF was 2.22 at the 145.5 inch station in the 316.8° plane. The minimum ASF was 2.19 at the 145.5 inch station in the 316.8° plane.

The 56.0, 177.7, and 299.1 inch stations are located in regions which require a 2.0 safety factor. The minimum CSFs at these stations were 3.33, 2.54, and 2.99, respectively. The minimum ASFs were 4.12, 3.82, and 4.54, respectively.

Figure 10 shows how the RSRM-7A aft cylinder MDDs compare with the HPM database median MDDs and the M +  $3\sigma$  design MDDs. The M +  $3\sigma$  design MDD was not exceeded at any station.

Station 56.0 at the 158.4 degree plane had a very high postfire measurement that resulted in a 0 MDD. This is believed to be due to a measurement error.



## 7.4 RSRM-7A AFT CENTER SEGMENT

The aft center segment was measured at eight degree planes. The safety factor analysis and the supporting measurement data for the RSRM-7A aft center segment are shown in Table 13. All safety factors for the aft center segment were acceptable. The minimum CSF was 2.43 at the 71.5 inch station in the 316° plane, and the minimum ASF was 2.60 at the 30.7 inch station in the 316° plane.

The 3.5 and 161.4 inch stations are located in regions which require a 2.0 safety factor. The minimum CSFs were 3.48 and 3.58, respectively. The minimum ASFs were 4.41 and 9.70, respectively.

Figure 11 shows how the RSRM-7A aft center segment MDDs compare with the HPM database median MDDs and the M +  $3\sigma$  design MDDs.

The M +  $3\sigma$  design MDD was not exceeded at any station.

One plane at the 39.7 inch station and one plane at the 71.5 had a postfire measurement that was higher than the surrounding postfire data. All prefire data at these stations was comparable. These resulted in a 0 MDD. This could indicate the prefire measurements and the postfire measurements were taken in different locations or that data was improperly measured or recorded.

# 7.5 RSRM-7A FORWARD CENTER SEGMENT

The forward center segment was measured at eight degree planes. The safety factor analysis and the supporting measurement data for the RSRM-7A forward center segment are shown in Table 14. All safety factors for the forward center segment were acceptable. The minimum CSF was 2.81 at the 39.7 inch station in the 316° plane, and the minimum ASF was 4.38 at the 214.1 inch station in the 270° plane.

The 3.5 and the 161.4 inch stations are located in regions which require a 2.0 safety factor. The minimum CSFs were 10.34 and 3.15, respectively. The minimum ASFs were 12.60 and 7.83, respectively.

Figure 12 shows how the RSRM-7A forward center segment MDDs compare with the HPM database median MDDs and the M +  $3\sigma$  design MDDs.

The M +  $3\sigma$  design MDD was exceeded at the following forward center segment station:



# (All Dimensions in Inches)

STATION	PLANES	HPM MED MDD	HPM MAX MDD	RSRM-7A MED MDD	RSRM-7A MAX MDD	M + 3 σ DES MDD	
214	1 of 16	0	0.026	0	0.032	0.029	4.06

The postfire measurements at this location was retaken and verified. No unusual conditions were noted in either the prefire or postfire data. Although the noted maximum MDD at this station exceeded the M +  $3\sigma$  used to design the insulation, the minimum CSF is well above the required 1.5 value.

### 7.6 RSRM-7A FORWARD SEGMENT

The forward segment performance data was separated into two groups: the star tip and non-star tip planes. The star tip planes are defined as the 90°, 154°, 222°, 286°, and 352° planes which lie under the thin portion of the propellant grain. These planes have a higher exposure time than the non-star tip planes. The non-star tip planes are defined as the 74°, 140°, 206°, 270°, and 336° planes. These planes lie under the thick parts of the forward segment propellant grain.

### 7.6.1 RSRM-7A Forward Segment Star Tip Planes

The safety factor analysis and the supporting measurement data for the RSRM-7A forward segment star tip planes are shown in Table 15. All safety factors for the forward segment star tip planes were acceptable. The minimum CSF was 1.71 at the 280.0 inch station in the 222° plane, and the minimum ASF was 2.14 also at the 280.0 inch station in the 222° plane.

The 3.5, 162.0, and 321.0 inch stations are located in areas which require a 2.0 safety factor. The minimum CSFs at these stations were 13.01, 3.06, and 3.15, respectively. The minimum ASFs for these stations were 16.21, 4.40, and 3.43, respectively.

Figure 13 shows how the RSRM-7A forward segment star tip MDDs compare with the HPM database median MDDs and the M +  $3\sigma$  design MDDs.

The  $M+3\sigma$  design MDD was exceeded at the following forward segment star tip station:

REVISION	DOC NO.	TWR-17546	AOF III
<del></del>	SEC	PAGE	
FORM TC 7994-310 (REV 2-88)			



# (All Dimensions in Inches)

STATION	PLANES	HPM MED MDD	HPM MAX MDD	RSRM-7A MED MDD	RSRM-7A MAX MDD	M + 3 σ DES MDD	
3.5	4 of 5	0*	0*	0.141	0.163	0.103	13.01

<sup>\*</sup> Data taken from closest adjacent station.

The MDD at the 3.5 inch station was higher than that experienced in the HPM motors. This condition, however, has been noted on all previous RSRMs and is not unexpected. Even with the increased MDD values, the minimum CSF noted at this station was 13.01. This condition will continue to be monitored on future motors.

# 7.6.2 RSRM-7A Forward Segment Non-Star Tip Planes

The safety factor analysis and the supporting measurement data for the RSRM-7A forward segment non-star tip planes are shown in Table 16. All safety factors for the forward segment non-star area were acceptable. The minimum CSF was 2.05 at the 305.0 inch station in the 206° plane, and the minimum ASF was 2.45 at the 383.0 inch station in the 206° plane.

The 3.5, 162.0, and 321.0 inch stations are in areas which require a 2.0 safety factor. The minimum CSFs at these stations were 9.72, 5.58, and 6.75, respectively. The minimum ASFs were 12.09, 7.59, and 7.29, respectively.

Figure 14 shows how the RSRM-7A forward segment non-star tip MDDs compare with the HPM database median MDDs and the M +  $3\sigma$  design MDDs.

The M +  $3\sigma$  design MDD was exceeded at the following forward segment non-star tip station:

### (All Dimensions in Inches)

STATION	PLANES	HPM MED MDD	HPM MAX MDD	RSRM-7A MED MDD	RSRM-7A MAX MDD	M + 3 σ DES MDD	
3.5	4 of 5	0*	0*	0.129	0.218	0.103	9.72

<sup>\*</sup> Data taken from closest adjacent station.

DOC NO.	TWR-17546	VOL	III
SEC	PAGE		



As in the star tip, the MDD at the 3.5 inch station was higher than that experienced in the HPM motors. This condition, however, has been noted on all previous RSRMs and is not unexpected. Even with the increased MDD values, the minimum CSF noted at this station was 9.72. This condition will continue to be monitored on future motors.

One plane at the 321.0 inch station had a postfire measurement that was higher than the surrounding postfire data with comparable prefire data. This resulted in a 0 MDD. This could indicate the prefire measurements and the postfire measurements were taken in different locations or that the data was improperly measured or recorded.

# 8.0 RSRM-7B VISUAL EVALUATIONS

The condition of the RSRM-7B insulation components is discussed in the following subsections. A copy of the inspection documentation can be found in Appendix B.

#### 8.1 RSRM-7B EXTERNAL INSULATION

# 8.1.1 RSRM-7B Factory Joint Weatherseals

The condition of the factory joint weatherseals is recorded in Tables B-1 through B-7. No water was noted under any of the RSRM-7B weatherseals as was evident by the lack of any corrosion when the weatherseals were removed. No significant areas of missing EPDM insulation were noted on any factory joint weatherseal. One debris hit area was noted on the aft edge of the forward center segment weatherseal. The missing material was located near 270° and measured approximately 2 inches circumferentially by 1 inch longitudinally. The debris was most likely from nozzle severance.

The weatherseals on all three aft segment factory joints were slightly heat affected generally from 220°-270°-320° due to the plume radiation from the solid rockets motor and shuttle main engines. The heaviest heat effects occurred near 270°. This is a normal occurrence that had no effect on the performance of the weatherseals.

Two insulation to case unbonds were identified on the forward edge of the RSRM-7B forward segment cylinder to cylinder weatherseal. The weatherseal was unbonded centered at 160° for 14 inches to a depth

29



ranging from 1.0 to 1.5 inches. The paint was also peeled and missing in two areas forward of the weatherseal. The occurrences measured 2.4 inches longitudinally by 5 inches circumferentially and 3.25 inches longitudinally by 7 inches circumferentially. The forward edge of the weatherseal was also unbonded centered at 135° for 11 inches to a depth of 0.1 inch. An aft edge unbond was noted at 210° and measured 0.6 inch longitudinally by approximately 1 inch circumferentially. All unbonds were at the Chemlok 205 to case interface.

Research of the manufacturing logs for the RSRM-7 factory joint weatherseals revealed that the Conscan readings for the RSRM-7B forward segment cylinder to cylinder weatherseal were above current planning requirements. The results of the swab sample taken in the unbond at KSC revealed no measurable contamination.

As was discussed on the RSRM-7A motor, a team has been established to evaluate the occurrence of weatherseal unbonds.

The remainder of the RSRM-7B weatherseals were in excellent condition.

# 8.1.2 RSRM-7B Stiffener Stub and Rings

The condition of the insulation over the forward stiffener stub and the stiffener rings is recorded in Tables B-8 through B-11. The insulation was in good condition with normal heat effects and discoloration on all surfaces. The heaviest heat effects occurred from 220°-270°-320° due to the plume radiation from the solid rocket motors and shuttle main engines. No visible damage to any stiffener ring insulation was noted. This was due to the high sea state at the time of booster splashdown. Some insulation unbonds were noted on the end of the ring segments after removal from the case. These unbonds were a result of the hydrolazing process. The K5NA repair on the outboard edge of the forward stiffener stub showed normal erosion and some small missing chunks intermittently around the circumference.



REVISIONA

FORM TC 7994-310

## 8.2 RSRM-7B NOZZLE TO CASE JOINT

The nozzle to case joint insulation condition is recorded in Table B-12 and B-13. The nozzle to case joint performed as expected with no polysulfide blowholes identified across the bondline. No voids in the polysulfide were identified. Slight polysulfide porosity was evident in the step region full circumference.

The failure mode of the polysulfide bondline at disassembly was approximately 89% cohesive within the polysulfide, 10% adhesive at the NBR to polysulfide interface, and 1% adhesive at the phenolic to polysulfide interface. The high amount of cohesive failure and the thickness of the polysulfide char on the phenolic at the joint entrance resulted in some slight disassembly damage to the joint stress relief flap. The flap appeared to have been folded over backwards upon itself at the baffle non-bonded areas as the nozzle was removed. The flap then returned to its normal position. This was evident by the scrape marks at the forward edge of the flap coinciding with many of the baffle non-bonded locations. It was also evident on the polysulfide forward of the wiper 0-ring where the decomposed polysulfide from the tip of the flap was folded over and had made contact leaving a black mark.

The baffle, which had been bonded back in place as a result of a prefire discrepancy, was still securely bonded at the proper locations.

The vent slots showed an average polysulfide fill of 84% with values ranging from 30% to 100% fill. The vent slot fill was the highest percentage seen to date on any motor.

The bondline around the circumference demonstrated erosion similar to that observed on previous RSRM motors. The polysulfide was decomposed further into the joint than the flap erosion. For approximately 0.40 inch aft of the erosion, the polysulfide was partially decomposed and bubbled. Although the material was partially decomposed, no gas flow occurred in the adhesive bondline decomposed region.

The insulation erosion in the joint region was similar to the condition of previous RSRM flight motors. The NBR flap and baffle appeared to be in excellent shape with normal heat effects and erosion.

	DOC NO.	TWR-17546	VOL	III
	SEC	PAGE		
(REV 2-88)		I	31	



## 8.3 RSRM-7B FIELD JOINTS

### 8.3.1 RSRM-7B Aft Field Joint

The joint insulation configuration performed as designed. The joint insulation surfaces exhibited normal charring and erosion. Measurements of the tang material char depths and bondline contact are provided in Table B-14.

The general appearance of the pressure sensitive adhesive was noted. Contact and non-contact within the joint was based on the flat appearance and matted texture, or the glossy appearance of the adhesive. The joint appeared to have made contact full circumference at the tip of the J-leg. The bondline contact was measured at 0°, 90°, 180°, and 270°. The average contact was 0.96 inch.

No evidence of motor chamber gas leakage to the 0-rings or past the J-joint insulation was identified. Wet sooting extending down the bondline was identified intermittently around the circumference ranging from a depth of 0.20 to 0.70 inch outboard of the remaining material. A maximum condition of 0.90 inch was noted between 176° and 182°. Wet sooting is believed to occur during motor re-entry or splashdown when the joint may flex and allow soot into the bondline.

Two areas which appeared similar to wet sooting were noted at 246°-254° and 286°-296°. These areas had smudge marks within the black area. It was later determined that charred material had been deposited on the bondline as the joint was separated, and the water flowed out. Someone had then attempted to wipe off the charred material causing the smudge marks. This area was solvent cleaned after the evaluation to insure that no heat effects were present.

Tape adhesive residue was noted intermittently on the clevis insulation surfaces and had no effect on the joint.

Cracks and crazing were noted on the clevis insulation in the radius region at  $0^{\circ}$ ,  $10^{\circ}-14^{\circ}$ ,  $35^{\circ}-42^{\circ}$ ,  $52^{\circ}$ ,  $82^{\circ}-100^{\circ}$ ,  $165^{\circ}$ ,  $224^{\circ}$ , and  $338^{\circ}-342^{\circ}$ . The cracks had no adverse effect on the performance of the joint.

No clevis or tang edge separations were identified at KSC. During inspection at Clearfield H-7, no recordable (over 0.10 inch deep) clevis edge separations were identified. Tang edge separations were visible on the aft field joint. The tang insulation edge separations were probed

REVISION DOC NO. TWR-17546 VOL III
SEC PAGE

FORM TC 7994-310 (REV 2-88)



during postflight inspection at Clearfield H-7. The deepest postfire tang edge separation had a depth of 0.25 inch, as compared with no prefire separation. These separations are documented in Tables 5 and 6.

# 8.3.2 RSRM-7B Center Field Joint

The joint insulation configuration performed as designed. The joint insulation surfaces exhibited normal charring and erosion. Measurements of the tang material char depths and bondline contact are provided in Table B-15.

The general appearance of the pressure sensitive adhesive was noted. Contact and non-contact within the joint was based on the flat appearance and matted texture, or the glossy appearance of the adhesive. The joint appeared to have made contact full circumference at the tip of the J-leg. The bondline contact was measured at 0°, 90°, 180°, and 270°. The average contact was 1.14 inches.

No evidence of motor chamber gas leakage to the 0-rings or past the J-joint insulation was identified. Wet sooting into the joint bondline ranged from 0.30 to 0.70 inch outboard from the remaining material. A maximum condition of 1.35 inches was noted from 166°-182°. This area was solvent cleaned after the evaluation, and no heat effects were noted.

Cracks and crazing were noted on the clevis insulation in the radius region intermittently from  $30^{\circ}-180^{\circ}-250^{\circ}$ . The cracks had no adverse effect on the performance of the joint.

Repair adhesive from a prefire clevis insulation separation repair was noted on the insulation 2.1 inches aft of the clevis tip at 260°, 265°, 292°, 295°, 296°, and 298°. The adhesive did not extend into the bonding region of the joint and did not affect the function of the joint. Evaluation of the segment logs indicates that the edge separation repair was performed at Thiokol before shipment to KSC.

No clevis or tang edge separations were identified at KSC. During inspection at Clearfield H-7, no recordable (over 0.10 inch deep) clevis edge separations were identified. Tang edge separations were visible on the center field joint. The tang insulation edge separations were probed during postflight inspection at Clearfield H-7. The deepest postfire

REVISIO#	DOC NO. TWR-17546		NOT III	
FORM TC 7994-310 (REV 2-88)	SEC	PAGE	33	



tang edge separation had a depth of 0.05 inch, as compared with a prefire separation of 0.03 inch. These separations are documented in Tables 5 and 6.

# 8.3.3 RSRM-7B Forward Field Joint

The joint insulation configuration performed as designed. The joint insulation surfaces exhibited normal charring and erosion. Measurements of the tang material char depths and bondline contact are provided in Table B-16.

The general appearance of the pressure sensitive adhesive was noted. The joint appeared to have made contact full circumference at the tip of the J-leg. The contact area appeared flat with a matted texture. The bondline contact was measured at 0°, 90°, 180°, and 270°. The average contact was 1.11 inches.

No evidence of motor chamber gas leakage to the O-rings or past the J-joint insulation was identified. Wet sooting into the joint bondline ranged from 0.30 to 0.50 inch outboard from the remaining material.

Tape adhesive residue was noted intermittently on the clevis insulation surfaces and had no effect on the joint.

Cracks and crazing were noted on the clevis insulation in the radius region intermittently from 300°-0°-220°. Cracks on this segment had previously been noted on a PR. The cracks had no adverse effect on the performance of the joint.

No clevis or tang edge separations were identified at KSC. During inspection at Clearfield H-7, no recordable (over 0.10 inch deep) clevis or tang edge separations were identified on the forward field joint. This is documented in Tables 5 and 6.

#### 8.4 RSRM-7B IGNITER JOINTS AND INSULATION

The condition of the igniter to case joint insulation is recorded in Tables B-17 through B-20. The condition of the igniter boss insulation was excellent. An evaluation of the insulation to case interface revealed no edge separations. There was loose flashing on the igniter

REVISION .	DOC NO.	TWR-17546	AOF III
FORM TC 7994-310 (REV 2-88)	SEC	PAGE	34



boss to a maximum depth of 0.075 inch intermittently between 200°-270°-20°. This is a fairly typical condition. The boss molded insulation surface was in good condition with normal erosion on the inboard surface.

The overall condition of the putty in the igniter to case joint was good. The color of the putty was a consistent light olive green. The putty exhibited 100% cohesive failure and nominal tack for the full circumference. There were no blowholes present, however, putty was extruded up to the adapter full circumference and onto the aft face of the adapter intermittently around the circumference. A map of the putty condition is shown in Figure 15.

The condition of the putty in the adapter to chamber joint was good. The color of the putty was a consistent light olive green. The putty exhibited 100% cohesive failure and nominal tack for the full circumference. A blowhole through the putty was noted at 340°. The gas path measured 0.53 inch at the aft edge and 0.50 inch at the forward edge. Soot was in the putty from 315° to 350° but did not extend to the gasket. No adverse effects on the performance of the joint resulted from the blowhole.

The igniter internal and external insulation was in normal condition. No areas of blistering or abnormal erosion were present.

### 8.5 RSRM-7B ACREAGE INSULATION

# 8.5.1 RSRM-7B Aft Segment Acreage Insulation

The aft segment internal insulation was in excellent condition and is recorded in Tables B-21 through B-23.

The forward facing NBR inhibitor stub exhibited scalloped erosion intermittently around the circumference. These areas had a very short inhibitor stub with intermittent inhibitor pieces taller than adjacent areas. A similar condition has been noted on all previous RSRM flight aft segments. Measurements of the remaining inhibitor stub were taken every 30° and are contained in Table B-22. The inhibitor height ranged from 3.5 to 9.0 inches. Although the erosion was uneven, the remaining inhibitor stub heights for this segment were within the expected

REVISIO	DOC NO.	TWR-17546	VOL III
- <del>-</del>	SEC	PAGE	
FORM TC 7994-310 (REV 2-88)			



tolerance band for past flight motors based on a statistical analysis of the historical database (Reference 5). There were no inhibitor tears greater than 3 inches in length noted on this inhibitor.

The segment had no liner remaining. This condition is common for an aft segment.

The erosion in the aft dome was similar to past flight motors. NBR under the CF/EPDM was exposed intermittently in the area roughly 15 to 20 inches forward of the nozzle boss. This is a common condition in the aft dome. No blisters were identified in the CF/EPDM in the aft dome. One area, located at 215° and approximately 15 inches forward of the nozzle boss, initially appeared to be a blister. The area was 3.1 inches circumferentially by 2.7 inches long and was triangular in shape. The peeled up area was approximately 0.05 inch thick. The back side of the remaining material did not exhibit the cross-hatched pattern that was seen on blisters. Instead, it had straight line parallel marks about 0.25 inch apart. It is the opinion of Thermal Insulation Design that this condition was a cut caused by splashdown debris.

Scratches and scuff marks from splashdown debris were noted between  $0^{\circ}-45^{\circ}$  from the aft dome factory joint to the NBR inhibitor.

The aft segment acreage insulation was in normal condition. There were no other gouges, separations, cuts, missing material, excessive erosion, or areas of blisters.

## 8.5.2 RSRM-7B Aft Center Segment Acreage Insulation

The aft center segment internal insulation condition is recorded in Tables B-24 through B-27.

The forward facing NBR inhibitor stub exhibited uniform erosion full circumference. Measurements of the remaining NBR inhibitor stub were taken every 30° and are contained in Table B-25. The inhibitor stub heights ranged from 11.0 to 15.0 inches for this segment, which is within the expected tolerance band.

Two radial tears greater than 3 inches long were noted. The longest tear measured 4.5 inches long and extended radially outward to approximately 10.0 inches inboard of the clevis I.D. surface. The edges

REVISION	DOC NO.	TWR-17546	VOL III
<u> </u>	SEC	PAGE	
FORM TC 7994-310 (REV 2-88)		1	36



of the tears demonstrated no material loss or erosion. This indicated that the tears occurred after motor burn. The location and length of the tears are shown in Table B-26.

Liner coverage in the aft center segment was heavy near the clevis end and generally missing aft of the factory joint. The diagram of the liner pattern is shown in Figure 16.

The condition of the flap region is recorded in Table B-27. The castable inhibitor was completely missing full circumference, and the stress relief flap was eroded back to the flap bulb full circumference. Both of these conditions are typical of an aft center segment. The CF/EPDM under the flap was missing full circumference, and the NBR underneath it was heat affected and slightly eroded.

Scratches and scuff marks from splashdown debris were noted between  $0^{\circ}-30^{\circ}$  the full length of the segment. No other evidence of blisters, separations, gouges, cuts, missing material, or excessive erosion was identified.

# 8.5.3 RSRM-7B Forward Center Segment Acreage Insulation

The condition of forward center segment internal insulation is recorded in Tables B-28 through B-31.

The forward facing NBR inhibitor stub exhibited uniform erosion full circumference. Measurements of the remaining NBR inhibitor were taken every 30° and are contained in Table B-29. The inhibitor stub heights for this segment ranged from 24.0 to 27.5 inches, which is within the expected tolerance band.

Eight radial tears greater than 3 inches long were noted. The longest tear was 11.5 inches and extended radially outward to approximately 13.5 inches inboard of the clevis I.D. surface. The edges of the tears demonstrated no material loss or erosion. This indicated that the tears occurred after motor burn. The location and length of the tears are contained in Table B-30. The tears are believed to be a result of re-entry or splashdown loads. The radial extent and frequency of the tears identified in the inhibitor stubs on all the RSRM-7 segments were within the range of tears noted on past flight motors.

REVISION	DOC NO.	TWR-17546	NOT III
	SEC	PAGE	
FORM TC 7994-310 (REV 2-88)		l	37



Liner coverage for the forward center segment was heavy near the clevis end and mostly missing aft of the factory joint. Small patches of thin liner were present intermittently on the insulation over the factory joint. The diagram of the liner pattern is shown in Figure 17.

The castable inhibitor was completely missing full circumference which is typical of a forward center segment. The end of the stress relief flap measured from 6.5 to 11.25 inches forward of the tip of the tang. Axial measurements were taken every 90° and are shown in Table B-31. There were no flap tears noted. The CF/EPDM under the flap was present, heat affected, and slightly eroded full circumference. There were a number of small blisters noted intermittently in the CF/EPDM; none were opened. These appeared to be the result of normal heat effects.

Scratches and scuff marks from splashdown debris were noted between 350°-355°-0° the full length of the segment. No other evidence of blisters, separations, gouges, cuts, missing material, or excessive erosion was identified.

# 8.5.4 RSRM-7B Forward Segment Acreage Insulation

The condition of forward segment internal insulation is recorded in Tables B-32 and B-33.

The eleven point star pattern in the liner was easily distinguishable, and the star and non-star liner termination points were comparable to past flight motors, as shown in Figure 18. The liner remaining under the star tip regions was present from the tip of the tang forward to 145.7 inches. The liner remaining under the non-star tip was present from the tip of the tang forward to 152.0 inches. The liner was light between the tip of the tang and the flap bulb.

The castable inhibitor was completely missing full circumference. The end of the stress relief flap measured from 3.5 (full length remaining) to 11.0 inches forward of the tip of the tang. Axial measurements were taken every 90° and are shown in Table B-33. The NBR under the flap was heat affected as has been seen on all previous RSRM forward segments.

Dissection and evaluation of the RSRM-7B igniter boss forward dome samples were completed. Thickness measurements, void mapping, and

PAGE

FORM TC 7994-310 (REV 2-88)

DOC NO. TWR-17546 VOL III

SEC PAGE

38



photographs of the samples were done. Inspection Engineering showed there were a few small voids (typically 0.10 inch with 0.17 inch maximum diameter) and also some small folds at the case surface. The average remaining insulation thickness (postfire) in the 5 inch to 7.5 inch distance from the igniter boss was 0.414 inch. The minimum remaining insulation thickness was 0.300 inch.

No evidence of blisters, separations, gouges, cuts, missing material, or excessive erosion was identified.

Table B-34 contains a list of all photographs taken of the RSRM-7B insulation.

## 8.6 POSTFIRE EVALUATION OF RSRM-7B PREFIRE DISCREPANCIES

The prefire discrepancy reports for the RSRM-7B insulation were evaluated prior to launch to identify significant items. These are identified in References 3 and 4, and the postfire conditions are discussed below.

Cuts, depressions, and missing material were noted on the nozzle boss insulation bonding surface. Also, the baffle to CF/EPDM interface was torn loose and repaired at several locations. The condition was the result of a prefire nozzle removal operation. The discrepancies were documented on DR 155269-01 and -02. Postfire evaluation of this condition indicated that the surface irregularities had no effect on the function of the nozzle to case joint. The conditions in the bonding area were filled with polysulfide adhesive at joint assembly. The repair to the baffle remained intact, and had no effect on the function of the joint.

Cracks existed in the forward center segment J-joint clevis insulation. The worst case was 31 inches circumferentially by 0.075 inch deep as noted on PR PV6-138717. The cracks were evaluated, and no effects on the function of the joint were noted.

A void was noted in the insulation in the igniter boss region. The discrepancy was documented on DR 161280-01. The insulation in this region was removed for further evaluation. No indications of voids were found at the insulation to case surface. Dissection and evaluation of

REVISIOR
CODM TO 7004 340 (DEV 2 00)

DOC NO.	TWR-17546		VOL	III
SEC	P	AGE		



the RSRM-7B igniter boss forward dome samples was completed. Thickness measurements, void mapping, and photographs of the samples were done as described in Section 8.5.4.

Thin insulation was noted on the igniter boot. The thinnest condition measured 0.085 inch at 315° per DR 164857-01. The igniter boot was completely burned away during normal motor operation, and no abnormal conditions were noted.

# 9.0 RSRM-7B INSULATION PERFORMANCE EVALUATION

The RSRM-7B segments were insulated to meet the RSRM design drawing requirements. The performance analysis on the RSRM-7B motor was conducted in the same manner as previously explained for the RSRM-7A motor.

### 9.1 RSRM-7B NOZZLE TO CASE JOINT

The safety factors for the nozzle to case joint are shown in Table 17. The minimum CSF for the nozzle to case joint was 4.0 at the 0° plane. The minimum ASF was 4.5, also at the 0° plane. The median MDD for the nozzle to case joint was 0.802 inch and ranged from 0.359 to 1.234 inch. The safety factors for the nozzle to case joint exceeded the 2.0 requirement in all areas.

#### 9.2 RSRM-7B FIELD JOINTS

### 9.2.1 RSRM-7B Aft Field Joint

The safety factors for the RSRM-7B aft field joint insulation interface are shown in Table 18. The minimum CSF for the joint interface was 5.1 at the 120° plane. The minimum ASF was 5.4, also at the 120° plane. The median MDD for the aft field joint was 0.444 inch and ranged from 0.394 to 0.513 inch. The safety factors for the aft field joint exceeded the 2.0 requirement in all areas.

REVISION	
FORM TC 7994-310 (REV 2-88)	

DOC NO.	DC NO. TWR-17546	VOL	III	
SEC		PAGE		



### 9.2.2 RSRM-7B Center Field Joint

The safety factors for the RSRM-7B center field joint insulation interface are shown in Table 19. The minimum CSF for the joint interface was 11.4 at the 136° plane. The minimum ASF was 12.1, also at the 136° plane. The median MDD for the center field joint was 0.191 inch and ranged from 0.136 to 0.227 inch. The safety factors for the center field joint exceeded the 2.0 requirement in all areas.

## 9.2.3 RSRM-7B Forward Field Joint

The safety factors for the RSRM-7B forward field joint insulation interface are shown in Table 20. The minimum CSF for the interface was 11.6 at the 136° plane. The minimum ASF was 12.4 also at the 136° plane. The median MDD for the forward field joint was 0.137 inch and ranged from 0.111 to 0.223 inch. The safety factors for the forward field joint exceeded the 2.0 safety factor requirement in all areas.

#### 9.3 RSRM-7B AFT SEGMENT

### 9.3.1 RSRM-7B Aft Dome

The safety factor analysis and the supporting measurement data for the RSRM-7B aft dome are shown in Table 21. All safety factors for the aft dome were acceptable. The minimum CSF was 1.84 at the 17.3 inch station in the 248.4° plane. The minimum ASF was 2.02 at the 16.0 inch station in the 248.4° plane.

Figure 19 shows how the RSRM-7B aft dome MDDs compare with the HPM database median MDDs and the M + 3 $\sigma$  design MDDs.

The M +  $3\sigma$  design MDDs were exceeded at the following aft dome stations:

# (All Dimensions in Inches)

STATION	PLANES	HPM MED MDD	HPM MAX MDD	RSRM-7B MED MDD	RSRM-7B MAX MDD	M + 3 σ DES MDD	MIN CSF
16.0	1 of 16	1.191	1.783	1.580	2.023	1.980	1.87
17.3	3 of 16	1.027	1.564	1.553	1.937	1.675	1.84
18.5	6 of 16	0.986	1.419	1.453	1.728	1.496	1.94

DOC NO.	TWR-17546		VOL	III
SEC		PAGE		



The postfire measurements at these locations were retaken and verified. Although the noted maximum MDD at these stations exceeded the M +  $3\sigma$  used to design the insulation, the minimum CSF is above the required 1.5 value.

# 9.3.2 RSRM-7B Aft Cylinder

The safety factor analysis and the supporting measurement data for the RSRM-7B aft cylinder are shown in Table 22. All safety factors for the aft cylinder were acceptable. The minimum CSF was 2.04 at the 145.5 inch station in the 316.8° plane. The minimum ASF was also 2.04 at the 145.5 inch station in the 316.8° plane.

The 56.0, 177.7, and 299.1 inch stations are located in regions which require a 2.0 safety factor. The minimum CSFs at these stations were 2.93, 2.34, and 2.85, respectively. The minimum ASFs were 3.66, 3.60, and 4.53, respectively.

Figure 20 shows how the RSRM-7B aft cylinder MDDs compare with the HPM database median MDDs and the M + 3 $\sigma$  design MDDs.

The M +  $3\sigma$  design MDD was not exceeded at any aft cylinder station.

### 9.4 RSRM-7B AFT CENTER SEGMENT

The aft center segment was measured at eight degree planes. The safety factor analysis and the supporting measurement data for the RSRM-7B aft center segment are shown in Table 23. All safety factors for the aft center segment were acceptable. The minimum CSF was 1.99 at the 11.0 inch station in the 180° plane, and the minimum ASF was 2.44 at the 30.7 inch station in the 46° plane.

The 3.5 and 161.4 inch stations are located in a region which requires a 2.0 safety factor. The minimum CSFs were 2.58 and 3.23, respectively. The minimum ASFs were 3.58 and 8.60, respectively.

Figure 21 shows how the RSRM-7B aft center segment MDDs compare with the HPM database median MDDs and the M +  $3\sigma$  design MDDs.

The M +  $3\sigma$  design MDDs were exceeded at the following aft center segment stations:

REVISION A	DOC NO.	TWR-17546	VOL	III
FORM TC 7994-310 (REV 2-88)	SEC	PAGE	4.2	
			42	



(All Dim	ensions	in	Inches)	)
----------	---------	----	---------	---

STATION	PLANES	HPM MED MDD	HPM MAX MDD	RSRM-7B MED MDD	RSRM-7B MAX MDD	M + 3 σ DES MDD	MIN CSF
11.0	8 of 8	0.451*	0.763*	0.885	0.956	0.829	1.99
44.6	3 of 8	0.026	0.141	0.089	0.098	0.090	3.67
48.0	3 of 8	0.045*	0.206*	0.082	0.096	0.089	3.00

# \* Data taken from closest adjacent station.

The prefire and postfire measurements at these stations were analyzed, and no apparent problems with the data could be seen. Evaluation of the RSRM database trend charts indicated that the prefire measurements at these stations for this segment are at the high end of the RSRM database. Although the noted maximum MDDs at these stations exceeded the M +  $3\sigma$  MDDs used to design the insulation, the minimum CSFs are above the required 1.5 value. These stations will be closely monitored in future motors to determine if the measurements indicate a trend.

## 9.5 RSRM-7B FORWARD CENTER SEGMENT

The safety factor analysis and the supporting measurement data for the RSRM-7B forward center segment are shown in Table 24. All safety factors for the forward center segment were acceptable. The minimum CSF was 3.32 at the 161.4 inch station in the 0° plane, and the minimum ASF was 4.15, at the 126.0 inch station in the 46° plane.

The 3.5 and 161.4 inch stations are located in regions which require a 2.0 safety factor. The minimum CSFs were 13.86 and 3.32, respectively. The minimum ASFs were 16.46 and 8.85, respectively.

Figure 22 shows how the RSRM-7B forward center segment MDDs compare with the HPM database median MDDs and the M +  $3\sigma$  design MDDs.

The M +  $3\sigma$  design MDD was not exceeded at any forward center segment station.

#### 9.6 RSRM-7B FORWARD SEGMENT

# 9.6.1 RSRM-7B Forward Segment Star Tip Planes

The safety factor analysis and the supporting measurement data for the RSRM-7B forward segment star tip planes are shown in Table 25. All safety factors for the forward segment star tip area were acceptable.

REVISION	DOC NO.	DOC NO. TWR-17546	
	SEC	PAGE	
FORM TC 7994-310 (REV 2.88)			



The minimum CSF was 1.76 at the 394.0 inch station in the 222° plane, and the minimum ASF was 2.31 also at the 394.0 inch station in the 222° plane.

The 3.5, 162.0, and 321.0 inch stations are located in areas which require a 2.0 safety factor. The minimum CSFs at these stations were 22.55, 2.42, and 4.06, respectively. The minimum ASFs for these stations were 26.54, 3.80, and 4.55, respectively.

Figure 23 shows how the RSRM-7B forward segment star tip MDDs compare with the HPM database median MDDs and the M +  $3\sigma$  design MDDs.

The M +  $3\sigma$  design MDD was exceeded at the following forward segment star tip station:

# (All Dimensions in Inches)

STATION	PLANES	HPM MED MDD	HPM MAX MDD	RSRM-7B MED MDD	RSRM-7B MAX MDD	M + 3 σ DES MDD	
13.0	5 of 5	0*	0*	0.172	0.214	0.101	3.04

<sup>\*</sup> Data taken from the closest adjacent station

The MDD at the 13.0 inch station was higher than that experienced in the HPM motors. This condition, however, has been noted on all previous RSRMs and is not unexpected. Even with the increased MDD values, the maximum CSF for station 13.0 was 3.04. This condition will continue to be monitored on future motors.

# 9.6.2 RSRM-7B Forward Segment Non-Star Tip Planes

The safety factor analysis and the supporting measurement data for the RSRM-7B forward segment non-star tip planes are shown in Table 26. All safety factors for the forward segment non-star tip area were acceptable. The minimum CSF was 1.93 at the 383.0 inch station in the 74° plane, and the minimum ASF was 2.36 also at the 383.0 inch station in the 74° plane.

The 3.5, 162.0, and 321.0 inch stations are in areas which require a 2.0 safety factor. The minimum CSFs at these stations were 18.93, 2.79, and 5.77, respectively. The minimum ASFs were 21.91, 4.53, and 6.26, respectively.

REVISION	DOC NO.	TWR-17546	VOL	III
	SEC	PAGE		
FORM TC 7994-310 (REV 2-88)			44	



Figure 24 shows how the RSRM-7B forward segment non-star tip MDDs compare with the HPM database median MDDs and the M +  $3\sigma$  design MDDs.

The M +  $3\sigma$  design MDDs were exceeded at the following forward segment non-star tip stations:

(All Dimensions in Inches)

STATION	PLANES	HPM MED MDD	HPM MAX MDD	RSRM-7B MED MDD	RSRM-7B MAX MDD	M + 3 $\sigma$ DES MDD	
3.5	1 of 5	0*	0*	0.070	0.112	0.103	18.93
13.0	4 of 5	0*	0*	0.155	0.250	0.101	2.60

<sup>\*</sup> Data taken from the closest adjacent station

The MDDs at the 3.5 and 13.0 inch stations were higher than that experienced in the HPM motors. This condition, however, has been noted on all previous RSRMs and is not unexpected. Even with the increased MDD values, the maximum CSFs were 18.93 and 2.60, respectively. This condition will continue to be monitored on future motors.

REVISIO#	DOC NO.	TWR-1
	SEC	
FORM TC 7994-310 (REV 2-98)		

45



### REFERENCES

- 1. TWR-50050 Vol. I Book 1 Rev. A, 'KSC Postflight Engineering Evaluation Plan (Internal and External Insulation)', L. E. MacCauley, 21 November 1989.
- 2. TWR-16475 Vol. III Book 2 Rev. C, 'Clearfield Postflight Engineering Evaluation Plan (Case Internal Insulation Component)', S. Olson and S. Manz, 10 June 1989.
- 3. TWR-50050 Vol. I Addendum A, 'KSC Postflight Engineering Evaluation Plan, Addendum A' (RSRM-7), M. Mueller, 22 November 1989.
- 4. TWR-16475 Vol. III Addendum F, 'RSRM-7 Unique Postfire Evaluation Insulation Component', S. Hicken, 15 November 1989.
- 5. Memo L232-FY89-M059, 'Inhibitor Database', B. Cannon, November 1988.
- 6. STW7-2831 Rev. D, 'Inspection and Process Finalization Criteria, Insulated Components, Space Shuttle Solid Propellant Rocket Motor', N. F. Eddy, 2 November 1989.
- 7. TWR-16278 Rev. A, 'HPM Internal Insulation Database for the RSRM Design', J. Passman, 5 August 1988.
- 8. TWR-18133 Rev. A, 'RSRM Internal Insulation Design Summary', J. Passman and S. Hicken, September 1988.
- 9. Interoffice Memo, L632-FY90-M057, 'RSRM Insulation Exposure Times', B. Laubacher, 18 April 1990.

REVISIONA\_\_\_\_\_\_\_
FORM TC 7994-310 (REV 2-88)

DOC NO. TWR-17546 VOL III

Α

REVISION

DOC NO. TWR-17546

SEC

VOL

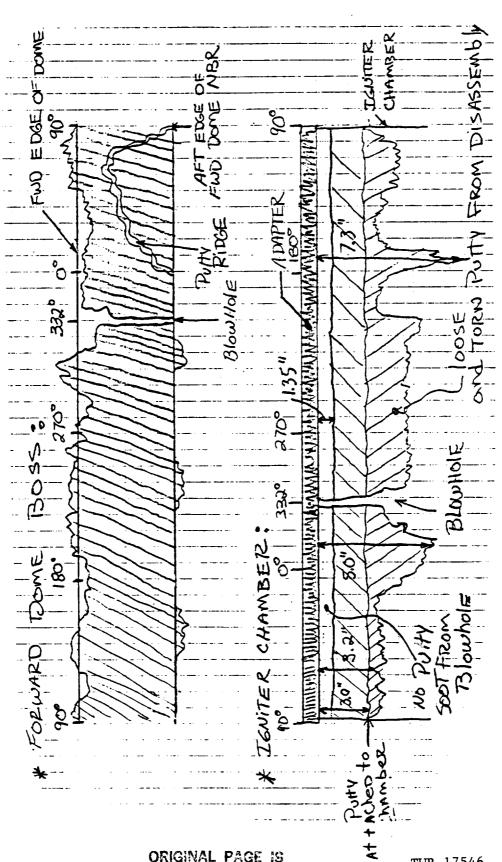
47

PAGE

III

RSRM Motor Configuration

Figure 1

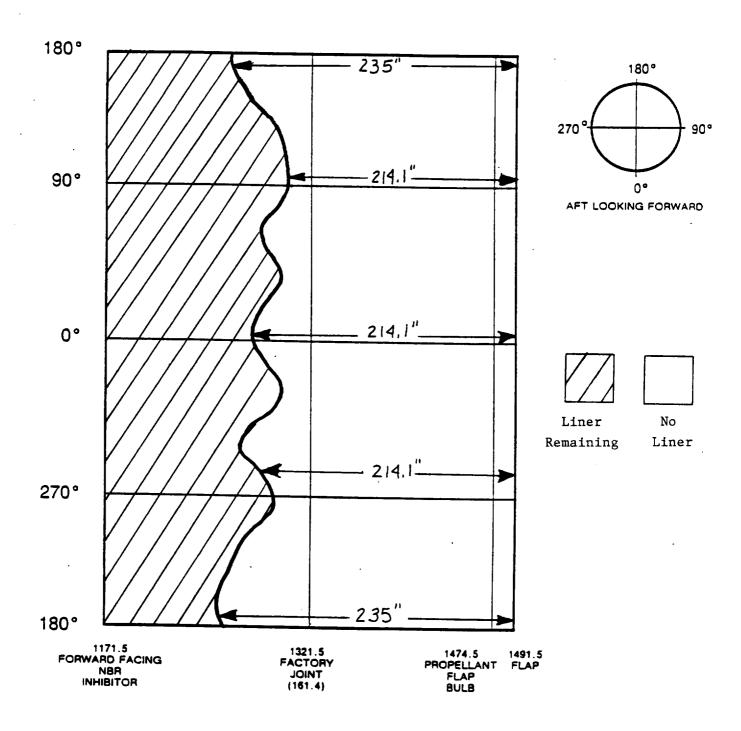


ORIGINAL PAGE IS OF POOR QUALITY

A

TWR-17546 Vol. III



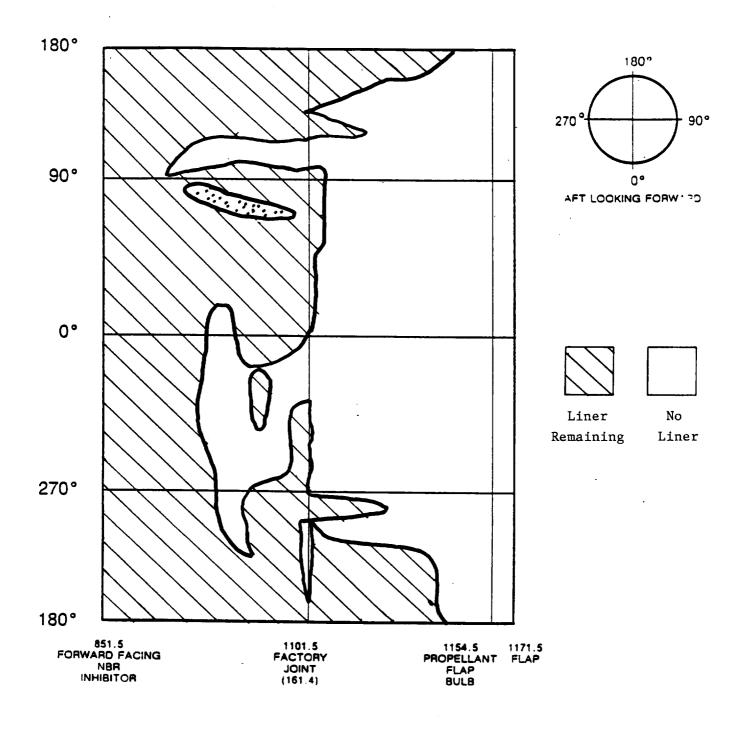


RSRM-7A Aft Center Segment Liner Pattern Figure 3

REVISION A
FORM TC 7994-310 (REV 2-88)

DOC NO.	TWR-17546		VOL	III
SEC		PAGE	49	

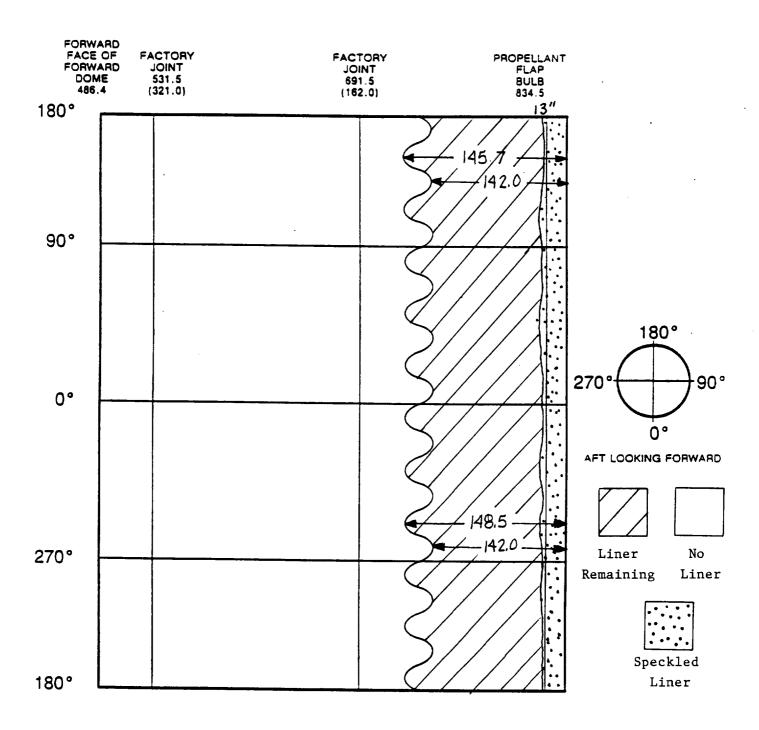




RSRM-7A Forward Center Segment Liner Pattern  $\mbox{ Figure 4}$ 

REVISION A	DOC NO.	TWR-17546		VOL	III
FORM TC 7994-310 (REV 2-88)	SEC		PAGE	50	





RSRM-7A Forward Segment Liner Pattern Figure 5

REVISION <u>A</u>

FORM TC 7994-310 (REV 2-88)

DOC NO.	TWR-17546		VOL	III
SEC		PAGE	51	

All stations are in inches, measured from the tip of the tang or nozzle boss aft face

	7.46 0.44 7.05 7.05 7.05 2.5			5.17 — 6.11 — 6.25 — 7.05 — 7.05 — 7.05 — 8.50 — 8.51 —		0.89 — 0.87 — 0.88 — 0.87 — 0.08 — 0.
				0.921 —		0.881 — 8.451 —
	0,541	_				9.841
ĒNT	0.581	<b>-</b> ]	ENT	2.531 —	<b>⊢</b>	S 851
FORWARD SEGMENT	0.531	—	CENTER SEGMENT	t.181	SEGMENT	7.771 — <b>1</b>
ARD	8.841	-1	TER		AFT S	
-'ORW	0.781	-	CEN		Ą	B.Sel
ш.	0.661	-				2. SOS
	0.215	_		1.415 -		0.41S
	0.452					E. TSS
		_				₹.8₹S
	0.042					0.08s
	0.182					0.785 —
	0.292			0.007		6.882 —
	0.082	_		0 082		0 202
	0.862	—		0.865 —		1.86S
	0.202	—		0.415 8.705		0.SSE —
. 00.	0.0.742			71		0.625 —
0.48£	\range \( \lange \)	Y				0.885 —
للله						0.795 —
						0.878
	A				TWR-17	546 Vol. III

Page 52

Measurement Factor Joint Safety Case **+** Nozzle

Page 53

Α

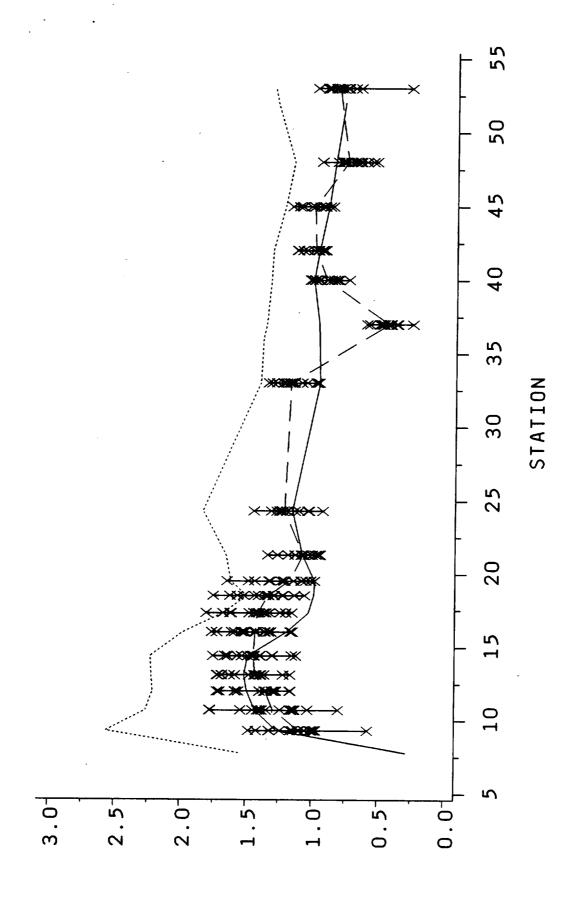
Field Joint (Clevis) Safety Factor Measurement

FIGURE

Vol. III TWR-17546

RSRM-7A AFT DOME INSULATION PERFORMANCE AFI DOME REGION





MATERIAL DECOMPOSITION DEPTH (MDD-IN.)

RSRM-7A MEDIAN RSRM-7A DATA CODE

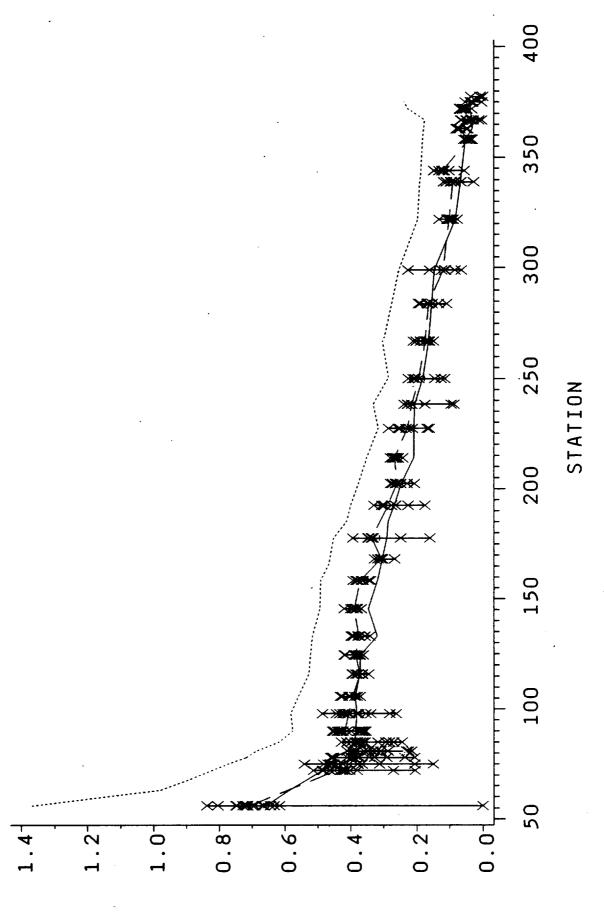
TWR-17546

Vol. III

Page 55

RSRM-7A AFT CYLINDER INSULATION PERFORMANCE





RSRM-7A MEDIAN

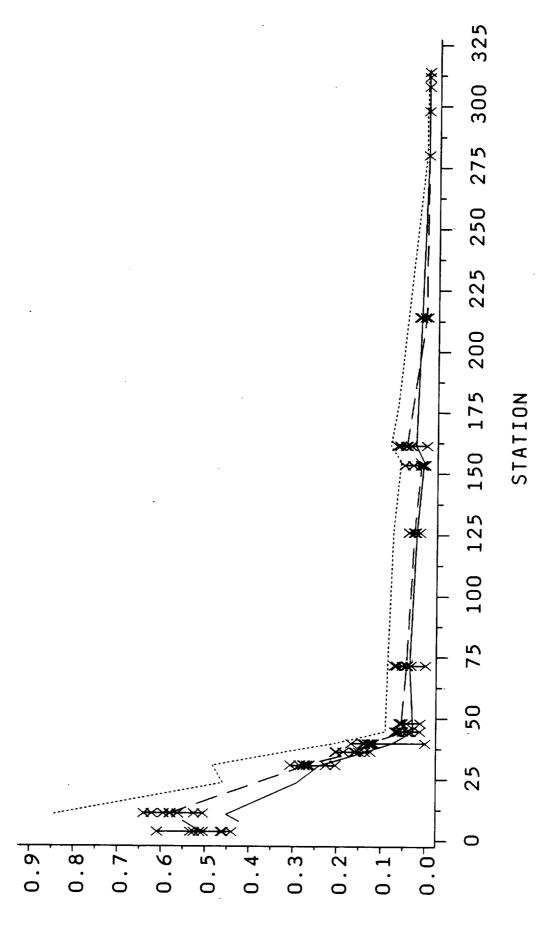
\* \* \* \* RSRM-7A DATA

CODE

AFI CENTER SEGMENT

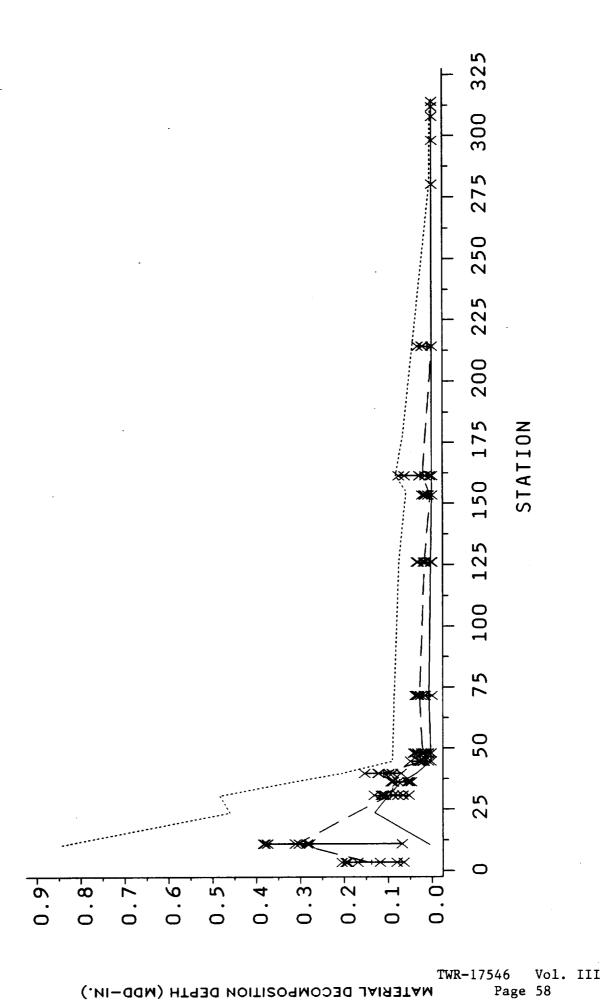
RSRM-7A AFT CENTER SEGMENT INSULATION PERFORMANCE





RSRM-7A MEDIAN RSRM-7A DATA CODE





M+30 DESIGN MDD HPM DATABASE MEDIAN - RSRM-7A MEDIAN \*\*\*\* RSRM-7A DATA CODE

M+30 DESIGN 400 350 RSRM-7A FORWARD SEGMENT STAR TIP INSULATION PERFORMANCE 300 250 STATION LUKWAKU SEGMENI (STAR TIP REGION) FIGURE 13 RSRM-7A MEDIAN 200 50 100 \* \* \* \* \* RSRM-7A DATA 50 0 0.10 -0.05  $0.30^{-}$  $0.40^{-}$ 0.001  $0.35^{-}$ 0.25 0.20 0.15 ORIGINAL PAGE IS CODE POOR QUALITY

MATERIAL DECOMPOSITION DEPTH (MDD-IN.)

450

TWR-17546

Vol. III

Page 59

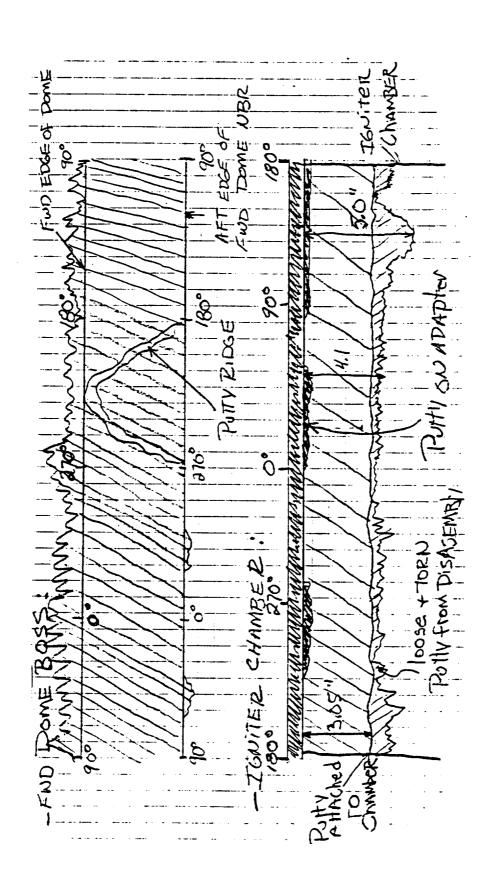
450 M+30 DESIGN MDD 400 RSRM-7A FORWARD SEGMENT NON-STAR TIP INSULATION PERFORMANCE 350 300 250 STATION FORWARD SEGMENT (NON-STAR TIP REGION) FIGURE 14 RSRM-7A MEDIAN 200 150 100 \*\*\* \* RSRM-7A DATA 50 0.05 0.001 0.45 0.30  $0.20^{-}$ 0.35 0.25 0 CODE

MATERIAL DECOMPOSITION DEPTH (MDD-IN.)

TWR-17546

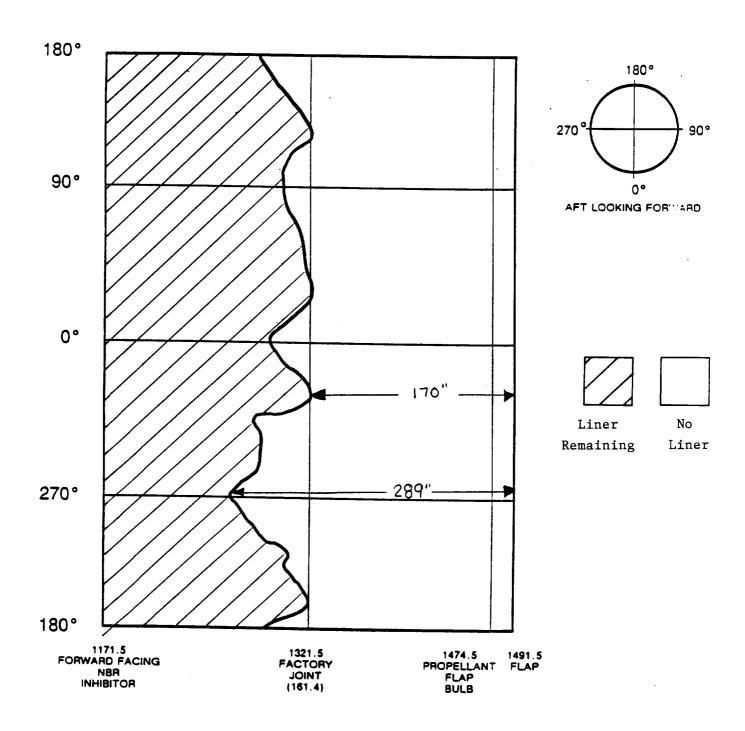
Vol. III

Page 60



TWR-17546 Vol. III



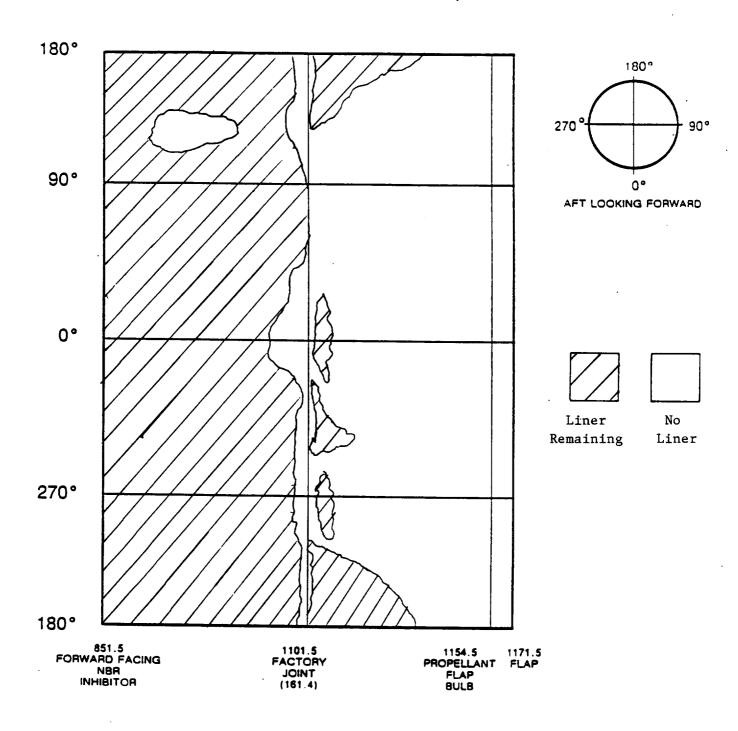


RSRM-7B Aft Center Segment Liner Pattern Figure 16

REVISION A FORM TC 7994-310 (REV 2-88)

DOC NO.	TWR-17546			VOL	III
SEC		PAGE	62	2	



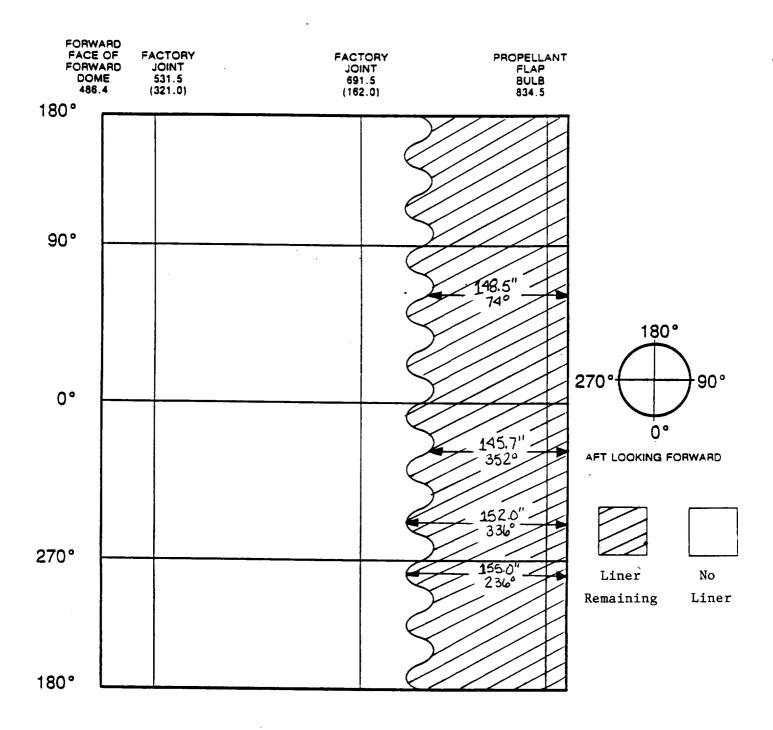


RSRM-7B Forward Center Segment Liner Pattern
Figure 17

REVISION A
FORM TC 7994-310 (REV 2-88)

DOC NO.	TWR-17546			VOL	III
SEC		PAGE	-6	 i3	





RSRM-7B Forward Segment Liner Pattern Figure 18

REVISION A
FORM TC 7994-310 (REV 2-88)

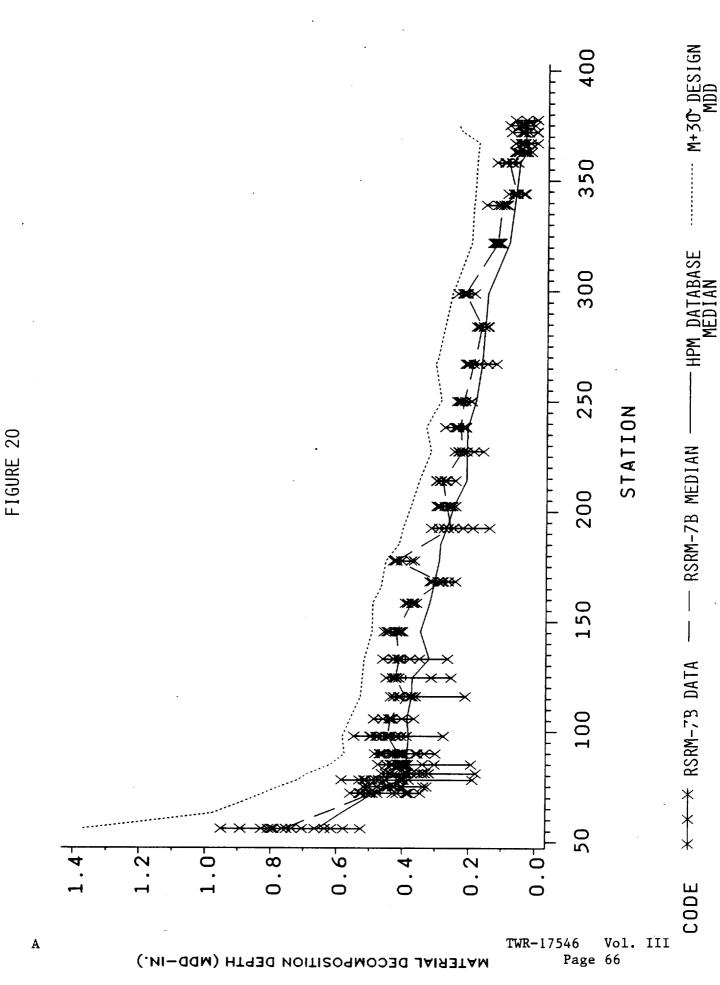
DOC NO.	TWR-17546		VOL	IÍI
SEC		PAGE	64	

AFT DOME REGION

CODE

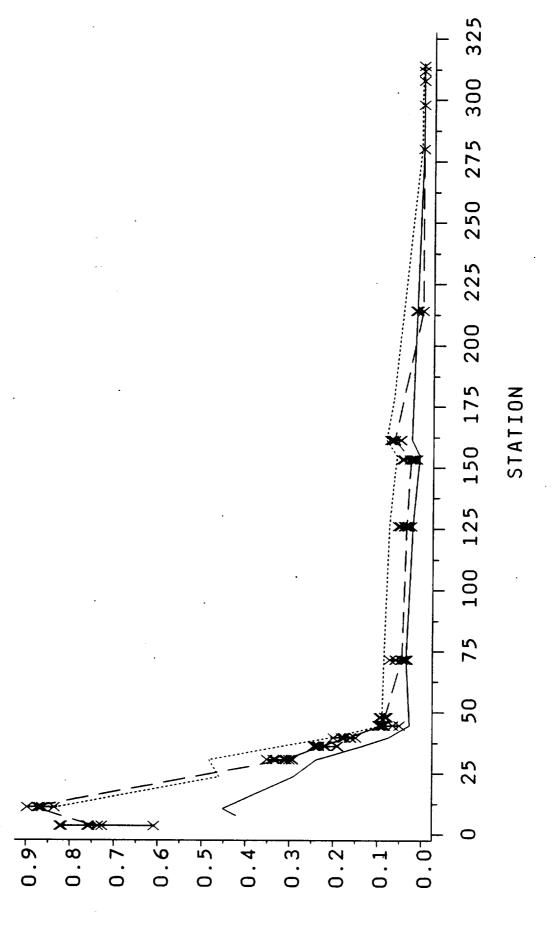
55

AFI CYLINDER REGION RSRM-7B AFT CYLINDER INSULATION PERFORMANCE



AFI CENIER SEGMENT RSRM-7B AFT CENTER SEGMENT INSULATION PERFORMANCE





TWr-17546 Vol. III Page 67 HPM DATABASE MEDIAN

RSRM-7B MEDIAN

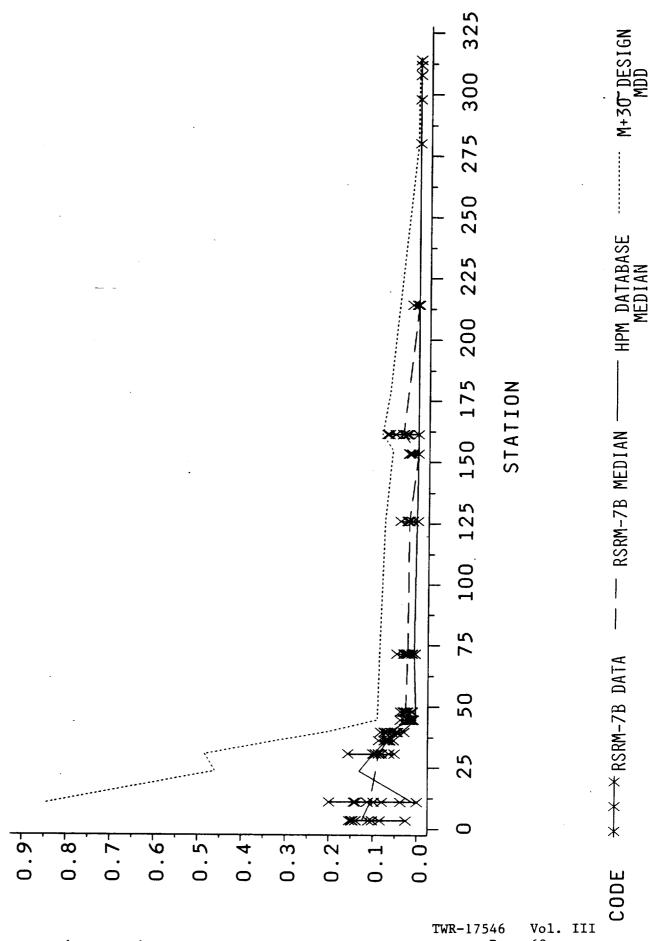
\* \* \* \* RSRM-7B DATA

CODE

FURWARD CENIER SEGMENT

RSRM-7B FORWARD CENTER SEGMENT INSULATION PERFORMANCE



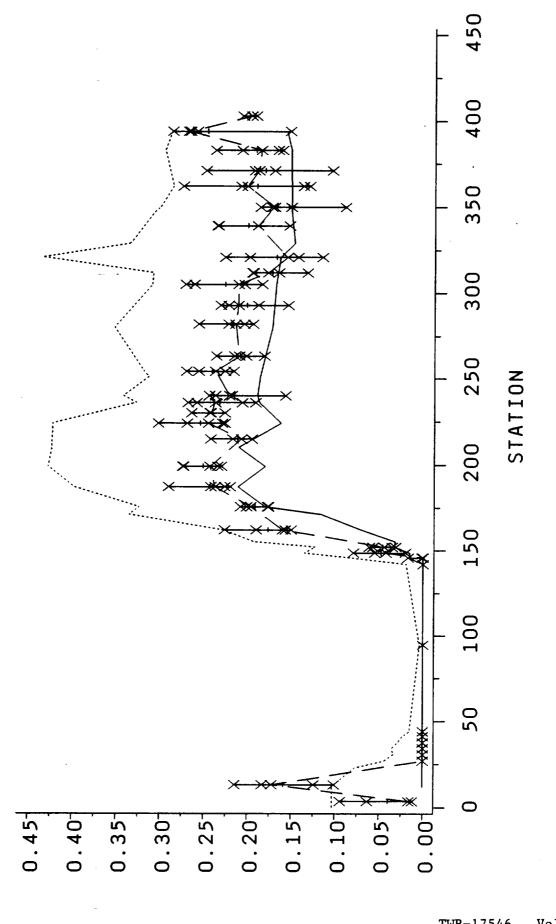


Page 68

LUKWAKU SEGMENI (STAR TIP REGION)

RSRM-7B FORWARD SEGMENT STAR TIP INSULATION PERFORMANCE





RSRM-7B MEDIAN

\* \* \* \* RSRM-7B DATA

CODE

400 **\*\***\*\* RSRM-7B FORWARD SEGMENT NON-STAR TIP INSULATION PERFORMANCE 350 300 250 STATION FUKWAKU SEGMENI (NON-STAR TIP REGION) FIGURE 24 RSRM-7B MEDIAN 200 150 100 \* \* \* \* RSRM-7B DATA 50 0.10 0.05 0.001  $0.20^{-}$  $0.30^{-}$  $0.25^{-}$  $0.15^{-}$ 0.35 0.40 CODE

MATERIAL DECOMPOSITION DEPTH (MDD-IN.)

A

450

746 Vol. III Page 70

TWR-17546



TABLE 1
SUMMARY OF NOZZLE TO CASE JOINT AND FIELD JOINT SAFETY FACTORS

JOINT	MINIMUM COMPLIANCE SAFETY FACTOR (CSF)	DEGREE LOCATION	MINIMUM ACTUAL SAFETY FACTOR (ASF)	DEGREE LOCATION	
					=
NOZZLE TO CASE A	4.6	0°	5.2	0 °	
NOZZLE TO CASE B	4.0	0°	4.5	0°	
A TOTAL A	E /	2102	F 0	0400	
AFT A	5.4	210°	5.8	210°	
AFT B	5.1	120°	5.4	120°	
CENTER A	9.6	90°	10.5	90°	
CENTER B	11.4	130°	12.1	130°	
FORWARD A	12.7	166° & 180°	13.4	180°	
FORWARD B	11.6	136°	12.4	136°	

NOTE: ALL SAFETY FACTORS MUST MEET A 2.0 MINIMUM.

CSF = MDT/MDD

ASF = Actual Prefire Thickness/MDD

Where: MDT = Minimum Design Thickness

MDD = Material Decomposition Depth

REVISIO#
FORM TC 7994-310 (REV 2-88)

DOC NO.	TWR-1754	VOL	III	
SEC		PAGE		



TABLE 2 SUMMARY OF FACTORY JOINT SAFETY FACTORS

SEGMENT	STATION	MINIMUM COMPLIANCE SAFETY FACTOR (CSF)	DEGREE LOCATION	MINIMUM ACTUAL SAFETY FACTOR (ASF)	DEGREE LOCATION
AFT A	56.0"	3.33	338.4°	4.12	338.4°
AFT B	56.0"	2.93	18.0°	3.66	180.0°
AFT A	177.7"	2.54	46.8°	3.82	46.8
AFT B	177.7"	2.34	90.0°	3.60	136.8°
AFT A	299.1"	2.99	26.8°	4.54	46.8°
AFT B	299.1"	2.85	90.00	4.53	90.0°
AFT CTR A	161.4"	3.58	46.0°	9.70	46.0°
AFT CTR B	161.4"	3.23	180.0°	8.60	180.0°
FWD CTR A	161.4"	3.15	136.0°	7.83	136.0°
FWD CTR B	161.4"	3.32	0.0°	8.85	0.0°
FORWARD A	162.0"	3.06	286.0°	4.40	286.0°
FORWARD B	162.0"	2.42	286.0°	3.80	286.0°
FORWARD A	321.0"	3.15	352.0°	3.43	352.0°
FORWARD B	321.0"	4.06	90.00	4.55	90.0°

NOTE: ALL FACTORY JOINT SAFETY FACTORS MUST MEET A 2.0 MINIMUM

CSF = MDT/MDD

ASF = Actual Prefire Thickness/MDD

Where: MDT = Minimum Design Thickness
MDD = Material Decomposition Depth

REVISION
FORM TC 7994-310 (REV 2-88)

DOC NO.	TWR-17546	VOL	III
SEC	PAGE		



TABLE 3
SUMMARY OF CASE INSULATION SAFETY FACTORS

MINIMUM COMPLIANCE SAFETY FACTOR			MINIMUM ACTUAL SAFETY FACTOR		
SEGMENT	(CSF)	STATION	(ASF)	STATION	
	·	-		40.5	
AFT DOME A	1.92	19.5"	2.27	18.5"	
AFT DOME B	1.84	17.3"	2.02	16.0"	
				4.5 5	
AFT A	2.22	145.5"	2.19	145.5"	
AFT B	2.04	145.5"	2.04	145.5"	
A DOM COMP. A	0. 70	71 50	0. (0	20.78	
AFT CTR A	2.43	71.5"	2.60	30.7"	
AFT CTR B	1.99	11.0"	2.44	30.7"	
FWD CTR A	2.81	39.7"	4.38	214.1"	
FWD CTR B	3.32	161.4"	4.15	126.0"	
FORWARD A	1.71	280.0"	2.14	280.0"	
FORWARD B	1.76	394.0"	2.31	394.0"	

NOTE: ALL ACREAGE AREA SAFETY FACTORS MUST MEET A MINIMUM OF 1.5.

CSF = MDT/MDD

ASF = Actual Prefire Thickness/MDD

Where: MDT = Minimum Design Thickness

MDD = Material Decomposition Depth

REVISIO	♣		
CODM TO	7004.210	/DEV/ 2.991	

DOC NO.	TWR-17546	VOL	III
SEC	PAGE		

## Table 4

CRITERIA FOR CLASSIFYING POTENTIAL ANOMALIES

Anomaly	Major Critical	<ul> <li>Could cause failure in combination with other anomaly</li> <li>Could cause damage preventing reuse of preventing required before subsequent static required before subsequent static test/flight</li> </ul>
	Minor	<ul> <li>Requires corrective action, but has no impact on:         <ul> <li>Motor Performance</li> <li>Program Schedule</li> </ul> </li> <li>Does not reduce usability of part for its intended function</li> <li>Could cause damage preventing reuse of hardware in combination with other anomaly</li> <li>Significant departure from the historical data base</li> </ul>
	Remains Observation	Requires no specific action

Note: This criteria is to be applied to the specific observed potential anomaly as it relates to the observed article and as it relates to subsequent articles

REVISION A

NO. TWR-17546 VOL III

SEC PAGE 74

FORM TC 7994-310 (REV 2-88)

88D26-1A

Prefire Condition Clevis at Thiokol Corporation\*\*\*

Total Area** h Unbonded		0.00 3.29 0.00	ار ی	0.0 0.0 0.0	0.00
Primary Bond Failure Depth	0.00 0.00,0.00 0.00	0.00	Primary Bond Failure Depth	0.00 0.00 0.00	0.00
Repair Failure Depth @ Postfire	N/A 0.00,0.00 0.00	N/A 0.00 N/A	ris at H-7 Repair Failure Depth	N/A N/A N/A	N/A N/A N/A
Depth After Repair	N/A 0.00,0.00 0.00	N/A 0.00 N/A	dition Clev Depth After Repair	N/A N/A N/A	N/A N/A N/A
Maximum Postfire Depth @ Degree	N/A 0.00,0.00 0.00	N/A 0.00 N/A	Postfire Condition Clevis at H-7  Maximum Depth Repair  Prefire After Pailure D  Depth @ Degree Repair @ Postfi	N/A N/A	N/A N/A N/A
Degree	N/A 114,223 179	N/A 326 N/A	Degree Location N/A	N/A N/A	N/A N/A N/A
Maximum* Prefire Depth	0.00 0.05 0.08	0.00	Maximum Postfire Depth	0.00	0.00
Segment	A F/C A A/C A Aft	B P/C B A/C B Aft	Segment A F/C	A A/C A Aft	B F/C B A/C B Aft

\* Depth Before Repair \*\* Total Area Full Circumference (Before Repair for Prefire) \*\*\* No prefire PRs at KSC

RSRM-7 Final Clevis Edge Separations

Table 5

Prefire Condition Tang at Thiokol Corporation\*\*\*\*

Total Area** Unbonded	0.69 0.16 4.95	0.50 0.50 0.04		Total Area** Unbonded	6.50 0.24 0.70	0.50 0.01 13.7
Primary Bond Failure Depth	0.00	0.00		Primary Bond Failure Depth	0.210 0.150 0.145	0.00 0.02 0.25
Repair Failure Depth @ Postfire	0.00	0.00 0.00 N/A	ng at H-7	Repair Failure Depth @ Postfire	N/A N/A 0.03	0.00 0.03 N/A
Depth After Repair	00.00	0.00 0.00 N/A	dition Ta	Depth After Repair	N/A N/A 0.00	0.00 N/A
Maximum Postfire Depth @ Degree	0.00	0.00	Postfire Condition Tang at H-7	Maximum Prefire Depth @ Degree	0.00	N/A 0.03 0.00
Degree Location	272 8 145-149	 122 0,121		Degree Location	333-336 279 200-204	N/A 114 173-174
Maximum* Prefire Depth	0.18 0.10 0.12	0.02 0.08 0.02	7	maximum*** Postfire Depth	0.210 0.150 0.175	0.00 0.05 0.25
Segment	A FVD A F/C A A/C	B FVD B F/C B A/C		Segment	A FWD A F/C A A/C	B FVD B F/C B A/C

\* Depth Before Repair \*\* Total Area Full Circumference (Before Repair for Prefire) \*\*\* Depth < 0.05 not documented at H-7 \*\*\*\* No prefire PRs at KSC, No postfire inspection at KSC

RSRM-7 Final Tang Edge Separations

#### RSRM-7A NOZZLE TO CASE JOINT PERFORMANCE

DEGREE LOCATION	PREFIRE (INCHES)	POSTFIRE (INCHES)	MDD	CSF	ASF
0.0 21.6 46.8 68.4 90.0 111.6 136.8 158.4 180.0 201.6 226.8 248.4 270.0 291.6 316.8	5.577 5.638 5.551 5.610 5.561 5.532 5.628 5.588 5.578 5.595 5.613 5.599 5.613	4.510 4.815 4.575 4.797 4.964 4.810 4.978 4.905 4.628 4.798 4.710 4.961 5.138 4.922 5.100	1.067 0.823 0.976 0.813 0.597 0.722 0.650 0.683 0.950 0.797 0.903 0.638 0.479 0.681 0.499	4.6 6.0 5.0 6.0 8.2 6.8 7.5 7.2 5.2 6.1 5.4 7.7 10.2 7.2 9.8	5.2 6.9 5.7 6.9 9.3 7.7 8.2 5.9 7.0 6.2 8.8 11.7 8.2
338.4	5.612 MEDIAN 5.599	4.953 MEDIAN 4.860	0.659 MEDIAN 0.703	7.4 MINIMUM 4.6	8.5 MINIMUM 5.2

#### RSRM-7A AFT FIELD JOINT PERFORMANCE

DEGREE LOCATION	PREFIRE (INCHES)	POSTFIRE (INCHES)	MDD	CSF	ASF
2.0 16.0 30.0 46.0 60.0 76.0 90.0 106.0 120.0 136.0 150.0 166.0 180.0 210.0 226.0 242.0 256.0 270.0 286.0	2.757 2.730 2.735 2.762 2.750 2.753 2.750 2.755 2.765 2.765 2.765 2.747 2.762 2.730 2.747 2.762 2.730 2.747 2.735 2.735 2.735 2.735	2.332 2.336 2.404 2.335 2.314 2.278 2.317 2.304 2.298 2.357 2.342 2.388 2.312 2.285 2.285 2.288 2.312 2.285 2.352 2.352 2.352	0.425 0.394 0.331 0.427 0.436 0.475 0.433 0.456 0.457 0.408 0.409 0.409 0.450 0.477 0.424 0.388 0.404	6.1 6.8 6.5 6.7 6.5 6.7 6.4 6.3 8.4 1.7 6.2 6.1 7.4 7.4 7.4	6.5 6.9 8.3 6.3 6.4 6.1 6.8 6.7 6.1 6.8 7.6
300.0	2.732	2.326	0.381 0.412	6.8 6.3	7.2 6.6
316.0	2.744	2.347	0.397	6.5	6.9
330.0	2.740	2.426	0.314	8.3	8.7
346.0	2.742	2.392	0.350	7.4	7.8
	MEDIAN	MEDIAN	MEDIAN	MINIMUM	MINIMUM
	2.746	2.335	0.411	5.4	5.8

#### RSRM-7A CENTER FIELD JOINT PERFORMANCE

2.0 2.775 2.534 0.241 10.8 11.5 16.0 2.775 2.518 0.257 10.1 10.8 30.0 2.766 2.559 0.207 12.5 13.4 46.0 2.756 2.566 0.190 13.7 14.5 60.0 2.739 2.532 0.207 12.5 13.2 76.0 2.813 2.570 0.243 10.7 11.6 90.0 2.814 2.545 0.269 9.6 10.5 106.0 2.748 2.549 0.199 13.0 13.8 120.0 2.728 2.540 0.188 13.8 14.5 136.0 2.716 2.585 0.131 19.8 20.7 150.0 2.720 2.580 0.140 18.5 19.4 166.0 2.705 2.552 0.153 17.0 17.7 180.0 2.715 2.586 0.129 20.1 21.0 196.0 2.735 2.580 0.155 16.7 17.6 210.0 2.734 2.615 0.119 21.8 23.0 226.0 2.715 2.595 0.120 21.6 22.6 242.0 2.729 2.566 0.163 15.9 16.7 256.0 2.769 2.562 0.207 12.5 13.4 270.0 2.738 2.590 0.140 18.5 19.4 270.0 2.738 2.590 0.120 21.6 22.6 242.0 2.729 2.566 0.163 15.9 16.7 256.0 2.769 2.562 0.207 12.5 13.4 270.0 2.733 2.570 0.163 15.9 16.8 300.0 2.738 2.592 0.146 17.8 18.8 316.0 2.728 2.588 0.140 18.5 19.5 330.0 2.735 2.595 0.140 18.5 19.5 330.0 2.735 2.595 0.140 18.5 19.5 330.0 2.735 2.595 0.140 18.5 19.5 330.0 2.735 2.595 0.140 18.5 19.5 330.0 2.735 2.595 0.140 18.5 19.5 330.0 2.735 2.595 0.140 18.5 19.5 330.0 2.735 2.595 0.140 18.5 19.5 330.0 2.732 2.534 0.198 13.1 13.8	DEGREE LOCATION	PREFIRE (INCHES)	POSTFIRE (INCHES)	MDD	CSF	ASF
346.0 2.732 2.534 0.198 13.1 13.8 MEDIAN MEDIAN MEDIAN MINIMUM MINIMUM	2.0 16.0 30.0 46.0 60.0 76.0 90.0 106.0 120.0 136.0 150.0 120	2.775 2.775 2.7766 2.756 2.739 2.813 2.814 2.748 2.728 2.716 2.720 2.705 2.715 2.735 2.735 2.735 2.735 2.735 2.736 2.739 2.730 2.733 2.738	2.534 2.518 2.559 2.566 2.532 2.570 2.545 2.549 2.580 2.580 2.580 2.580 2.580 2.580 2.595 2.595 2.5662 2.595 2.5622 2.570 2.595	0.257 0.207 0.190 0.207 0.243 0.269 0.199 0.188 0.131 0.140 0.153 0.129 0.155 0.119 0.163 0.207 0.121 0.163 0.146	10.1 12.5 13.7 12.5 10.7 9.6 13.0 13.8 19.8 18.5 17.0 20.1 16.7 21.8 21.6 15.9 12.5 21.4 15.9 17.8 18.5	10.8 13.4 14.5 13.2 11.6 10.5 13.8 14.5 20.7 19.4 17.7 21.0 17.6 23.0 22.6 16.7 13.4 22.6 16.8 18.8 19.5

### RSRM-7A FORWARD FIELD JOINT PERFORMANCE

DEGREE LOCATION	PREFIRE (INCHES)	POSTFIRE (INCHES)	MDD	CSF	ASF
2.0 16.0 30.0 46.0 60.0 76.0 90.0 120.0 136.0 150.0 166.0 180.0 196.0 210.0 226.0 242.0 256.0 270.0 286.0 300.0	2.715 2.709 2.739 2.728 2.733 2.749 2.750 2.741 2.752 2.748 2.758 2.760 2.736 2.736 2.736 2.730 2.744 2.731 2.740 2.738 2.735 2.746	2.542 2.600 2.572 2.650 2.565 2.571 2.606 2.588 2.594 2.556 2.555 2.555 2.555 2.560 2.560 2.560 2.569 2.579	0.082 0.160 0.164 0.204 0.204 0.160 0.185 0.174 0.163 0.175 0.136 0.166 0.167	15.0 23.8 15.5 33.3 15.0 14.1 14.5 19.2 31.6 16.2 15.8 12.7 16.2 14.9 14.9 15.9 14.8 19.1	15.7 24.9 16.4 35.0 15.8 14.9 15.4 20.3 33.6 17.2 16.8 17.0 14.8 15.8 15.8
316.0 330.0 346.0	2.733 2.723 2.725	2.581 2.568 2.580	0.152 0.155 0.145	17.1 16.7 17.9	18.0 17.6 18.8
	MEDIAN 2.737	MEDIAN 2.570	MEDIAN 0.165	MINIMUM 12.7	MINIMUM 13.4

TABLE 11 RSRM-7A AFT DOME INSULATION PERFORMANCE

COMPLIANCE SAFETY FACTOR (CSF)

A

4 90.0 111.6 136.
4.4
60 L
Ξ
_
80 4
ION
CTUAL
•
2
7
7
2
<b>10</b>
r.
5
ĭ
Ξ
_
NO

TWR 17546 Vol. III

	PERFORMANCE
LE 11	INSULATION
TABLE	DOME
	AFT
	RSRM-7A

NATERIAL DECOMPOSITION DEPTH (NDD) INCHES

DESIG M+3S	22.22 22.22 22.22 22.22 22.22 23.22		ω <b>ι</b>
HAX.	1.481 1.718 1.718 1.751 1.751 1.750 1.802 1.644 1.338 1.445 1.339 0.597 1.027 1.127		EXPOSUR TINE 122.8 120.6 114.6 114.6 115.9 105.9 101,7 101,7 101,7 77.7 77.7 77.7 77.7
MEDIAN	1.096 1.392 1.392 1.4430 1.4430 1.331 1.014 1.014 1.169 0.990 0.999		AV 100.11 113.5 11 100.11 113.5 11 100.11 1100
338.4	11.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1		33 36 37 37 37 37 37 37 37 37 37 37 37 37 37
316.8	1.0011 1.1644 1.13574 1.13574 1.13574 1.1358 1.1358 1.1173 1.1263		6 9 8 4 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9
0 291.6	0 1.090 1.239 3 1.297 7 1.421 7 1.421 3 1.285 3 1.285 3 1.285 9 1.030 9 1.364 6 0.364 6 0.901 0 0.935 6 0.935		2 0 2 9 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
.4 270.	24 1.14 171 1.34 18 1.34 18 1.34 11.43 11.43 11.43 11.65 11.60 11.	ERIA )	2 4 6 4 6 4 6 7 7 7 7 7 7 7 7 7 7 7 7 7 7
6.8 248	071 1.0 1630 1.1 1631 1.2 1631 1.2 1631 1.4 1631 1.4 1631 1.4 174 0.3 174 0.4 175 0.9 175 0.9 175 0.9	GN CRITER TE (MDR)	24 2 2 3 2 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3
s 1.6 22	2577 0 3296 1 3296 1 329 1 329 1 329 1 329 1 329 1 329 1 302 0 302 0 698 0	ESI	MS 01.6 22 4.7 4.7 11.0 11.1 11.2 11.7 11.7 11.7 11.7 11.6 13.9 13.9 13.9 13.9 13.9 13.9 13.9
LOCATION 180.0 20	0.983 1.032 1.1283 1.1386 1.390 1.390 1.312 1.312 1.134 1.134 1.134 1.135 0.982 1.035 0.96	+ 3 SIGMA D COMPOSITION SECOND	LOCATION 180.0 20 8.0 8.0 10.9 1 12.1 1 12.1 1 11.0 9 1 14.1 1 14.1 1 14.1 1 16.5 1 10.5 1
DEGREE 158.4	0.999 0.799 1.166 1.166 1.1120 1.120 1.163	THE MIAL DE	158. 158. 8. 9. 10. 10. 11. 12. 12. 12.
6 136.8	5 1.102 5 1.412 6 1.583 1.583 9 1.529 0 1.5	XCEEDED '	6 1 3 6 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9
0 111.6	11.0 11.7 11.7 11.7 11.7 11.7 11.7 11.7	D HAS E	0 111 11 11 11 11 11 11 11 11 11 11 11 1
.4 90.	19 1.48 11 1.70 28 1.70 25 1.71 65 1.65 17 1.53 76 1.40 05 1.22 00 1.00 44 1.22 44 1.22 97 0.48 88 0.81 12 1.02	ING MD	4
6.8 68	323 1.3 396 1.5 579 1.5 718 1.6 775 1.5 772 1.5 674 1.4 519(1.4 126 1.1 771 1.2 771 1.2 771 1.2 771 1.2 771 1.2 771 1.2 771 1.2 771 1.2 771 1.3 772 0.5 773 0.6	PRECED	
21.6 4	242 1.347 1.	TES THE	11.0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
0.0	1.157 1.3948 1.3948 1.3948 1.456 1.584 1.566 1.566 1.483 1.263 1.483 1.263 1.165 1.165 1.163 1.123 1.123 1.103 1.003 1.0	INDICA	0 6 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7
STATION (IN)	00111111111111111111111111111111111111	:	STATION (IN) 9.3 10.7 112.0 113.1 114.4 4 119.5

02

MOTOR ACTION TIME = 123.4 SECONDS

1076668-03

Α

TWR-17546 III Vol. Page 83

SEGMENT MINIMUM = 2.22 AT THE 145.5 INCH STATION A " + " MEANS NEGLIGIBLE MDD HAS OCCURRED

TWR-17546 Vol. III

PERFORMANCE
INSULATION
CYLINDER
AFT
RH-7A

ACTUAL SAFETY FACTOR (ASF)

REQUIRED S.F.	•	1.5	•	1.5	1.5	1.5	•	1.5			٠	•		•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	1.5	1.5	5.5
PLANE	•		0.0	91.	•	0.0	•	•	•	•		16.	•	16.	。	9	90.	Ġ	16.			Ġ	16.	ö	ė		ö	26.	16.		36.		136.8	16.
MIM.	4.12	7	9	9.	۲.	3.77	۳.	٥.	ŝ	9.	'n.	∞.	٦.	7.		₩.	۲.	9.	'n	ŝ	9.	₹.	۲.	4.	'n.	-	'n	S.	٦:	۳.	~	٥.	_	
338.4	٦.	4.	٣.	S	'n	6.43	Τ.																											
316.8	4.75	ς.	7	7	~	4.30	۲.	۳.	'n	9	۲.	۰.	٦.		ĸ.	.ო.	σ.	9.	ď.	7.	٥.	₹.	۲.	'n.	m.	∞.	ĸ.	٥.	7	۳.	₹.	6.9	+	24.53
291.6	'n	6	۲.	9.	∞.	4.24	₹.	9.																				•						
270.0	9	9	'n	7	٠.	5.58	S	7	۲.	•	•	σ.	4	'n.	'n	'n.	7	Ξ.	•	٧.	۹.	۲.	۲.	₹.	9.	σ.	7	7	۳.	Γ,	۳.	٦.	٣,	+
248.4	~	7	-	. 2	. 7	4.34	₹.	8																										
226.8	6	0	4.63	4.33	4.74	4.27	5.	3.48	∞.	0	7	٦.	4.	4	.5	4.	۰.	8	۲.	٦.	∞.	∞.		€.	7.	۰.	∞.	ς.	'n	٥.	۲.	۲.	5.3	+
TIONS 0 201.6	6		~	٦.	۳.	4.09	'n	٠.																										
LOCATI 180.0	٠.	0	0	m	~		6	4	0	٦.	6	٦.	4	m,	٣.	7	٦.	'n	80	0	٦.	٣.	0,	2.98	0	4	*	٣.	-	7.1	+	8.61	+	+
EGREE 158.4	+	0.5	9	8.0	٣.	4.48	٥.																											
D 136.8	0	m	•	~	_	5.44	0	0	∞.	90		7	4.	9	ω.	٥.	۲.	۲.	9.	89.	σ.		9	₹.	٩.	٦.	٥.	۳,	٥.	٥.	6.2	7.	7	+
111.6	3	. "	: -		∞.	4.09	4.	4.																										
0.06	9		. "	m	7	4.18	m	4	7	∞.	7	0	۳.	2.3	~	4	۲.	6.	9.	ĸ.	9	9	٦.	4.	4.	3.1	ς.	۲.	ď	ĸ.	'n	σ,	7	+
68.4	٧	. "	. ~	8	0	4.24	80	٣.									_																	
46.8	ď		. 0	-	80	5.64	٦.	7	.5	9	2	ω.	m	4	7	σ,	٥.	8	9	۲.	6	'n	٥.	٠.		٦.	٦,	∞.	6	٥.	6.7	٥.	۲.	+
21.6	-		. "	. 0	_	5.01	۳,	m.																										
0.0	4	•		-	,	3.77	۳.	0	80	Φ,	2	0	۳.	۳,	4	. 7	۳,	φ.	9	4.	ω,	Θ.	۰	Φ.	٥.	۳.		~	Τ.	9.9	4	6.5	7	+
STATION (IN)	v				: _:	85.0			50	16.	24.	. 6	5	. 89	89	77.	92.	0.2	14.	27.	80	50.	67.	83.	99.	22.	39.	44	58.0	63.0	67.0	72.0	2.0	77.

SEGMENT MINIMUM = 2.19 AT THE 145.5 INCH STATION A " + " MEANS NEGLIGIBLE MDD HAS OCCURRED

# MATERIAL DECOMPOSITION DEPTH (MDD) INCHES

STATION (IN)	0.0	21.6	46.8	68.4	90.0	111.6	136.8	DEGREE 158.4	LOCATI	ONS 201.6	226.8	248.4	270.0	291.6	316.8	338.4	MEDIAN	MAX.	DESIGN M+3S
0	746	208	7.2	.71	7.2	0.75	99		6.4	. 69	99	. 63	.71	.617	700	.83	. 70	. es	. 36
0	514	0.381	41	0.486	46	0.483	40	0.20	4	0.451	41	0.485	.27	31	.463	0.487	. 44	. 51	. 8 1
0	541	366	37	4.5	43	0.46	40	0.15	. 38	. 46	42	. 48	. 20	.313	469	. 45	. 43	. 54	. 77
0	455	.344	29	. 45	. 37	0.45	. 32	0.20	. 39	. 41	39	. 40	. 23	.461	394	.37	. 39	46	. 71
0	.397	. 287	. 21	.36	.35	0.38	. 32	0	. 35	. 34	30	. 41	. 22	.382	349	. 33	. 34	. 41	. 68
0 0.9	.429	.317	.27	. 38	.37	0.38	. 29	0.35	. 41	. 40	.37	. 37	. 28	.364	.371	. 24	.37	. 42	. 61
0.00	. 456	.449	36	. 39	. 45	0.44	.37	0.36	.37	. 42	. 42	. 35	. 43	.430	.412	.37	. 41	.45	.57
0 0.5	.486	. 424	.37	. 26	.40	0.40	. 33	0.38	. 41	.35	40	. 28	. 43	.382	.424	. 44	. 40	4.8	. 58
05.8 0	.381		.43		40		. 38		.37		36		.40		42		. 39	. 43	. 55
16.0	38		. 39		.36		.36		.34		.34		.37		.39		.37	. 39	. 52
24.5 0	41		41		.38		.37		.36		.39		.37		.38		.38	. 41	. 52
33.0	.37		.39		.37		.35		.34		. 35		.39		.39		.37	. 39	. 51
45.5	40		. 39		. 39		.36		.38		. 38		. 38		. 41		. 38	. 41	. 49
58.5	.38		.36		.38		. 34		.37		.36		. 34		. 39		.37	. 39	. 49
68.3 0	. 30		. 32		. 31		. 26		.31		30		. 30		.30		. 30	. 32	. 45
0 7.77	. 34		. 39		.16		. 24		. 33		. 33		. 33		.34		. 33	. 39	. 45
92.5 0	. 27		. 29		.33		. 22		.17		. 29		. 26		30		. 28	.33	. 40
02.5 0	. 26		. 26		. 24		.27		. 20		. 25		. 22		. 27		. 26	. 27	.37
14.0 0	. 27		. 26		. 26		. 26		. 25		. 26		. 24		. 28		. 26	. 28	. 35
27.3 0	. 21		. 25		. 28		. 25		. 16		. 23		91.		. 22		. 22	. 28	.31
38.3 0	. 22		. 21		. 23		.17		80.		. 22		. 09		. 21		. 21	. 23	. 33
50.0 0	. 19		. 21		. 20		. 14		. 12		. 19		. 11		. 22		. 19	. 22	. 28
67.0 0	. 18		.17		. 16		. 14		.17		. 21		91.		. 20		.17	. 21	30
83.9 0	. 16		. 15		. 13		.10		. 16		. 16		. 13		. 18		. 16	. 19	. 25
99.1 0	.11		. 22		õ		. 11		80.		. 12		. 16		. 16		. 11	. 22	. 25
22.0 0	.09		2		<b>:</b>		. 10		0.		60.		. 10		-		€.	.13	. 13
39.0 0	1.0		.09		Ξ.		90.		80.		80.		.09		.02		.09	. 11	. 19
44.0 0	.12		.13		1.		.10		.13		. 14		. 12		.05		. 12	. 14	. B
58.0 0	.04		.04		.03		.05		6		.03		•		.05		.04	. 05	
63.0 0	.0.		.04		90.		. 05		٥.		.07		.07		8		.07	80.	.17
67.0 0	.02		90.		ö		90.		00.		. 04		.01		.03		.04	90.	7
2.0 0	•		.07		0.053		0.069		0.049		0.033		0.058		9		0.059	Γ.	. 2
75.0	.03		0.031		0		. 0.5		00.		. 03		.03		0.003		. 03	0.053	0.237
77.	0		00.		0		0		0		•		•		.03		0	~	.23

MOTOR ACTION TIME = 123.4 SECONDS

PREFIRE MEASUREMENTS INCHES

TWR-17546 Vol. III Page 88

PART NO. 1U76668-03

SERIAL NO. 0000004

POSTFIRE MEASUREMENTS INCHES

<b>t=</b>																										-								
HEDIAN	.67	69	. 52	30	. 16	. 23	.09	.01	.71	. 68	99.	. 74	. 53	. 52	.76	. 16	. 61	. 47	. 45	. 49	. 42	. 35	. 35	. 31	. 91	. 31	. 31	. 39	.37	4	3	0.364	. 49	. 8
MIN.	52	9.	44	. 22	.08	.17	.04	.97	. 65	99.	. 62	. 73	.49	.49	. 69	. 11	. 57	. 46	. 43	. 43	. 39	.32	. 34	. 28	8.	. 28	. 29	.37	35	. 43	. 35	0.352	. 48	8.
338.4	2.61	1.66	1.50	1.31	1.17	1.326	1.18	1.00																										
316.8	. 62	.64	4.8	. 28	.13	. 22	. 14	.01	. 67	99.	99.	. 74	. 49	. 49	.77	. 14	. 60	. 46	. 43	. 48	. 42	. 32	. 34	.30	.86	. 31	. 38	. 50	.35	. 43	. 38	0.358	.54	4
291.6	69.	.70	9.	. 22	.08	1.179	.07	.02																										
270.0	. 78		.75	. 51	. 25	. 29	.09	98	.71	70	. 69	. 74	.54	. 55	. 76	. 18	. 65	. 50	.47	. 57	.53	. 42	.35	. 32	. 91	.31	.31	.40	.36	. 43	. 41	0.365	. 49	8
248.4	69.	. 65	. 49	. 29	.11	1.238	. 20	.09																										
226.8	. 65	. 70	. 53	.30	.15	. 24	90.	00.	.71	. 70	.67	.75	. 54	. 53	. 11	. 15	.60	.47	. 46	. 50	. 42	.35	.36	.32	.89	. 32	.32	.37	.37	. 46	.37	0.388	. 51	8
ONS 201.6	. 70	.68	. 50	. 28	.16	1.234	.09	90.																										
LOCATI	69	.72	54	.31	.17	. 21	.12	. 01	. 75	.72	69.	. 73	.54	. 52	. 73	. 16	.72	. 52	.46	. 51	. 54	. 42	.36	.32	. 93	.34	.32	.39	.37	. 45	. 41	0.373	. 53	.83
EGREE 158.4	. 33	. 94	. 75	. 44	. 23	1.243	.10	. 0 3																										
D.	73	74	55	39	. 21	30	12	0.4	. 70	68	99.	.74	54	. 55	.76	. 26	.62	.46	. 44	. 45	.51	.40	.39	.37	.92	.31	.33	39	. 35	. 45	. 35	0.363	. 48	. 0.
111.6	. 622	604	.465	. 263	860.	1.197	.067	066.																										
0.06	631	613	.457	.275	.118	. 205	990.	.001	.71	. 68	. 65	.76	. 51	. 51	. 69	. 34	. 57	. 48	. 45	. 45	.39	. 34	. 35	. 28	°.	. 28	. 29	.40	.37	. 44	.37	0.367	. 49	8.
68.4	.619	.620	480	.306	.112	237	. 144	.145																										
46.8	597	773	543	379	246	254	158	023	.657	99.	.62	. 74	. 52	. 52	. 73	. 11	. 59	.47	. 44	. 43	. 41	. 33	.35	.31	.80	. 32	. 31	.37	.37	. 45	.37	0.352	.48	8
21.6	.526	.773	608	389	. 203	1.271	.049	666		2	_	_	=																					
0.0	. 703	627	449	. 257	060	189	.063	974	.715	69	62	. 75	. 51	.51	76	. 13	. 64	47	. 43	. 51	. 41	. 35	. 34	. 31	.91	. 32	29	39	.37	. 43	. 41	0.363	.49	8
TATION (IN)	0.9	0	0	0.	0.		0	0.	89	0.9	. T	0.	5.5		۳. . ها	7.7	2.5	2.5	0.	7.3	۳.	0.0	7.0	3.9	9.1	2.0	0.6	4.0	8.0	3.0	7.0	2.0	5.0	7.5

PART NO. 1U76657-01 SERIAL NO. 0000002

TABLE 13
RSRM-7A AFT CENTER SEGMENT INSULATION PERFORMANCE

COMPLIANCE SAFETY FACTOR (CSF)

0.0	46.0	9	•	•						
			.0 136.0 180.0 226.0	180.0	7.46.0	270.0	316.0	MIM.	PLAME	S. #
4.13	4.61	3.48	4.04	4.82	4.20	4.58	3.98	3.48	90.0	2.0
3.76	3.28	2.97	3.38	3.19	3.06	3.62	3.28	2.97	90.0	1.5
2.80	2.74	2.63	3.68	2.85	3.33	2.72	2.45	2.45	316.0	1.5
4.84	2.96	2.99	4.00	3.82	3.75	4.38	3.24	2.96	46.0	1.5
+	3.07	2.57	3.68	3.14		3.58	3.31	2.57	0.06	1.5
30.00	9	5.22	8.57	7.06	10		5.63	5.22	0.06	1.5
5.18	5.33	5.05	4.88	6.86	ĸ		5.05	4.88	136.0	1.5
3.86	4.15	2.62	4.05	5.15	m	+	2.43	2.43	316.0	1.5
5.00	3.9	3.95		6.25		'n	3.85	3.85	316.0	1.5
5.00	20.0	4.52	10.77	14.00	11		2.80	2.80	316.0	1.5
+	m	6.74		3.93		•	5.02	3.58	46.0	2.0
7.22		+	+	21.67			8.13	7.22	0.0	1.5
+	+	+	+	+		+	+	+	0.0	1.5
+	+	+	+	+	+	+	+	+	0.0	1.5
+	+	+	+	+	+	+	+	+	0.0	1.5
+	+	+	+	+	+	+	+	+	0.0	1.5
+	+	+	+	+	+	+	+	+	0.0	1.5
(NI)	MINIMUM = 2.43 AT THE	. 43 A		71.5	71.5 INCH STATION	TATION				
(EA!	MEANS NEGLIGIBLE MDD HAS OCCURRED	GIBLE	MDD H	S occ	URRED					
	•	CTUAL	ACTUAL SAFETY FACTOR (ASF)	FACT	OR (ASI	î.				
		ā	DEGREE LOCATIONS	COCATI	ONS					REQUIRED
0.0	0.94	90.0	.0 136.0 180.0 226.0	180.0	226.0	270.0	316.0	MIN.	PLANE	S. F.
5.13	5.98	4.41	4.98	5.90	5.30	5.66	4.87	4.41	90.0	2.0
4.73		4.07	4.39	4.17	4.02	4.63	4.15	4.02	226.0	1.5
3.04	4 2.90	2.87	4.11	3.03	3.54		2.60	2.60	316.0	1.5
6.51	3.90	4.04		5.13	4.98		4.27	3.90	46.0	1.5
+	4.66	3.96	5.73	4.95	5.22	5.59	4.82	3.96	90.0	1.5
30.2	9	5.43	9.12	7.33	10.91			5.43	0.06	1.5
33.91	86.98	6.44	6.47	8.98	96.9		6.46	6.44	0.06	1.5
4.41	4	3.00	4	8.	3.85		7	2.84	316.0	1.5
,										

SEGMENT MINIMUM = 2.60 AT THE 30.7 INCH STATION A " + " MEANS NEGLIGIBLE MDD HAS OCCURRED

3.20 9.70 7.61

40.00 22.43 5.13 12.54 15.80 13.25 5.33 3.20 + 9.70 18.43 13.53 10.48 13.91 17.03 12.66 7.61 + + 23.67 10.00 + 8.69

+ 7.61

153.5 161.4 214.1 280.0 298.0 307.8 311.8

TABLE 13 RSRM-7A AFT CENTER SEGMENT INSULATION PERFORMANCE

(MDD)	
DEPTH	
DECOMPOSITION DEPTH	INCHES
MATERIAL	

DESIGN M+3S	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000		
HAX.	0 . 6 . 6 . 6 . 6 . 6 . 6 . 6 . 6 . 6 .	0.00 0.018 0.00 0.00	TYPOSURE TIME 113.0 98.0 447.8 32.7 12.0 111.3 10.2 10.0 6.0 6.0 2.6 2.0 2.0
MEDIAN	0.50 0.158 0.127 0.053 0.046 0.053	 	A 400000 44 400000000000000000000000000
316.0	0.533 0.306 0.185 0.1130 0.064 0.057		64 4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6
270.0		0.03 0.00 0.00 0.00 0.00 0.00 0.00 0.00	0 400400000000000000000000000000000000
ONS 226.0		0 0 0 14 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 28 2 26 0 0 2 28 2 2 6 0 0 2 2 2 6 0 0 2 2 2 6 0 0 0 0 0
LOCATIONS	5 0 .4 4 0 .5 9 4 0 0 .5 9 4 0 0 .5 9 4 0 0 .1 5 7 7 0 .1 3 7 7 0 .1 3 7 7 9 9 0 0 0 0 3 3 3 0 0 0 0 0 0 0 0 0 0 0	0.06 0.00 0.00 0 0 0 0 0 0 0 0 0 0 0 0 0	LOCATIONS 0 180.0 22 180.0 22 4 3.9 5 4 6.1 5 4 7 3 3.2 7 6.0 7 6.0 7 6.0
DEGREE 1 0 136.0	0.0000000000000000000000000000000000000	000000	00 44004404 01 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
90.	000480000000000000000000000000000000000	0.03 0 0 0 0 0 0 0 0 0	0 4 9 L S W D 80 W Q Q
46.0	6 8 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	900000	
0.0	1000 11400	0.0	. 4 w w w a 4 4 4 4 0 0 0 0 0 0 0
STATION (IN)	H H B B B B B B B B B B B B B B B B B B	408744	CTATIO (IN) 3.5 11.0 30.7 36.2 39.7 448.0 711.5 711.5 1126.0 1153.5 1611.4 218.1 2280.0 307.8 311.0

MOTOR ACTION TIME = 123.4 SECONDS

TABLE 13 RSRM-7A AFT CENTER SEGMENT INSULATION PERFORMANCE

PREFIRE MEASUREMENTS INCHES

PART NO. 1U76667-01 SERIAL NO. 0000005

( 11 7 )	• •	0.0		7.00T	377 O.OOT		2.2.3	2.017	11.11		100
	.63	. 74	99	.61	.59	.67	.62	5.	.59	.62	2.1
11.0	2.389		2.607	2.467	2.482	2.498	2.432		. 2.389	2.467	1.9
	. 8 1	. 79	. 8 1	.83	. 79	. 79	.80	. 79	. 79	.80	
9	.80	. 79	. 8.1	. 83	.80	. 79	.80	. 79	. 79	.80	9.0
39.7	.63	. 65	99.	.67	.67	.65	.67	. 62	.62	. 65	0.4
4	.36	.36	.37	. 38	.37	.37	.37	.36	.36	.37	0.3
•	.37	.36	. 36	. 38	.37	.36	. 37	.36	98.	.37	•
4	. 19	. 19	. 19	. 19	. 19	. 20	. 19	. 19	. 19	. 19	
26.	. 15	. 15	. 15	. 16	. 15	. 16	. 16	. 15	. 15	. 15	•
53.	.16	. 15	.15	. 16	. 15	. 15	. 16	. 16	. 15	. 16	0.1
61.	.63	. 64	.64	.63	. 62	. 61	. 61	. 59	. 59	. 63	
14.	.13	.13	. 14	. 14	. 14	. 14	. 14	. 13	. 13	. 14	٠
80.	.09	.09	.10	. 10	. 10	.10	.10	. 09	.09	. 10	•
98.	.10	60.	.09	. 09	.09	.10	60.	60	.09	. 09	
7.	.10	.09	.09	. 09	.09	. 10	.09	.09	.09	.09	٠.
11.	.10	.09	.09	.10	.09	. 09	.09	σ	. 09	. 09	0.0
14.	. 10	.10	0.	. 10	. 11	. 10	60	0.097	.09	. 10	0.
PART NO. SERIAL N	1U7 0.0	6652-0	т е	POSTFIRE INCHE	E MEAS	MEASUREMENT S	N H				
STATION			DE	GREE	LOCATIONS	SNS					
(NI)	0	46.0	0	136	180.0	226.0	270.0	316.0	MIN	MEDIAN	
( F		28	. 0	. 6	2, 155		15	. 9	90	2.138	
						, נ		7 0		, ה	
;			,	•	•	;	•	֡֝֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֡֓֓֓֡֓֓֓֡		•	
ċ	0	. 0	. 0	0	0	7	0	9	. 0	. 0	
Ġ	. 64	. 51	. 49	. 55	2	. 52	. 55	. 4.9	4.9	. 53	
4.	. 35	. 30	.30	. 34	. 32	. 33	. 33	. 29	. 29	.32	
<b>.</b>	.36	. 31	. 31	. 32	. 33	. 31	. 32	. 31	.31	. 31	
ä	.15	. 15	. 13	. 15	. 16	. 14	. 19	.12	.12	. 15	
26.	.12	.11	0.120	_	.13	.13	0.135	.11	. 11	. 13	
53.	. 15	. 15	. 12	.15	. 14	. 14	.13	.11	.11	. 14	
61.	0.674	0.574	.61	•	0.569		.57		0.548	.57	
14.	. 11	. 15	'n	.1	. 13	~	ы	.12	.11	.13	
80	u	ı	J		ב	٦,	ы	1	ı	٦.	
98.	u	H	ы	.1	.1	ב	ų	ų	7	.09	
07.	ы	ы	ы	1	בו	,,	u	u	1	.09	
11.	.1	'n	.1		L	,	'n	u	ы	60.	
•	ם	ы	ч	.1	.1	.1	н	ы	ı	0.101	
AN T	IND	INDICATES	THAT	LINER	MATERIAL	AL WAS	REMAINING	THE AT	THAT LOCATION	MOTTA	

TABLE 14 RSRM-7A FORWARD CENTER SEGMENT INSULATION PERFORMANCE

COMPLIANCE SAFETY FACTOR (CSF)

0.0 46.0 90.0 136.0 180.0 226.0 270.0 316.0	STATION			ā	DEGREE I	LOCATIONS	SNC					REQUIRED
1.5 26.50 26.50 33.13 10.34 17.97 12.54 11.04 10.82 10.34 136.0  1.0 6.49 4.99 6.14 6.11 6.11 5.07 5.73 7.08 6.29 279.0  2.1 6.47 7.79 11.54 12.77 10.71 6.45 6.52 6.82 6.82 2.81 2.81 2.81 2.81 2.81 2.81 2.81 2	( IIN )	0	9			180.0	. 9	270.0	0.9	MIN	PLANE	
1.0 6.69 4.95 4.99 6.11 6.81 5.07 6.29 27.94 4.95 46.0  5.7 6.74 7.79 11.24 12.77 10.71 6.45 6.52 6.82 5.73 270.0  5.7 3.55 4.39 11.64 12.77 10.71 6.45 6.52 6.82 5.70 6.85  5.7 3.55 4.39 11.64 12.77 10.71 6.45 6.52 6.82 5.70 6.85  5.8 6.13 31.1.61		6.5	6.5	3.1	0.3	7.9	2.5	-	8.0	0.3	٠.	
1.7 6 47 8.52 14.42 9.62 11.36 6.70 5.73 7.08 5.73 270.0 5.7 6.74 4.79 11.54 12.77 10.71 6.45 6.52 6.82 6.82 6.45 226.0 5.7 6.7 4.79 11.54 12.77 10.71 6.45 6.52 6.82 6.82 6.45 226.0 5.0 7.58 12.00 32 0.00 8.00 + 15.16 6.86 9.00 4.47 270.0 5.0 7.58 12.00 32 0.00 8.00 + 15.16 6.86 9.00 4.47 270.0 5.0 8.24 9.33 75.00 10.00 6.80 + 10.62 4.47 5.00 4.47 270.0 5.1 8.24 9.33 75.00 10.00 6.80 + 10.62 4.47 5.00 4.47 270.0 5.2 8.24 9.33 75.00 10.00 6.80 + 10.62 4.47 5.00 4.47 270.0 5.1 8 8.43 15.73 47.20 3.15 + 4.75 6.36 6.36 6.36 9.10.0 5.1 8 8.43 15.73 47.20 3.15 + 4.75 6.36 6.36 9.10.0 5.1 8 8.43 15.73 47.20 3.15 + 4.75 6.36 6.36 9.10.0 5.1 8 8.43 15.73 47.20 3.15 + 4.75 6.36 6.36 9.10.0 5.0 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9		9.9	6.	σ.	٦.	80	٥.	6.29	7.9	σ.		
5.2 6.74 7.79 11.54 12.77 10.71 6.45 6.52 6.82 6.45 226.0  6.6 13.33 11.61		4	٠,	4.4	9.	1.3	۲.	5.73	°.	۲.		
15. 5.48 12.51 4.38 6.14 3.52 4.78 4.39 3.52 2.81 2.81 316.0  16. 6. 13.33 11.61	Š	7	۲.	1.5	2.7	0.7	4	6.52	•	4.		٠
1.6 13.3 11.61 + 45.00 18.00 20.00 735 14.40 7.35 270.0  1.6 7.58 12.00 32.00 18.00 + 10.62 4.47 4.00 6.66 270.0  1.7 8 13.0 10.00 0 + 10.62 4.47 4.00 6.66 270.0  1.8 8.33 75.00 10.00 + 8.33 4.41 4.84 4.41 270.0  1.9 8.43 15.73 47.20 3.15 + 4 4.06 5.91 4.06 270.0  1.1 6.19 + + + + + + + + + + + + + + + + + + +		3	۳.	6.1	3.5	4.7	m.	3.52	89	8		٠
15.5 5.48 5.00 18.00 + 15.16 6.86 9.00 6.86 270.0  16.5 5.48 5.00 10.00 6.80 + 10.02 4.47 5.00 4.47 270.0  16.5 8.24 9.33 75.00 10.00 + 8.33 4.41 7 5.00 4.47 270.0  16.14 8.43 15.73 47.20 3.15 + 4.46 5.91 4.06 5.91  16.19 + + + + + + + + + + + + + + 0.6 5.91  16.10 + + + + + + + + + + + + + + + 0.6  16.10 + + + + + + + + + + + + + + + + 0.0  17.10 + + + + + + + + + + + + + + + + 0.0  18.10 + + + + + + + + + + + + + + + + + 0.0  18.10 + + + + + + + + + + + + + + + + + 0.0  18.10 + + + + + + + + + + + + + + + + + + 0.0  19.10 + + + + + + + + + + + + + + + + + + 0.0  19.10 + + + + + + + + + + + + + + + + + + +	4	ы.	1.6	+	5.0	8.0	0.0	7.35	4.4	۳.		•
11.5 5.48 5.00 10.00 6.80 + 10.62 4.47 5.00 4.47 270.0  5.0 + 8.33 75.00 10.00 + 8.33 4.41 4.81 4.41 270.0  5.0 + 8.33 75.00 10.00 + 8.33 4.41 4.81 4.41 270.0  11.4 8.43 15.73 47.20 3.15 + 4.46 5.91 4.06 270.0  4.1 6.19 + + + + + + + + + + + + + 0 0.0  8.0 + + + + + + + + + + + + + + + 0 0.0  8.0 + + + + + + + + + + + + + + + + 0 0.0  8.0 + + + + + + + + + + + + + + + + 0 0.0  8.0 + + + + + + + + + + + + + + + + 0 0.0  8.0 + + + + + + + + + + + + + + + + 0 0.0  8.0 + + + + + + + + + + + + + + + + + 0 0.0  8.0 + + + + + + + + + + + + + + + + + 0 0.0  8.0 + + + + + + + + + + + + + + + + + + 0 0.0  8.0 + + + + + + + + + + + + + + + + + + +	-	7.5	2.0	2.0	8.0		5.1	98.9	9.0	₩.		
## 8.33 75.00 10.00 + 8.33 4.41 4.84 4.41 270.0  ## 8.43 15.73 47.20 3.15 + 4 + 4 17.50 6.56 6.35 116.0  ## 8.43 15.73 47.20 3.15 + 4 + 4 4.06 5.91 4.06 270.0  ## 8.43 15.73 47.20 3.15 + 4 + 4 4.06 5.91 4.06 270.0  ## 9.40 + 4 + 4 + 4 + 4 + 4 + 6 6 5.91 4.06 270.0  ## 1	_	4	5.0	0.0	8.9	+	9.0	4.47	•	₹.		
11.4 8.43 15.73 47.20 3.15 + + + + 17.50 6.36 6.36 316.0  4.1 6.19 + + + + + + + + + + 10.6 5.91 4.06  10.0 + + + + + + + + + + + + + + + + + +			۳.	5.0	0.0	+	8.3	4.41	€0	4.		
1.4 8.43 15.73 47.20 3.15 + 8.74 + 3.81 3.15 136.0 4.1 6.19 + + + + + + + + + + + + + + + + + + +		7	۳.	+		+	+	_	۳.	۳.		
## # # # # # # # # # # # # # # # # # #	-	4	5.7	7.2	٦.	+	7	+	•	7		•
0.0 + + + + + + + + + + + + + + + + + +	•	-	+	+	+	+		•	6.	°.		•
# # # # # # # # # # # # # # # # # # #	6	+	+	+	+	+	+	+	+	+		
THE STATE ST	•	+	+	+	+	+	+	+	+	+		•
GMENT MINIMUM = 2.81 AT THE 39.7 INCH STATION  ACTUAL SAFETY FACTOR (ASF)  ACTUAL SAFETY HINIMUM = 4.38 AT THE 214.1 INCH STATION	• r	. 4	٠ +	٠ +	٠ +	٠ +	. 4	٠ 4		•		•
GMENT MINIMUM = 2.81 AT THE 39.7 INCH STATION  " + " MEANS NEGLIGIBLE MDD HAS OCCURRED  ACTUAL SAFETY FACTOR (ASF)  ATION  DEGREE LOCATIONS  IN)  0.0 46.0 90.0 136.0 180.0 226.0 270.0 316.0 MIN. PLANE  1.0 9.05 6.83 6.80 7.97 8.96 6.11 7.30 6.11 270.0  0.7 6.66 8.69 15.19 9.86 11.61 6.96 6.11 7.30 6.11 270.0  0.7 6.66 8.69 15.19 9.86 11.61 6.96 6.11 7.30 6.11 270.0  0.8 92 10.22 15.25 16.68 13.88 8.67 8.47 8.84 8.47 270.0  0.9 6.1 15.50 41.44 22.94 + 19.63 8.71 11.37 8.71 270.0  1.5 6.13 5.62 11.24 7.52 + 11.25 4.92 5.53 4.92 270.0  1.6 6.13 5.62 11.24 7.52 + 11.25 4.92 5.53 4.91 37.83 136.0  1.7 6.68 8.69 15.19 9.86 11.61 6.36 9.79 1.37 8.70 1.37 8.70 1.37 8.70 1.37 8.70 1.37 8.70 1.37 8.70 1.37 8.70 1.37 8.70 1.37 8.70 1.37 8.70 1.37 8.70 1.37 8.70 1.37 8.70 1.37 8.70 1.37 8.70 1.37 8.70 1.37 8.70 1.37 8.70 1.37 8.70 8.70 1.37 8.70 8.70 8.70 8.70 8.70 8.70 8.70 8.7	٠.	+ +	٠ -	- 4	- +	- 4	٠ +	٠ 4	. 4	• +		
GMENT MINIMUM = 2.81 AT THE 39.7 INCH STATION  " + " MEANS NEGLIGIBLE MDD HAS OCCURRED  ACTUAL SAFETY FACTOR (ASF)  ACTUAL SAFETY FACTOR (ASF)  ATION  DEGREE LOCATIONS  3.5 31.55 32.64 40.72 12.60 21.69 15.53 13.59 13.18 12.60 136.0  1.0 9.05 6.83 6.80 7.97 8.96 7.01 8.37 34.31 6.80 90.0  0.7 6.66 8.69 15.19 9.86 11.61 6.96 6.11 7.30 6.11 270.0  0.7 6.66 8.69 15.19 9.86 11.61 6.96 6.11 7.30 6.11 270.0  0.7 6.67 8.92 10.22 15.25 16.68 13.88 8.67 8.47 8.84 8.47 270.0  4.6 13.33 11.94 4 45.75 18.70 20.61 7.45 14.44 7.45 270.0  4.6 13.33 11.94 7.52 4 11.25 5.53 4.92 2.70.0  4.6 13.33 11.94 7.52 4 19.63 8.71 11.37 8.71 270.0  4.6 13.33 11.40 7.70 10.73 4.94 4 7.85 7.68 7.68 7.68 7.68 7.68 7.68 7.68 7.68		٠	٠	٠	٠	٠	•	-		•	•	•
EGMENT MINIMUM = 2.81 AT THE 39.7 INCH STATION  ACTUAL SAFETY FACTOR (ASF)  TATION  ACTUAL SAFETY FACTOR (ASF)  TATION  O. 46.0 90.0 136.0 180.0 226.0 270.0 316.0 MIN. PLANK  3.5 31.55 32.64 40.72 12.60 21.69 15.53 13.59 13.18 12.60 136.0  30.7 6.66 8.69 15.19 9.86 11.61 6.96 6.11 7.30 6.11 270.0  30.7 6.66 8.69 15.19 9.86 11.61 6.96 6.11 7.30 6.11 270.0  34.6 13.33 11.94 + 45.75 18.70 20.61 7.45 14.44 7.45 270.0  44.6 13.33 11.94 + 45.75 18.70 20.61 7.45 14.44 7.45 270.0  44.6 13.33 11.94 + 45.75 18.70 20.61 7.45 14.44 7.45 270.0  48.0 9.61 15.50 41.44 22.94 + 19.63 8.71 11.37 8.71 270.0  53.5 9.82 11.40 + 7.52 + 11.25 4.92 5.53 4.92 270.0  61.4 20.25 38.87 + 7.83 + 20.89 + 9.13 7.83 136.0  14.1 6.71 + + + + + + + + + + + + + + + + + + +	T	+	+	+	+	+	+	+	+	+		•
0.0 46.0 90.0 136.0 180.0 226.0 270.0 316.0 MIN. PLANE 31.55 32.64 40.72 12.60 21.69 15.53 13.59 13.18 12.60 136.0 6.66 8.69 15.19 9.86 11.61 6.96 6.11 7.30 6.11 270.0 8.92 10.22 15.25 16.68 13.88 8.67 8.47 8.84 8.47 270.0 5.74 6.94 10.03 6.02 7.96 7.42 5.90 4.73 4.73 316.0 9.61 15.50 41.44 22.94 + 19.63 8.71 11.37 8.71 270.0 6.13 5.62 11.24 7.52 + 11.25 4.92 5.53 4.92 270.0 9.82 11.40 + 45.75 18.70 20.61 7.45 14.44 7.45 270.0 9.82 11.40 + 4 5.75 18.70 20.63 7.68 7.68 316.0 20.25 38.87 + 7.83 + 20.89 + 9.13 7.83 136.0 6.71 + + + + + + + + + + + + + + + + + + +	+ = '	MEAN		IGIBLE ACTUAL	MDD	Ŋ	URRED OR (AS)	î.				
0.0 46.0 90.0 136.0 180.0 226.0 270.0 316.0 MIN. PLANE 31.55 32.64 40.72 12.60 21.69 15.53 13.59 13.18 12.60 136.0 9.05 6.83 6.80 7.97 8.96 7.01 8.37 34.31 6.80 90.0 6.66 8.69 15.19 9.86 11.61 6.96 6.11 7.30 6.11 270.0 8.92 10.22 15.25 16.68 13.88 8.67 8.47 8.84 8.47 270.0 13.33 11.94 + 45.75 18.70 20.61 7.45 14.44 7.45 270.0 9.61 15.50 41.42 7.94 + 19.63 8.71 11.37 8.71 270.0 9.82 11.40 + 4 22.94 + 19.125 4.92 5.53 4.92 270.0 9.82 11.40 + 4 4.38 7 7.68 7.68 7.68 7.68 7.68 7.68 7.68 7				í	, ,		2					90711090
(IN) 0.0 46.0 90.0 136.0 180.0 226.0 270.0 316.0 MIN. PLANE  3.5 31.55 32.64 40.72 12.60 21.69 15.53 13.59 13.18 12.60 136.0  11.0 9.05 6.83 6.80 7.97 8.96 7.01 8.37 34.31 6.80 90.0  36.2 8.92 10.22 15.25 16.68 13.88 8.67 8.47 8.84 8.47 270.0  39.7 5.74 6.94 10.03 6.02 7.96 7.42 5.90 4.73 4.73 316.0  44.6 13.33 11.94 + 45.75 18.70 20.61 7.45 14.44 7.45 270.0  48.0 9.61 15.50 41.44 22.94 + 19.63 8.71 11.37 8.71 270.0  48.0 9.61 15.50 41.44 22.94 + 19.63 8.71 11.37 8.71 270.0  48.0 9.61 15.50 41.44 22.94 + 19.63 8.71 11.37 8.71 270.0  48.0 9.61 15.50 41.44 22.94 + 19.63 8.71 11.37 8.71 270.0  48.0 9.61 15.0 10.73 + 9.13 4.91 2.0.0  49.1 4 20.25 38.87 + 7.83 + 20.89 + 9.13 7.83 136.0  49.1 6.71 + + + + + + + + + + + + + + + + + + +	STATION			<b>a</b>	בפאנה	3						****
3.5 31.55 32.64 40.72 12.60 21.69 15.53 13.59 13.18 12.60 136.0 11.0 9.05 6.83 6.80 7.97 8.96 7.01 8.37 34.31 6.80 90.0 11.0 6.66 8.69 15.19 9.86 11.61 6.96 6.11 7.30 6.11 270.0 11.0 36.2 8.92 10.22 15.25 16.68 13.88 8.67 8.47 8.84 8.47 270.0 11.0 4.6 13.33 11.94 + 45.75 18.70 20.61 7.45 14.44 7.45 270.0 11.0 9.61 15.50 41.44 22.94 + 19.63 8.71 11.37 8.71 270.0 11.1 27 8.71 20.0 11.1 27 8.71 20.0 11.1 27 8.71 20.0 11.1 27 8.71 20.0 11.1 27 8.71 20.0 11.1 27 8.71 20.0 11.1 27 8.71 20.0 11.1 27 8.71 20.0 11.1 27 8.71 20.0 11.1 27 8.71 20.0 11.1 27 8.71 20.0 11.1 27 8.71 20.0 11.1 27 8.71 20.0 11.1 27 8.71 20.0 11.1 27 8.71 20.0 11.1 20.25 38.87 + 7.83 + 20.89 + 9.13 7.83 136.0 2.1 14.1 6.71 + 7.83 + 7.83 + 20.89 + 9.13 7.83 136.0 11.1 20.0 20.0	( I N )	•	9		136.	-		270.	9	MIN.	PLANE	
11.0 9.05 6.83 6.80 7.97 8.96 7.01 8.37 34.31 6.80 90.0 11.0 90.05 6.66 8.69 15.19 9.86 11.61 6.96 6.11 7.30 6.11 270.0 11.30 6.12 15.25 16.68 13.88 8.67 8.47 8.84 8.47 270.0 11.30 4.74 6.94 10.03 6.02 7.96 7.42 5.90 4.73 4.73 316.0 11.34 4.6 13.33 11.94 + 45.75 18.70 20.61 7.45 14.44 7.45 270.0 11.31 7.30 6.13 2.00 11.31 8.11 2.94 + 19.63 8.71 11.37 8.71 270.0 11.31 8.71 2.20 4.00 10.73 + 9.11 4.91 5.29 4.91 2.70 0 11.31 8.31 8.71 11.37 8.71 2.70 0 11.31 8.31 8.71 11.37 8.71 2.70 0 11.31 8.31 8.31 8.71 11.37 8.71 2.70 0 11.31 8.31 8.31 8.31 8.31 8.31 8.31 8.3	3.5	1.5	2.6	40.7	12.	21.6	15.5	13	13.1	2.6	9	•
30.7 6.66 8.69 15.19 9.86 11.61 6.96 6.11 7.30 6.11 270.0 1.  36.2 8.92 10.22 15.25 16.68 13.88 8.67 8.47 8.84 8.47 270.0 1.  39.7 5.74 6.94 10.03 6.02 7.96 7.42 5.90 4.73 4.73 316.0 1.  44.6 13.33 11.94 + 45.75 18.70 20.61 7.45 14.44 7.45 270.0 1.  48.0 9.61 15.50 41.44 22.94 + 19.63 8.71 11.37 8.71 270.0 1.  71.5 6.13 5.62 11.24 7.52 + 11.25 4.92 5.53 4.92 270.0 1.  26.0 + 9.22 84.00 10.73 + 9.11 4.91 5.29 4.91 270.0 1.  53.5 9.82 11.40 + + + + + + + + + + + + + + + + + + +		9.0	6.8	8.9	7.	8.9	7.0	∞	34.3	€.	0	٠
36.2 8.92 10.22 15.25 16.68 13.88 8.67 8.47 8.84 8.47 270.0 1.  39.7 5.74 6.94 10.03 6.02 7.96 7.42 5.90 4.73 4.73 316.0 1.  44.6 13.33 11.94 + 45.75 18.70 20.61 7.45 14.44 7.45 270.0 1.  48.0 9.61 15.50 41.44 22.94 + 19.63 8.71 11.37 8.71 270.0 1.  71.5 6.13 5.62 11.24 7.52 + 11.25 4.92 5.53 4.92 270.0 1.  26.0 + 9.22 84.00 10.73 + 9.11 4.91 5.29 4.91 270.0 1.  53.5 9.82 11.40 + + + + + + + + + + + + + + + + + + +	0	9	9	15.1	9	11.6	6.9	9	7.3	٦.		•
39.7 5.74 6.94 10.03 6.02 7.96 7.42 5.90 4.73 4.73 316.0 1.  44.6 13.33 11.94 + 45.75 18.70 20.61 7.45 14.44 7.45 270.0 1.  48.0 9.61 15.50 41.44 22.94 + 19.63 8.71 11.37 8.71 270.0 1.  71.5 6.13 5.62 11.24 7.52 + 11.25 4.92 5.53 4.92 270.0 1.  26.0 + 9.22 84.00 10.73 + 9.11 4.91 5.29 4.91 270.0 1.  53.5 9.82 11.40 + + + + + + 4.38 6.36 4.38 270.0 1.  14.1 6.71 + + + + + + + + + + + + + + + + 1.00 1.  80.0 + + + + + + + + + + + + + + + + 1.00 1.  14.1 6.71 + + + + + + + + + + + + + + 1.00 1.  14.0 + + + + + + + + + + + + + + + 1.00 1.  EGMENT MINIMUM = 4.38 AT THE 214.1 INCH STATIOM	9	6	0.2	15.2	16.	13.8	8.6	40	89.	4.		•
44.6 13.33 11.94 + 45.75 18.70 20.61 7.45 14.44 7.45 270.0 1.48.0 9.61 15.50 41.44 22.94 + 19.63 8.71 11.37 8.71 270.0 1.71.5 6.13 5.62 11.24 7.52 + 11.25 4.92 5.53 4.92 270.0 1.25 6.13 5.62 11.24 7.52 + 11.25 4.92 5.53 4.92 270.0 1.25 6.13 5.62 11.24 7.52 + 11.25 4.92 5.53 4.92 270.0 1.25 33.5 9.82 11.40 + + + + + + + + + + + + + + + + + + +	•		6.9	10.0	9	7.9	7.4	'n	4.7		9	•
48.0 9.61 15.50 41.44 22.94 + 19.63 8.71 11.37 8.71 270.0 1.  71.5 6.13 5.62 11.24 7.52 + 11.25 4.92 5.53 4.92 270.0 1.  26.0 + 9.22 84.00 10.73 + 9.11 4.91 5.29 4.91 270.0 1.  53.5 9.82 11.40 + + + + 20.87 7.68 7.68 316.0 1.  61.4 20.25 38.87 + 7.83 + 20.89 + 9.13 7.83 136.0 2.  14.1 6.71 + + + + + + + + + 0.0 1.  80.0 + + + + + + + + + + + + + + + 0.0 1.  11.8 + + + + + + + + + + + + + + + 0.0 1.  EGMENT MINIMUM = 4.38 AT THE 214.1 INCH STATIOM	4		1.9	+	45	18.7	20.6	-	14.4	4		
71.5 6.13 5.62 11.24 7.52 + 11.25 4.92 5.53 4.92 270.0  26.0 + 9.22 84.00 10.73 + 9.11 4.91 5.29 4.91 270.0  53.5 9.82 11.40 + + + 20.87 7.68 7.68 316.0  61.4 20.25 38.87 + 7.83 + 20.89 + 9.13 7.83 136.0  14.1 6.71 + + + + + + + + + + + + + + + + + + +	•	9	. P.	41.4	22.	+	19.6	•	11.3	7	0	
26.0 + 9.22 84.00 10.73 + 9.11 4.91 5.29 4.91 270.0 1.  53.5 9.82 11.40 + + + 20.87 7.68 7.68 316.0 1.  61.4 20.25 38.87 + 7.83 + 20.89 + 9.13 7.83 136.0 2.  14.1 6.71 + + + + + + + + + + + + + + + + + + +	, ,-		5.6	11.2	7		1.2	4	5.5	6		
53.5 9.82 11.40 + + + + 20.87 7.68 7.68 316.0 1.  61.4 20.25 38.87 + 7.83 + 20.89 + 9.13 7.83 136.0 2.  14.1 6.71 + + + + + + + + + + + + + + + + + + +	26	+		84.0	10.		9.1	4	5.2	6	ď	•
61.4 20.25 38.87 + 7.83 + 20.89 + 9.13 7.83 136.0 2.  14.1 6.71 + + + + + + + + + + + + + + + + + + +	5		1.4	+	+		+	20	7.6	9	9	
14.1 6.71 + + + + + + + 4.38 6.36 4.38 270.0 1.  80.0 + + + + + + + + + + + + + + + 10.0 1.  98.0 + + + + + + + + + + + + + + + 0.0 1.  17.8 + + + + + + + + + + + + 0.0 1.  11.8 + + + + + + + + + + + + 0.0 1.  EGMENT MINIMUM = 4.38 AT THE 214.1 INCH STATIOM	61	0.2	80		∞.		8.0		9.1	٠	.0	
80.0 + + + + + + + + + + + + + + + + 0.0 1. 98.0 + + + + + + + + + + + + + + 0.0 1. 11.8 + + + + + + + + + + + + 0.0 1. 14.0 + + + + + + + + + + + 0.0 1. EGMENT MINIMUM = 4.38 AT THE 214.1 INCH STATIOM	14	6.7	+	·	+		+	4.3	٣.	۳.		•
98.0 + + + + + + + + + + + + + + + + 0.0 1. 07.8 + + + + + + + + + + + + 0.0 1. 11.8 + + + + + + + + + + + 0.0 1. 14.0 + + + + + + + + + + 0.0 1. EGMENT MINIMUM = 4.38 AT THE 214.1 INCH STATIOM	8.0	+	+	+	+	+	+		+	+	6	•
11.8 + + + + + + + + + + + + + + 11.8 + + + + + + + + + + + + + + + + + + +	8	+	+	+	+	+	+	+	+	+	0.0	
11.8 + + + + + + + + + + + + + + + 14.0 1.0 1.0 1.1.8	07	+	+	+	+	+	+	+	+	+	0.0	•
14.0 + + + + + + + + + + + + + + 1.0 1.0 1.0 EGMENT MINIMUM = 4.38 AT THE 214.1 INCH STATION	: [	+	+	+	+	+	+	+	+	+	0.0	•
EGMENT MINIMUM = 4.38 AT THE 214	14	+	+	+	+	+	+	+	+	+	0.0	•
EGMENT MINIMUM = 4.38 AT THE 214				;		,	1	1				
	ω		MUM	4.38 A	THE	214.1	INCH	TATION				

TWR-17546 Vol. III

TABLE 14 RSRM-7A FORWARD CENTER SEGMENT INSULATION PERFORMANCE

MATERIAL DECOMPOSITION DEPTH (MDD) INCHES

NESTON.	M+3S	1.067	0.820	0.484	0.318	0.205	060.0	0.089	0.086	0.074	9 6	0.082	0.029	0.005	0.005	0.003		0.003	
	HAX.	0.205	0.384	0.131	0.093	0.153	0.049	0.042	0.038	0.034	0.022	0.075	0.032	<b>'</b> 0	•		• =	. 0	
	MEDIAN	0.143	0.306	0.097	0.083	0.109	0.023	0.022	0.028	0.016	0.004	0.021	0	0	0	•	· c	0	
	316.0	0.196	0.068	0.106	0.088	0.153	0.025	0.032	0.034	0.031	0.022	0.062	0.022	0	0	0	c	0	
	270.0	0.192	0.302	0.131	0.092	0.122	0.049	0.042				•	0.032<0.022	0	0	0	0	0	
SNC	46.0 90.0 136.0 180.0 226.0 270.0 316.0	0.169	0.375	0.112	0.093	0.098	0.018	0.019	0.016	0.018	0	0.027	0	0	0	0	0	0	
LOCATI	180.0	0.118	0.279	990.0	0.056	0.090	0.020	0.002	0	0	0	0	0	0	0	•	0	0	
DEGREE LOCATIONS	136.0	0.205	0.311	0.078	0.047	0.122	0.008	0.016	0.025	0.015	0	0.075	0	0	0	0	0	0	
Δ	90.0	0.064	0.381	0.052	0.052		0.002	0.009	0.017	0.002	0	0.005	0	0	0	0	0	0	
		0.080	0.384	0.088	0.077	0.098	0.031	0.024	0.034	0.018	0.015	0.015	0	0	•	0	0	0	
z	0.0	0.080	0.284	0.116	0.089	0.121	0.027	0.038	0.031	•	0.017	0.028	0.021	0	0	0	0	0	
STATION	(IN)	3.5	11.0	30.7	36.2	39.7	44.6	48.0	71.5	126.0			214.1	280.0	298.0	307.8	311.8	314.0	

A " < " INDICATES THE PRECEDING NDD HAS EXCEEDED THE M + 3 SIGMA DESIGN CRITERIA

MATERIAL DECOMPOSITION RATE (MDR) MILS / SECOND

		DEGREE LOCATIONS	LOCATIC	SNS		. '		EXPOSURE
4. 0 0	_	136.0	180.0	226.0	270.0	316.0	AVE.	TIME
0.7 0.7 0.6		1.8		1.5	1.7	1.7	1.2	113.0
3 · 9				ω. Θ	3.1	0.7	3.0	68.3
1.8		1.6		2.3	2.7	2.2	1.9	48.1
2.3		1.4		2.8	2.8	2.6	2.2	33.3
4.3		5.4		4.3	5.4	6.7	4.8	22.8
		9.0	1.6	1.4	3.8	2.0	1.8	12.8
2.0		1.3		1.6	3.5	5.6	1.9	12.1
3.1		2.3	0	1.5	3.5	3.1	2.2	11.0
1.9		1.6	0	1.9	3.5	3.2	1.5	9.6
1.7		0	0	0	0.9	2.5	6.0	80 80
1.4		6.9	0	2.5	0	5.7	2.5	10.8
0		0	0	0	4.4	3.1	1.3	7.2
0		0	0	0	0	0	0	4.2
0		0	0	0	0	0	0	0.4
0		0	0	0	0	0	0	. K
0		0	0	0	0	0	. 0	7 7
•		•	•		,	)	•	:

MOTOR ACTION TIME = 123.6 SECONDS

TABLE 14 RSRM-7A FORWARD CENTER SEGMENT INSULATION PERFORMANCE

PREFIRE MEASUREMENTS INCHES

PART NO. 1U76667-01 SERIAL NO. 0000007

5 2.524 2.611 2.606 2.542 2.562 2.623 2.544 2.523 2.595 2.54 2.501 2.623 2.524 2.611 2.623 2.596 2.548 2.501 2.623 2.595 2.595 2.595 2.591 2.623 2.595 2.595 2.595 2.591 2.623 2.595 2.595 2.591 2.623 2.595	770000000	24		•		•	•				NY 10 3 4	TOL
7 5.571 2.625 2.596 2.584 2.562 2.528 2.538 2.534 2.524 2.595 2 7 6.751 2.625 2.590 0.759 0.756 0.766 0.701 2.628 2.528 2.533 2.595 2 7 6.751 2.625 0.790 0.759 0.756 0.706 0.801 0.774 0.775 0.785 0 7 6.752 0.756 0.790 0.769 0.766 0.706 0.801 0.774 0.775 0.785 0 7 6.0.560 0.370 0.703 0.746 0.771 0.365 0.361 0.707 0.735 0.706 0.7073 0.708 0.707 0.708 0.707 0.708 0.707 0.708 0.707 0.708 0.707 0.708 0.707 0.708 0.707 0.708 0.707 0.708 0.707 0.708 0.707 0.708 0.707 0.708 0.707 0.708 0.707 0.708 0.707 0.708 0.707 0.708 0.707 0.708 0.708 0.707 0.708 0.708 0.707 0.708 0.708 0.707 0.708 0.7		7	,	,								
7. 6772 0.765 0.765 0.776 0.766 0.768 2.528 2.333 2.333 2.550 1.0 0.757 0.765 0.765 0.765 0.765 0.766 0.765 0.766 0.765 0.765 0.766 0.765 0.765 0.765 0.765 0.765 0.765 0.765 0.765 0.765 0.765 0.765 0.765 0.765 0.765 0.765 0.776 0.776 0.775 0.765 0.776 0.775 0.765 0.776 0.775 0.776 0.775 0.776 0.775		* * * * * * * * * * * * * * * * * * * *	. 61	2.60	2.58	. 26	9	2.60	2.58	.5	. 59	.12
7 0.744 0.785 0.795 0.765 0.766 0.795 0.794 0.775 0.77		1/6	70	2.59	2.47	. 20	۰.	2.52	2.33	.3	.55	96.
7 0.695 0.680 0.702 0.784 0.777 0.806 0.779 0.778 0.777 0.785 0.777 0.785 0.777 0.785 0.777 0.785 0.777 0.785 0.787 0.787 0.787 0.787 0.787 0.787 0.787 0.788 0.786 0.376 0.366 0.376 0.365 0.366 0.376 0.365 0.366 0.376 0.365 0.366 0.376 0.365 0.367 0.365 0.367 0.365 0.378 0.365 0.367 0.365 0.378 0.365 0.367 0.365 0.378 0.365 0.386 0.386 0.386 0.386 0.386 0.386 0.386 0.386 0.386 0.387 0.385 0.387 0.385 0.387 0.385 0.387 0.385 0.387 0.387 0.385 0.387 0.38	7.7.9.0.5.0.4	7//	٥ :	6/.0	0.76	. 76		0.80	0.77	٠ ٦	. 7	.75
10   10   10   10   10   10   10   10		400		67.0	0.78	. 77	∞.	0.77	0.77	. 7	. 78	.60
0 0.365 0.370 0.370 0.376 0.374 0.371 0.365 0.361 0.360 0.368 0 0.366 0.365 0.378 0.0350 0.378 0.366 0.386 0.395 0.366 0.367 0.368 0.190 0.191 0.191 0.183 0.161 0.162 0.167 0.167 0.168 0.167 0.118 0.122 0.119 0.112 0.111 0.111 0.112 0.112 0.112 0.113 0.114 0.113 0.117 0.113 0.117 0.113 0.117 0.113 0.117 0.113 0.117 0.113 0.117 0.113 0.117 0.113 0.117 0.113 0.117 0.113 0.117 0.113 0.117 0.113 0.117 0.113 0.117 0.112 0.112 0.112 0.114 0.118 0.118 0.117 0.112 0.112 0.112 0.114 0.118 0.118 0.112 0.112 0.112 0.112 0.113 0.114 0.118 0.118 0.112 0.112 0.112 0.113 0.114 0.113 0.117 0.113 0.117 0.113 0.117 0.113 0.117 0.113 0.117 0.112 0.112 0.114 0.118 0.118 0.112 0.112 0.113 0.114 0.113 0.114 0.113 0.114 0.113 0.114 0	• • • • • •	9	9	0 . 70	0.73	. 71	٠.	0.72	0.72	. 68	.71	. 43
0 0.1355 0.1372 0.373 0.365 0.365 0.365 0.364 0.364 0.365 0.372 0.0135 0.1367 0.365 0.372 0.373 0.365 0.365 0.365 0.397 0.188 0.190 0.189 0.190 0.190 0.190 0.190 0.190 0.190 0.190 0.190 0.190 0.190 0.190 0.190 0.190 0.190 0.190 0.190 0.190 0.190 0.190 0.160 0.166 0.166 0.166 0.166 0.166 0.167 0.167 0.167 0.167 0.167 0.190 0.107 0.107 0.190 0.107 0.190 0.107 0.190 0.107 0.190 0.107 0.190 0.107 0.110 0.100	. w	360	.37	0.37	0.36	.37	۳.	0.36	0.36	.36	.36	.36
5 0.190 0.191 0.191 0.188 0.190 0.180 0.187 0.188 0 0.189 0.190 0.191 0.191 0.188 0.190 0.190 0.191 0.198 0.190 0.190 0.190 0.190 0.190 0.190 0.190 0.190 0.190 0.100 0.	v. o. 4	365	. 37	0.37	0.36	. 36	٣.	0.36	0.36	.36	.36	. 28
0 0.170 0.166 0.168 0.161 0.168 0.164 0.167 0.164 0.167 0.167 0 5 0.167 0.171 0.172 0.152 0.166 0.168 0.167 0.169 0.169 0.169 0.167 0.171 0.172 0.172 0.156 0.168 0.167 0.169 0.168 0.167 0.167 0.171 0.172 0.172 0.180 0.180 0.180 0.191 0.172 0.181 0.181 0.181 0.191 0.192 0.192 0.191 0.193 0.194 0.193 0.194 0.193 0.194 0.193 0.194 0.193 0.194 0.193 0.194 0.193 0.194 0.193 0.194 0.195 0.195 0.194 0.197 0.196 0.196 0.196 0.196 0.196 0.196 0.197 0.196 0.197 0.196 0.197 0.196 0.197 0.196 0.197	0.4	190	. 19	0.19	0.18	. 19	٦.	0.18	0.18	. 18	. ± 8	.17
5 0.167 0.171 0.172 0.163 0.166 0.168 0.167 0.169 0.163 0.168 0.167 0.170 0.171 0.172 0.163 0.166 0.168 0.167 0.187 0.181 0.141 0.143 0.141 0.143 0.141 0.143 0.141 0.143 0.141 0.143 0.141 0.143 0.141 0.143 0.141 0.143 0.141 0.143 0.141 0.143 0.141 0.141 0.143 0.142 0.141 0.143 0.116 0.117 0.116 0.117 0.119 0.112 0.113 0.114 0.117 0.119 0.112 0.119 0.112 0.119 0.110 0.111 0.11	4	170	. 16	0.16	0.16	.16	٦.	0.16	0.16	. 16	1.6	1.5
4 0.567 0.583 0.541 0.587 0.528 0.564 0.570 0.566 0.528 0.567 0 0.114 0.114 0.114 0.114 0.115 0.114 0.115 0.114 0.115 0.114 0.115 0.114 0.115 0.114 0.115 0.114 0.115 0.116 0.114 0.115 0.117 0.116 0.118 0.112 0.119 0.117 0.119 0.112 0.119 0.112 0.119 0.110 0.110 0.110 0.110 0.110 0.110 0.110 0.110 0.110 0.110 0.110 0.111 0.117 0.118 0.112 0.111 0.117 0.118 0.117 0.118 0.117 0.118 0.117 0.118 0.117 0.118 0.117 0.118 0.117 0.119 0.117 0.118 0.117 0.119 0.117 0.118 0.117 0.119 0.117 0.118 0.117 0.119 0.117 0.118 0.117 0.110 0.111 0.117 0.118 0.117 0.110 0.	٠.	167	.17	0.17	0.16	. 16	٦.	0.16	0.16	1.	1.	14
1 0.141 0.143 0.144 0.139 0.141 0.137 0.140 0.140 0.137 0.141 0.10 0.115 0.115 0.115 0.115 0.116 0.116 0.116 0.116 0.119 0.115	4.	267	. 58	0.54	0.58	. 52	'n	0.57	0.56	. 52	. 56	. 23
0 0.117 0.119 0.122 0.114 0.117 0.116 0.117 0.116 0.117 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	.10	141	. 14	0.14	0.13	. 14	٦.	0.14	0.14	. 13	1.	13
0 0.116 0.119 0.122 0.114 0.122 0.118 0.115 0.115 0.1119 0 8 0.118 0.122 0.113 0.113 0.117 0.111 0.111 0.111 0.111 0.111 0.111 0.111 0.118 0 0 0.117 0.120 0.120 0.113 0.118 0.115 0.111	0	111	. 11	0.12	0.11	.11	٦.	0.11	0.11	11.	11	60
8 0.118 0.122 0.119 0.113 0.118 0.117 0.119 0.112 0.116 0 8 0.117 0.118 0.122 0.113 0.117 0.115 0.117 0.111 0.111 0.117 0 0 0.117 0.120 0.122 0.114 0.118 0.115 0.117 0.111 0.111 0.117 0 0 0.117 0.120 0.122 0.114 0.118 0.115 0.112 0.112 0.112 0.118 0  MO. 1U76651-03 POSTFIRE MEASUREMENTS  AL NO. 0000003 INCHES  INCHES  10 0.0 46.0 90.0 136.0 180.0 226.0 270.0 316.0 MIN. MEDIAN 10 0.0 46.0 90.0 136.0 180.0 226.0 270.0 316.0 MIN. MEDIAN 11 0.0 2.287 2.239 2.209 2.167 2.225 2.226 2.265 2.167 2.233 12 0.287 2.239 2.209 2.167 2.225 2.226 2.265 2.167 2.233 12 0.056 0.677 0.738 0.691 0.700 0.668 0.670 0.688 0.656 0.677 0.714 12 0.574 0.592 0.632 0.631 0.737 0.721 0.713 0.687 0.690 0.687 0.714 13 0.574 0.582 0.358 0.358 0.354 0.353 0.316 0.316 0.316 0.316 14 0.574 0.582 0.157 0.148 0.166 0.146 0.133 0.133 0.147 15 0.159 0.157 0.174 0.163 L L L L L L L L L L L L L L L L L L L	o o.	116	. 11	0.12	0.11	.12	Ξ.	0.11	0.12	11	111	60
*** 0.117 0.118 0.120 0.113 0.117 0.115 0.117 0.111 0.117 0.118 0.117 0.118 0.117 0.117 0.118 0.117 0.118 0.117 0.118 0.118 0.118 0.118 0.118 0.118 0.112 0.112 0.118 0.	<b>8</b> .	118	.12	0.11	0.11	.11	۲.	0.11	0.11	11	111	0
MO. 1U76651-03 POSTFIRE MEASUREMENTS  AL NO. 0000003 INCHES  INCHE	8.	117	11	0.12	0.11	.11	٦.	0.11	0.11	11.	11	
MO. 1U76651-03 POSTFIRE MEASUREMENTS  INCHES  ION  0.0 46.0 90.0 136.0 180.0 226.0 270.0 316.0 MIN. ME  5 2.444 2.531 2.542 2.379 2.442 2.456 2.417 2.388 2.379 2.  0 2.287 2.239 2.209 2.167 2.222 2.253 2.226 2.265 2.167 2.  0 0.556 0.677 0.738 0.691 0.701 0.688 0.687 0.688 0.687 0.688 0.687 0.688 0.687 0.688 0.687 0.688 0.687 0.688 0.687 0.688 0.687 0.688 0.687 0.687 0.688 0.687 0.688 0.687 0.688 0.687 0.688 0.687 0.688 0.687 0.588 0.338 0.338 0.338 0.338 0.338 0.338 0.358 0.354 0.354 0.324 0.332 0.316 0.336 0.324	۰.	-		0.12	0.11	. 11	٦.	0.12	0.11	.11	11.	,
AL NO. 0000003  INCHES  ION  DEGREE LOCATIONS  1 0.0 46.0 90.0 136.0 180.0 226.0 270.0 316.0 MIN. ME  2 2.444 2.531 2.542 2.379 2.442 2.456 2.417 2.388 2.379 2.  2 2.444 2.531 2.542 2.379 2.442 2.456 2.417 2.388 2.379 2.  3 2.287 2.239 2.209 2.167 2.222 2.253 2.226 2.265 2.167 2.  4 0.656 0.677 0.738 0.691 0.737 0.721 0.713 0.687 0.668 0.656 0.  5 0.705 0.710 0.741 0.737 0.721 0.713 0.687 0.668 0.656 0.  6 0.333 0.339 0.368 0.358 0.354 0.353 0.316 0.336 0.316 0.  6 0.333 0.339 0.368 0.358 0.354 0.353 0.316 0.336 0.316 0.  6 0.339 0.368 0.358 0.358 0.354 0.324 0.332 0.316 0.  9 0.159 0.157 0.174 0.163 L 0.146 0.149 0.154 0.149 0.  1 0.150 0.150 0.156 0.146 L L L L L L L L L L L L L L L L L L L	NO	u 7 6	51-0		ď	4	979 911				i	
0.0 46.0 90.0 136.0 180.0 226.0 270.0 316.0 MIN. ME 2.444 2.531 2.542 2.379 2.442 2.456 2.417 2.388 2.379 2. 2.287 2.239 2.209 2.167 2.222 2.253 2.226 2.265 2.167 2. 2.287 2.239 2.209 2.167 2.222 2.253 2.226 2.265 2.167 2. 0.656 0.677 0.738 0.691 0.700 0.668 0.670 0.668 0.656 0. 0.574 0.582 0.632 0.613 0.626 0.629 0.598 0.570 0.687 0. 0.333 0.339 0.368 0.358 0.354 0.353 0.316 0.336 0.316 0. 0.339 0.368 0.358 0.354 0.354 0.332 0.324 0. 0.159 0.157 0.174 0.163 L L L L L L L L L L L L L L L L L L L	AL N	00	0003		Z	s						
N) 0.0 46.0 90.0 136.0 180.0 226.0 270.0 316.0 MIN. ME  5 2.444 2.531 2.542 2.379 2.442 2.456 2.417 2.388 2.379 2. 0 2.287 2.239 2.209 2.167 2.222 2.253 2.226 2.265 2.167 2. 7 0.656 0.677 0.738 0.691 0.701 0.668 0.670 0.668 0.656 0. 7 0.656 0.677 0.738 0.691 0.701 0.668 0.670 0.668 0.656 0. 7 0.574 0.582 0.632 0.633 0.721 0.713 0.687 0.668 0.657 0. 8 0.337 0.348 0.368 0.358 0.354 0.353 0.316 0.336 0.316 0. 9 0.327 0.348 0.364 0.351 0.363 0.354 0.324 0.332 0.324 0. 9 0.327 0.348 0.366 0.368 0.358 0.354 0.324 0.332 0.316 0. 10 0.179 0.148 0.166 0.146 L 0.146 0.133 0.133 0.133 0.133 0. 10 0.179 0.148 0.166 0.146 L 0.146 0.133 0.133 0.134 0.147 0. 10 0.179 0.156 L L L L L L L L L L D 0.108 0.118 0.108 0. 11 0.120 L L L L L L L L L L L L L L L L L L L	TION				GREE	OCATIC	Z					
2 2.444 2.531 2.542 2.379 2.442 2.456 2.417 2.388 2.379 2.70 6.56 0.656 0.670 0.668 0.656 0.670 0.656 0.656 0.70 0.656 0.670 0.668 0.656 0.70 0.656 0.656 0.70 0.738 0.691 0.700 0.668 0.670 0.668 0.656 0.70 0.70 0.741 0.737 0.721 0.713 0.687 0.690 0.687 0.656 0.70 0.70 0.70 0.70 0.70 0.70 0.70 0.7	(Z	•	9	。	36.0	180.0	226.	70.	16.	MIN.	MEDIAN	
0 2.287 2.239 2.209 2.167 2.22 2.253 2.226 2.265 2.267 2.237 2.239 2.209 2.167 2.22 2.253 2.226 2.265 2.265 2.267 2.237 0.666 0.677 0.738 0.691 0.700 0.668 0.670 0.668 0.656 0.677 0.738 0.691 0.701 0.687 0.690 0.687 0.690 0.687 0.710 0.741 0.737 0.721 0.713 0.687 0.690 0.687 0.717 0.574 0.582 0.632 0.613 0.626 0.629 0.598 0.570 0.687 0.717 0.338 0.339 0.368 0.354 0.353 0.316 0.336 0.316 0.337 0.324 0.337 0.348 0.364 0.351 0.363 0.324 0.334 0.337 0.348 0.360 0.351 0.363 0.324 0.334 0.335 0.316 0.337 0.149 0.159 0.159 0.150 0.150 0.146 0.160 0.133 0.133 0.133 0.146 0.150	۳.	4 4	. 53	. 54	.37	4 4	4	4	بر و		•	
7 0.656 0.677 0.738 0.691 0.700 0.668 0.670 0.668 0.656 0.656 0.670 0.656 0.656 0.656 0.656 0.705 0.710 0.741 0.737 0.721 0.713 0.687 0.690 0.687 0.705 0.710 0.741 0.737 0.721 0.713 0.687 0.690 0.687 0.705 0.710 0.741 0.737 0.721 0.713 0.687 0.690 0.687 0.705 0.70	0.	8 7	. 23	. 20	. 16	. 22	. 25		, ,		, c	
.2 0.705 0.710 0.741 0.737 0.721 0.713 0.687 0.690 0.687 0.713 0.657 0.690 0.687 0.713 0.6582 0.632 0.613 0.626 0.629 0.598 0.570 0.6570 0.670 0.691 0.354 0.353 0.316 0.336 0.316 0.336 0.316 0.336 0.324 0.353 0.315 0.324 0.324 0.325 0.324 0.325 0.324 0.325 0.324 0.325 0.324 0.325 0.325 0.324 0.325 0.325 0.324 0.335 0.324 0.325 0.325 0.324 0.325 0.325 0.325 0.324 0.325 0.325 0.325 0.325 0.324 0.325 0	۲.	99	. 67	. 73	69	7.0		֓֞֜֜֜֜֝֓֜֜֝֓֓֓֓֓֜֜֜֜֓֓֓֓֓֡֜֜֜֡֓֓֓֡֓֜֜֜֡֓֓֡֓֡֡֡֡֡֓֡֓֡֡֡֡֡֡		94.		
.7 0.574 0.582 0.632 0.613 0.626 0.629 0.596 0.570 0.570 0.60 .6 0.333 0.339 0.368 0.358 0.354 0.353 0.316 0.336 0.316 0.336 .0 0.327 0.348 0.364 0.351 0.363 0.354 0.324 0.332 0.316 0.336 .0 0.327 0.348 0.364 0.351 0.363 0.354 0.324 0.332 0.324 0.335 .5 0.159 0.157 0.174 0.163 L 0.164 0.149 0.154 0.149 0.16 .0 0.179 0.148 0.166 0.146 L 0.146 0.133 0.133 0.133 0.146 .5 0.150 0.156 L L L L L L L L L D 0.159 0.147 0.147 0.16 .1 0.120 L L L L L L L L L L L L L L L L L L L	7.	0 2	71	74			5 -	• «	9 4		9	
0.333 0.339 0.368 0.358 0.354 0.353 0.316 0.336 0.316 0.336 0.339 0.368 0.358 0.354 0.353 0.316 0.336 0.316 0.337 0.327 0.348 0.364 0.351 0.363 0.354 0.353 0.336 0.336 0.316 0.337 0.327 0.348 0.364 0.351 0.363 0.354 0.353 0.324 0.324 0.326 0.169 0.165 0.146 0.146 0.133 0.133 0.133 0.136 0.36 0.316 0.366 0.366 0.366 0.366 0.366 0.366 0.366 0.366 0.366 0.366 0.366 0.366 0.366 0.37 0.645 0.364 0.364 0.363 0.136 0.	.7	74	. 58	63	. 61	6.5			. נ	9 1	7 ,	
0 0.327 0.348 0.364 0.351 0.363 0.354 0.324 0.332 0.354 0.355 0.357 0.645 0.350 0.357 0.357 0.645 0.350 0.357 0.357 0.645 0.504 0.504 0.553 0.357 0.558 0.558 0.535 0.512 0.697 0.537 0.645 0.504 0.504 0.537 0.457 0.355 0.355 0.355 0.357 0.645 0.504 0.504 0.504 0.537 0.457 0.357 0.457 0.357 0.457 0.357 0.457 0.357 0.457 0.357 0.457 0.357 0.457 0.357 0.457 0.357 0.457 0.357 0.457 0.357 0.457 0.357 0.457 0.357 0.457 0.357 0.457 0.357 0.457 0.35	9.	33		36	- C				, ,		0 1	
.5 0.159 0.157 0.174 0.163 L 0.164 0.149 0.154 0.155 0.157 0.149 0.163 L 0.164 0.149 0.154 0.154 0.148 0.166 0.146 L 0.146 0.133 0.133 0.143 0.135 0.146 0.179 0.156 L L L L D 0.159 0.147 0.147 0.167 0.150 0.150 L L L L L L D 0.159 0.147 0.147 0.167 0.151 0.150 0.150 L L L L L L L L L L L L L L L L L L L	.0	27	. 34	36	35	36			֓֞֜֝֜֝֓֓֞֜֝֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֓֡֓֓֓֓֡֓֡֓֡֓֡֓֡֓֡֡֡֓֡֓		* u	
0 0.179 0.148 0.166 0.146 L 0.146 0.133 0.133 0.143 0.145 0.146 0.156 L L L 0.159 0.147 0.143 0.145 0.150 0.156 L L L L 0.159 0.147 0.147 0.167 0.150 0.150 0.156 L L L L L 0.159 0.147 0.147 0.167 0.151 0.150 0.150 L L L L L L L L L L L L L L L L L L L	.5	59	. 15	.17	. 16		1 9	4			) +	
.5 0.150 0.156 L L L L D 0.159 0.147 0.147 0.16 .4 0.539 0.568 0.536 0.512 0.697 0.537 0.645 0.504 0.504 0.539 0.568 0.536 0.512 0.697 0.537 0.645 0.504 0.504 0.10 L L L L L L L L L L L L L L L L L L L	.0 0.	79	. 14	. 16	. 14	-1	14			: ~ :		
.4 0.539 0.568 0.536 0.512 0.697 0.537 0.645 0.504 0.534 0.535 0.108 0.118 0.108 0.131 0.120 L L L L L L L L L L L L L L L L L L L	.5 0.	20	. 15	-1		'n	J	1.5	14	7	7.	
.1 0.120 L L L L L L 0.108 0.118 0.108 0.13 .0 L L L L L L L L L L L L L L L L L L L	.4 0.	39	. 56	. 53	. 51	. 69	.53	64	50	. 2	. "	
.0	.1 0.	~	u	u	h		ы	10	111	10		
O L L L L L L L L L L L L L L L L L L L	٥.	ı	'n	ы	<b>.</b> 1	u	ы	'n	1	<u>.</u>	: -	
.8 L L L L L L L L L L L L L L L L L L L	0.	ב	u	בו	H	J	ı	ב, ו	نو ا	نه ۱	! -	
.8 L L L L L L L L L L L L L L L L L L L	∞.	ני	J		J	H	ı	ı 4	ם ו	ن. ا	: =	
OLL L L L L L L L L L L L L L L L L L L	∞.	ני	ы	ı	Ŋ	ı,ı	ŭ	· "i	ı µ1	1 🛋	: =	
L " INDICATES THAT LINER MATERIAL WAS REMAINING AT THAT LOCATION	0.	و		ы	ч	1	ב, ו	בן ו	1 -	1	<del>-</del> -	
TARLE A DELL'ARTER COM ACTUALITY THE PROPERTY OF THE PROPERTY		INDIC				ATERTA	3	2 2 2 2				
NIMUM VALUES WERE CALCHILLERS WERE CALCUIT.	MEDIA	N AND	MINI	, >	; v	•	4110	1011 041	4 2 F		. 2	Ç

TABLE 15 RSRM-7A FORWARD SEGMENT STAR TIP INSULATION PERFORMANCE

	PLANE		352.0	25						0.06				90.	54.	86.	54.	9	86.		54.	9	86.	54.	86.	90	22.	9	22.	86.	52.	99	866.	22.	52.	22.	54.	TATION
	MIM.		16.21	₹.	+	+	+	+	+	+	+	+	۲.	1.7	٦.	*	ų.	٥.	9.	9.	4	₹.		4.	80	2.71	٦.	7	٦.	S.	₹.	٦.	m.	٥.	₹.	€,	2.46	INCH STA
FACTOR (ASF)	352.0			₹.	+	+	+	+	+	+	+	+	+	+	۲.	6.	~	7	₩.	6.	Š	σ.	۲.	∞.	٦.	3.33	۳.	۳.	ŝ	σ.	7.	~	٠	۲.	∞.	₹.	m.	280.0
	LOCATIONS .0 286.0		18.62	0	+	+	+	+	+	+	<b>+</b>	+	+	+	25.0	4.4	3.9	3.0	7.6	3.1	2.9	2.4	2.5	2.7	2.8	Н	2.6	2.4	2.4	. 2.5	5.6	3.1	2.3	3.1	6.5	5.2	3.1	ЛТ ТНЕ
SAFETY	REE 222		16.42	12.3	+	+	+	+	+	+	+	+	+	+	10.1	4.7	4.3	3.7	2.7	4.4	2.8	3.2	2.5	2.7	9. O	0 2.74	2.1	3.0	2.1	7.6	5.9	4.7	2.9	3.0	3.4	7	2.7	= 2.14
ACTUAL	DEG 0 154.0		4 19.41	11.2	+	+	+	+	+	+	+	+	+	+	9.1	5.3	3.3	3.1	2.9	3.4	2.4	2.8	2.9	2.4	2.9	1 3.10	2.3	1 3.3	8 2.4	7 2.8	3 4.2	5 4.5	4 2.7	0 3.1	6 2.9	1 2.9	8 2.4	MINIMUM
	2		26.7	14.1	+	+	+	+	+	+	+	+	64.7	11.7	21.8	5.3	5.3	3.5	2.8	2.9	3.0	2.7	2.8	3.0	3.0	2.7	3.1	3.0	2.8	3.4	5.7	5.5	2.3	3.7	3.6	2.9	۳.	GMENT MI
	STATIO		3.5	m	۲.		4	7.	Ξ.	-		12.	5.	8.	52.	52.	75.	87.	99.	15.	24.	30.	36.	40.	51.	•	80.	93.	05.	12.	21.	30.	47.	59.	71.	83.	394.0	SEGR
	REQUIRED	•	٠	•	•	1.5	•	•		•	1.5	•	•	•		•	•	•	•		•					1.5	•	•	•	•	•	•	•	•	•	•	•	
	92.4	2	352.0	52.		_:	:		_:			_:	_:		54.	86.	54.	86.	٠.	90.	54.	86.	22.	54.	86.	~	22.	86.	22.	22.	52.	86.	86.	22.	52.	22.	54.	ATION
<b>.</b>	2		13.01	₹.	+	+	+	+	+	+	+	+	58.50		8.3	0	-	0	'n	9	~	4	m	7	٤,	2.55	۲.	ĸ.	₩.	۲.	Τ.	۰,	σ.	۲.	9.	4.	∹	ST
TOR (CSF)	•	. 70	13.01	7.47	+	+	+	+	+	+	+	+	+	+	24.38	6.1	'n	7		6	۳.	0	9		m	3.26	6.	7	۲.	4.	٦.	4	٥.	∞.	9	٦.	°.	80.0 S OCC
TY FACTOR	CATIONS	•	15.04	8.02	+	٠	+	+	+	+	+	+	+	+	22.64	3.0	4	0	'n			7	۳.	۰	٣.		٣.	۳.	٥,	٦,	4.	₩.	σ.	₩.	۳.	•	•	TH GOM
E SAFETY	EE LO	0.222	13.17	10.16	+	+	+	+	+	+	+	+	+	+		3		. 5	2 . 5	4	2 . 5	. m	2.3	2.5	2.4	7	1.7	2 . 8	1.8	2.1	5.7	2.7	2.5	2.7	3.1	7	2.3	= 1.71 AT EGLIGIBLE
COMPLIANCE	DE	154.0	15.36		+	+	+	+	. +	. +	+	+	. +	+	8 34		2 . 7	3.0	2.7	. m	2.2	2 . 8	2.6	2.1	2 . 3	m	1.9	3.1	1.9	2.3	4.1	2.5	2.2	2.8	2.8	2.6	2.1	MUM = S NEGL
COP	6	o .	1.2	10.83	+	+	+	. +	+	. +	+	. +	58.50	1.5	•	. «	ď	4		. 0			,	•	4	2.62	9	6	9	٥.	۳.	7	6	4	4	-	4.02	H MIN
	F :	(NI)	٠	•	7	•	4	-	_	. 4	4		4	4.8		•					. 4		9	0		263.0	0 8	. E	50	12.	21.	30.	47	5	71	8	46	. ŭ =

MATERIAL DECOMPOSITION RATE (MDR)

MATERIAL DECOMPOSITION DEPTH (MDD)

Α

			INCHE	S.							M	MILS / SI	SECOND			
STATION (IN)	90.06	DEGR 154.0	GREE LOC 0 222.0	LOCATIONS	s 352.0	MEDIAN	MAX.	DESIGN M+3S	STATION (IN)	0.06	DEGREE 154.0 222	ZZZ.0	LOCATIONS 2.0 286.0 3	352.0	AVE.	EXPOSURE
٠.	. 10	. 13	0.16	0.141	16	. 1.4	0.163	0.103	ις. Ε	2.9	4.0	4.7	4.1	4.7	4.1	34.5
13.0 0	090.	0.075	64	0.081	0.087	0.075	0	0.101	13.0	3.1			4.2	. 5		6
7	0	•	0	0	0	0	0	0.044	27.0	0	•	0	0	0	•	
•	0	•	0	•	0	0	0	.03	30.7	0	0	0	0	•	•	8.8
4.	0	•	•	0	0	0	•	٥.	34.2	0	0	•	0	0	0	
7.	0	0	0	0	0	0	0	٠.	37.7	•	0	0	0	0	0	•
Ξ.	0	0	0	•	0	0	•	0.023	41.2	0	0	•	•	0	•	
÷.	0	•	0	0	0	0	0	.01	•	0	0	0	0	0	•	
94.	0	0	0	0	0	0	0	٠	94.7	0	0	0	0	0	•	•
42.	0	0	•	0	0	0	0	.01	42.	0	0	0	0	0	•	
5.7	00.	0	•	0	0	•	0	.08	145.7	0.3	0	0	0	•	0.1	
48.5	. 02	0	0	00.	0	0	. 02	. 13		1.1	0	0	0	0	0.5	
52.0	. 01	.03	. 03	.01	.01	. 01	.03	.12	152.0	0.5	1.2	1.0	0.4	9.4	0.7	
62.	٠		0.158	0.179	0.089	0.142	-		~	•	2.4	2.7	•	1.5	2.4	₩.
75.5	. 13	. 21	. 16	. 17	. 17	. 17	. 21	. 32	175.5	1.5	2.4	1.9	7.0	1.9	1.9	89.3
87.0	. 18	. 21	. 17	. 21	. 19	. 19	. 21	. 39	87.	•		٠	•	1.9		02.
0.66	. 23	. 23	. 25	. 25	. 23	. 23	. 25	. 42	6	•	2.3	2.5	2.5	2.3		02.
15.0	. 21	. 19	. 14	. 20	. 16	. 19	. 21	. 42	15.	٠	•	•	٠			7
24.0	. 22	. 28	. 25	. 23	. 19	. 23	. 28	. 42	4.	٠	7.8	2.5	•		•	02.
30.0	. 22	. 22	. 19	. 25	. 20	. 22	. 25	.37	30.	•	٠		•	•	•	02.
36.0	. 21	. 21	. 25	. 24	. 22	. 22	. 25	. 32	36.	•	•		٠		٠	2
40.0	. 19	. 26	. 22	. 22	. 21	. 22	0.262	. 34	240.0	1.9	5.6	2.2	2.2	2.1	2.2	102.2
51.0	. 23	. 24	. 23	. 24	.17	. 23	. 24	. 31	51.	٠	•	•	•		٠	02.
63.0	. 21	. 18	. 22	. 19	. 17	. 19	. 22	. 33	63.	٠			٠	•	•	7
0.08	. 21	. 29	. 33	. 24	. 28	. 28	. 33	. 35	80.	•	2.9	٠	•	2.8	٠	02.
93.0	. 18	. 17	. 19	. 23	. 17	. 18	. 23	. 33	•	•	٠	•	•	1.7	•	02.
0.50	. 20	. 27	. 28	. 25	. 24	. 25	. 28	m.	05.	•	5.6		٠	٠	•	•
12.0	. 17	. 23	. 24	. 24	. 22	. 23	. 24	. 30	12.	1.7	2.3		٠	2.2	2.2	?
21.0	.17	. 22	. 15	. 17	. 29	. 17	. 29	. 43	21.	•	2.1	•	•	2.8	٠	04.
30.0	. 17	. 21	. 20	. 30	. 22	. 21	. 30	. 33		1.7	2.1	2.0	•	•	•	ς.
47.0	. 27	. 23	. 20	. 27	. 12	. 23		•	47.	2.7	2.3	2.1	•	1.3	٠	0
29.0	. 14	. 18	. 19	. 18	. 18	. 18	. 19	. 27	. 65	1.5	1.9	1.9	٠	1.8	1.8	6
71.0	. 15	. T	. 16	80.	. 19	. 16	. 19	30	7	1.6	1.9	1.8		2.1	•	95.2
83.0	. 18	. 19	. 20	. 10	. 16	. 1.8		7	383.0	1.9	2.0	2.1	1.1	1.7	1.8	
94.0	. 12	. 23	. 21	. 17	. 16	.17	m	. 28	9	1.3	2.4		1.8	1.7	1.9	0.86

" INDICATES THE PRECEDING MDD HAS EXCEEDED THE M + 3 SIGMA DESIGN CRITERIA

MOTOR ACTION TIME = 123.4 SECONDS

TABLE 15 RSRM-7A FORWARD SEGMENT STAR TIP INSULATION PERFORMANCE

STATION   NEDLAN   NEDLAN   NDT   NEDLAN   NDT   NEDLAN   NDT   NEDLAN   NDT   NEDLAN   NDT   NEDLAN   NDT	STATION   STAT	### STATION   PROPERE LOCATIONS   CONTRICT	19.   19.	52.					SERIAL	L NO. 0000003
643         2.626         2.644         2.120         3.5         2.574         2.631         2.485         2.486         2.480         2.480         2.480         2.480         2.480         2.480         2.480         2.480         2.480         2.480         0.731         0.731         0.727         0.732         0.737         0.737         0.727         0.737         0.7	2.643   2.626   2.644   2.120   3.5   2.574   2.541   2.483   2.485   2.480	1.0   1.0	1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,	2.64	E	IAN MD	₽ ~	DEGREE LOCATIONS 90.0 154.0 222.0 286.0 3	2.0 MI	. MEDIA
13.0   0.791   0.820   0.650   0.650   0.650   0.721   0.765   0.727   0.733   0.727   0.733   0.727   0.733   0.727   0.733   0.727   0.733   0.731   0.746   0.660	18.0   0.791   0.824   0.650   0.594   0.791   0.765   0.727   0.733   0.727   0.733   0.727   0.733   0.727   0.733   0.727   0.733   0.727   0.733   0.727   0.733   0.727   0.733   0.727   0.733   0.727   0.733   0.727   0.733   0.727   0.733   0.727   0.733   0.727   0.733   0.727   0.734   0.734   0.734   0.734   0.735   0.735   0.735   0.735   0.735   0.735   0.735   0.735   0.728	### 1971 0.751 0.752 0.753 0.7	0.131   0.131   0.132   0.132   0.132   0.131	•	.626 2.	44 2.12	m.	.574 2.541 2.483 2.485	480 2.4	0 2.48
410   0.416   0.416   0.400   34.2   L   L   L   L   L   L   L   L   L	111 0 0.416 0.416 0.400 34.2 L L L L L L L L L L L D 0.418 1.414 0.411 0.416 0	110 0 410 0	14.10	5.0	586	94 0.65	m r	.791 0.765 0.727 0.729	733 0.7	7 0.73
442         0.431         0.438         0.380         34.2         L	1442   0.431   0.438   0.340   34.2   L   L   L   L   L   L   L   L   L	441 0.441 0.448 0.300 344 1	441 0.441 0.448 0.380 344.2 L.	4.	.410 0.	16 0.40		3 14		
1341         0.337         0.341         0.337         0.341         0.339         37.7         L	134 0.233 0.244 0.230 441 0.330 33.7 L L L L L L L L L L L L L L L L L L L	141 0.137 0.341 0.130 4.1.2 L. C. 254 0.256 0.25	111 0.233 0.236 0.236 0.236 44.0 L L L L L L L L L L L L L L L L L L L	4	.431 0.	38 0.38	4	11		4.4
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	128 0.288 0.288 0.288 44.0 L L L L L L L L L L L C C 0.284 0.289 0.288 0.288 0.289 0.294 0.295 0.288 0.289 0.294 0.295 0.288 0.294 0.296 0.294 0.295 0.294 0.295 0	225 0.285 0.286 0.286 44.0 L L L L L L L L L L L L L L L L L L L	258 0.284 0.285 0.286 0.280 41.2 L L L L L L L L L L L L L L L L L L L	м. Т	.337 0.	41 0.33	۲.			.34
1.29         0.259         44.0         L <th< td=""><td>118 0.108 0.294 0.250 44.0 L L L L L L L L L L L L L L L L L L L</td><td>112 0.106 0.126 0.250 44.0 L L L L L L L L L L L L L L L L L L L</td><td>112 0.108 0.1284 0.250 44.0 L L L L L L L L L L L L L L L L L L L</td><td>2.</td><td>.283 0.</td><td>86 0.28</td><td>ä</td><td>น</td><td></td><td>. 28</td></th<>	118 0.108 0.294 0.250 44.0 L L L L L L L L L L L L L L L L L L L	112 0.106 0.126 0.250 44.0 L L L L L L L L L L L L L L L L L L L	112 0.108 0.1284 0.250 44.0 L L L L L L L L L L L L L L L L L L L	2.	.283 0.	86 0.28	ä	น		. 28
1,000	1166 0.161 0.1103 0.039 0 94.7 L L L L L L L L L L L L L L L L L L L	141. 0 1.10	16. 0.105		.289 0.	94 0.25	₹.	ว		. 29
269         0.259         0.266         0.234         145.0         L	142.0 0.255 0.266 0.213 145.0 L L L L L L L L L D 0.165 0.255 0.256 0.257 0.296 0.257 0.296 0.257 0.296 0.257 0.296 0.257 0.296 0.257 0.296 0.257 0.296 0.257 0.296 0.297 0.29	282 0.185 0.286 0.287 0.187 142.0 0.255 0.185 0.185 0.185 0.185 0.185 0.285 0.185 0.287 0.287 0.287 0.287 0.287 0.285 0.185 0.285 0.185 0.	222 0.285 0.286 0.287 0.287 142.7 0.285 0.315 0.32 0.386 0.315 0.285 0.315 0.287 0.287 0.285 0.315 0.385 0.315 0.3	7 -	161	0.0	4.	1 ·		. 10
262         0.281         0.282         0.274         1.727         0.252         0.131         0.252         0.131         0.252         0.131         0.252         0.131         0.225         0.144         0.444         0	181 0.281 0.282 0.277 148.5 0.252 0.312 0.325 0.315 0.325 0.315 0.325 0.315 0.325 0.315 0.325 0.315 0.326 0.336 0.444 0.444 0.444 0.444 0.444 0.444 0.444 0.443 0.656 0.663 0.663 0.663 0.663 0.663 0.663 0.663 0.663 0.663 0.663 0.663 0.663 0.663 0.633 0.442 0.442 0.442 0.443 0.452 0.444 0.444 0.444 0.444 0.444 0.442 0.442 0.451 0.433 0.452 0.444 0.444 0.444 0.444 0.444 0.442 0.442 0.451 0.443 0.452 0.444 0.444 0.444 0.444 0.442 0.443 0.464 0.444 0.444 0.444 0.444 0.442 0.444 0.442 0.464 0.444 0.442 0.444 0.442 0.441 0.441 0.441 0.444 0.442 0.442 0.441 0.441 0.441 0.444 0.442 0.442 0.441 0.441 0.444 0.444 0.444 0.444 0.442 0.441 0.	115. 0.281 0.282 0.274 1.42.7 0.252 0.215 0.245	115	7	259 0	11.0 69	. 7 F		, ,	0.16
348         0.346         0.348         0.348         0.317         152.0         0.533         0.312         0.326         0.529         0.533         0.537         0.536         0.549         0.513         0.529         0.613         0.549         0.513         0.549         0.513         0.549         0.513         0.549         0.513         0.549         0.513         0.549         0.613         0.613         0.620         0.612         0.639         0.613         0.621         0.639         0.614         0.445         0.445         0.467         0.447         0.447         0.447         0.447         0.447         0.447         0.447         0.447         0.447         0.447         0.447         0.447         0.447         0.447         0.447         0.447         0	748 0.346 0.348 0.317 152.0 0.337 0.309 0.312 0.336 0.339 0.239 0.233 0.348 0.346 0.348 0.317 0.641 0.641 0.641 0.641 0.641 0.641 0.641 0.641 0.641 0.641 0.641 0.641 0.641 0.641 0.642 0.612 0.563 0.512 0.515 0.549 0.613 0.643 0.643 0.643 0.642 0.442 0.443 0.444 0.444 0.444 0.444 0.444 0.641 0.641 0.641 0.641 0.641 0.641 0.642 0.442 0.443 0.443 0.442 0.444 0.444 0.444 0.444 0.444 0.643 0.663 0.663 0.639 0.639 0.639 0.639 0.639 0.639 0.639 0.639 0.639 0.642 0.426 0.436 0.643 0.650 0.639 0.	134 0 346 0 346 0 348 0 317 152.0 0 0313 0 000 0 0312 0 0315 0 0317 0 0 0317 0 0 0318 0 0 0314 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	148 0 346 0 347 0 153 0 137 152.0 0 1313 0 1310 0 1312 0 1315 0 1	. 28	.281 0.	82 0.27	. 4	185.0 255.0 C12.0 CC2.	7.0 61	0.31
706         0.756         0.757         0.547         162.0         0.620         0.612         0.595         0.617         0.595         0.613           720         0.642         0.718         0.640         175.5         0.583         0.513         0.515         0.549         0.513         0.549           641         0.643         0.640         187.0         0.473         0.429         0.444         0.444         0.443           645         0.643         0.643         187.0         0.475         0.413         0.429         0.428         0.444         0.444         0.453           645         0.643         0.643         187.0         0.478         0.464         0.433         0.428         0.464         0.428         0.444         0.444         0.464           601         0.643         0.643         187.0         0.478         0.464 <td>706         0.706         0.753         0.547         162.0         0.620         0.612         0.595         0.613         0.595         0.613         0.595         0.613         0.595         0.613         0.595         0.613         0.595         0.613         0.595         0.613         0.595         0.613         0.595         0.613         0.595         0.613         0.595         0.613         0.595         0.613         0.644         0.613         0.644         0.613         0.644         0.613         0.644         0.613         0.644         0.613         0.644         0.613         0.644         0.613         0.644         0.613         0.645         0.644         0.613         0.644         0.613         0.445         0</td> <td>706 0.706 0.733 0.547 162.0 0.622 0.612 0.559 0.607 0.513 0.513 0.514 0.444 0.</td> <td>706 0.706 0.733 0.547 162.0 0.622 0.612 0.559 0.607 0.513 0.525 0.617 0.539 0.617 0.641 0.644 0.649 0.639 0.640 0.639 0.640 0.639 0.649 0.659 0.</td> <td>. 34</td> <td>.346 0.</td> <td>48 0.31</td> <td>52</td> <td>333 0 300 0 312 0 326</td> <td>2.0 0.5 E. 0</td> <td>0.230</td>	706         0.706         0.753         0.547         162.0         0.620         0.612         0.595         0.613         0.595         0.613         0.595         0.613         0.595         0.613         0.595         0.613         0.595         0.613         0.595         0.613         0.595         0.613         0.595         0.613         0.595         0.613         0.595         0.613         0.595         0.613         0.644         0.613         0.644         0.613         0.644         0.613         0.644         0.613         0.644         0.613         0.644         0.613         0.644         0.613         0.644         0.613         0.645         0.644         0.613         0.644         0.613         0.445         0	706 0.706 0.733 0.547 162.0 0.622 0.612 0.559 0.607 0.513 0.513 0.514 0.444 0.	706 0.706 0.733 0.547 162.0 0.622 0.612 0.559 0.607 0.513 0.525 0.617 0.539 0.617 0.641 0.644 0.649 0.639 0.640 0.639 0.640 0.639 0.649 0.659 0.	. 34	.346 0.	48 0.31	52	333 0 300 0 312 0 326	2.0 0.5 E. 0	0.230
720         0.692         0.718         0.604         175.5         0.583         0.513         0.552         0.515         0.549         0.444         0.445         0.459         0.426         0.629         0.439         0.639         0.639         0.639         0.639         0.639         0.639         0.240         0.472         0.451         0.451         0.484         0.442         0.451         0.451         0.484         0.426         0.427         0.369         0.446         0.501         0.446         0.501         0.446         0.501         0.446         0.501         0.446         0.501         0.446         0.447         0	. 720 0.692 0.718 0.604 175.5 0.583 0.513 0.552 0.515 0.549 0.513 0.545 0.641 0.658 0.640 119.0 0.442 0.445 0.452 0.452 0.454 0.444 0.444 0.444 0.653 0.653 0.653 0.653 0.453 0.453 0.453 0.452 0.452 0.426 0.426 0.426 0.643 0.659 0.639 0.639 0.442 0.442 0.459 0.465 0.643 0.659 0.639 0.639 0.475 0.417 0.459 0.460 0.482	541 0 641 0 652 0 718 0 604 117.5 0 5.583 0 513 0 552 0 515 0 549 0 544 0 641 0 641 0 658 0 644 0 641 0 641 0 658 0 644 0 641 0 641 0 658 0 644 0 641	641 0 6491 0 718 0 604 1175. S 0 583 0 513 0 552 0 515 0 549 0 551 0 641	. 70	.706 0.	53 0.54	62.	.620 0.612 0.595 0.608 0	713	0.533 7.613
641         0.658         0.640         187.0         0.473         0.453         0.444         0.444         0.444         0.444         0.444         0.444         0.444         0.444         0.444         0.444         0.446         0	641         0.641         0.658         0.640         187.0         0.443         0.453         0.444         0.446         0.603         0.461         0.639         0.464         0.603         0.444         0.444         0.446         0.446         0.446         0.444         0.446         0.446         0.448         0.448         0.441         0.446         0.603         0.441         0.446         0	641 0.6641 0.684 0.640 0.640 187.0 0.4473 0.453 0.444 0.444 0.444 0.444 0.445 0.455 0.663 0.664 0.684 0.884	641 0.658 0.664 10.658 0.640 187.0 0.473 0.453 0.449 0.444 0.444 0.444 0.444 0.444 0.645 0.663 0.663 0.664 10.658 0.664 10.658 0.664 0.643 10.658 0.664 0.643 10.659 0.6	. 72	.692 0.	18 0.60	75.	.583 0.513 0.552 0.515 0	549 0.5	3 0 54
663         0.684         0.643         199.0         0.442         0.451         0.429         0.426         0.426         0.426         0.426         0.428         0.464         0.503         0.428         0.428         0.464         0.503         0.428         0.428         0.469         0.428         0.469         0.428         0.429         0.428         0.429         0.428         0.429         0.429         0.639         224.0         0.475         0.417         0.459         0.469         0.439         0.309         0.394         0.371         0.394         0.379         0.497           611         0.619         0.578         236.0         0.405         0.417         0.459         0.371         0.331         0.371         0.394         0.379         0.391         0.371         0.371         0.371         0.371         0.371         0.371         0.371         0.371         0.371         0.381         0.457         0.447         0.458         0.381         0.372         0.381         0.457         0.447         0.451         0.457         0.459         0.381         0.372         0.381         0.457         0.457         0.451         0.381         0.381         0.382         0.382         0.382 </td <td>0.663 0.664 0.643 0.684 0.643 199.0 0.442 0.451 0.433 0.426 0.426 0.426 0.448 0.645 0.645 0.650 0.653 0.650 0.639 0.650 0.442 0.475 0.454 0.503 0.451 0.482 0.462 0.462 0.462 0.657 0.659 0.650 0.639 0.639 0.600 0.441 0.628 0.650 0.639 0.639 0.400 0.407 0.417 0.459 0.460 0.484 0.369 0.400 0.611 0.611 0.619 0.578 0.578 0.407 0.412 0.427 0.369 0.460 0.394 0.371 0.391 0.391 0.391 0.599 0.599 0.568 0.568 0.568 0.568 0.407 0.411 0.372 0.381 0.385 0.388 0.372 0.38 0.588 0.588 0.588 0.588 0.588 0.588 0.568 0.568 0.568 0.568 0.568 0.568 0.568 0.568 0.568 0.568 0.568 0.568 0.568 0.568 0.568 0.568 0.574 0.372 0.391 0.391 0.391 0.391 0.391 0.591 0.588 0.588 0.588 0.588 0.588 0.568 0.568 0.568 0.568 0.568 0.568 0.574 0.392 0.389 0.387 0.400 0.380 0.401 0</td> <td>645 0.663 0.654 0.643 199.0 0.442 0.451 0.426 0.426 0.426 0.426 0.436 0.456 0.456 0.659 0.</td> <td>645 0.663 0.684 0.643 199.0 0.442 0.451 0.426 0.426 0.426 0.426 0.426 0.426 0.643 0.659 0.639 0.639 2.250 0.442 0.441 0.659 0.469 0.639 0.401 0.611 0.612 0.139 0.514 0.611 0.613 0.613 0.426 0.417 0.1391 0.391 0.417 0.513 0.421 0.310 0.418 0.417 0.1391 0.391 0.411 0.391 0.411 0.392 0.659 0.606 0.574 0.659 0.606 0.574 0.609 0.401 0.417 0.134 0.411 0.391 0.391 0.411 0.391 0.391 0.411 0.391 0.391 0.391 0.411 0.391 0.411 0.391 0.391 0.411 0.411 0.391 0.411 0.411 0.391 0.411 0.411 0.391 0.411</td> <td>.64</td> <td>.641 0.</td> <td>58 0.64</td> <td>87.</td> <td>.473 0.453 0.493 0.444 0</td> <td>444 0.4</td> <td>4 0.45</td>	0.663 0.664 0.643 0.684 0.643 199.0 0.442 0.451 0.433 0.426 0.426 0.426 0.448 0.645 0.645 0.650 0.653 0.650 0.639 0.650 0.442 0.475 0.454 0.503 0.451 0.482 0.462 0.462 0.462 0.657 0.659 0.650 0.639 0.639 0.600 0.441 0.628 0.650 0.639 0.639 0.400 0.407 0.417 0.459 0.460 0.484 0.369 0.400 0.611 0.611 0.619 0.578 0.578 0.407 0.412 0.427 0.369 0.460 0.394 0.371 0.391 0.391 0.391 0.599 0.599 0.568 0.568 0.568 0.568 0.407 0.411 0.372 0.381 0.385 0.388 0.372 0.38 0.588 0.588 0.588 0.588 0.588 0.588 0.568 0.568 0.568 0.568 0.568 0.568 0.568 0.568 0.568 0.568 0.568 0.568 0.568 0.568 0.568 0.568 0.574 0.372 0.391 0.391 0.391 0.391 0.391 0.591 0.588 0.588 0.588 0.588 0.588 0.568 0.568 0.568 0.568 0.568 0.568 0.574 0.392 0.389 0.387 0.400 0.380 0.401 0	645 0.663 0.654 0.643 199.0 0.442 0.451 0.426 0.426 0.426 0.426 0.436 0.456 0.456 0.659 0.	645 0.663 0.684 0.643 199.0 0.442 0.451 0.426 0.426 0.426 0.426 0.426 0.426 0.643 0.659 0.639 0.639 2.250 0.442 0.441 0.659 0.469 0.639 0.401 0.611 0.612 0.139 0.514 0.611 0.613 0.613 0.426 0.417 0.1391 0.391 0.417 0.513 0.421 0.310 0.418 0.417 0.1391 0.391 0.411 0.391 0.411 0.392 0.659 0.606 0.574 0.659 0.606 0.574 0.609 0.401 0.417 0.134 0.411 0.391 0.391 0.411 0.391 0.391 0.411 0.391 0.391 0.391 0.411 0.391 0.411 0.391 0.391 0.411 0.411 0.391 0.411 0.411 0.391 0.411 0.411 0.391 0.411	.64	.641 0.	58 0.64	87.	.473 0.453 0.493 0.444 0	444 0.4	4 0.45
645         0.650         0.639         215.0         0.428         0.464         0.503         0.451         0.484         0.428         0.467         0.469         0.639         0.600         0.340         0.341         0.341         0.341         0.341         0.341         0.341         0.341         0.341         0.371         0.391           699         0.704         0.568         251.0         0.411         0.467         0.467         0.457         0.473           699         0.704         0.568         263.0         0.370         0.389         0.387         0.406         0.370         0.389           699         0.564         0.568         280.0         0.454         0.392         0.389         0.387         0.466         0.370         0.389         0.381         0.381         0.389           653         0.563         0.568         25	0.645 0.643 0.650 0.639 215.0 0.428 0.464 0.503 0.451 0.482 0.428 0.466 0.647 0.659 0.639 0.639 224.0 0.475 0.417 0.459 0.460 0.484 0.417 0.466 0.611 0.613 0.539 0.639 234.0 0.407 0.412 0.429 0.460 0.394 0.379 0.407 0.611 0.611 0.619 0.578 236.0 0.407 0.412 0.437 0.384 0.371 0.391 0.371 0.399 0.599 0.606 0.574 240.0 0.411 0.372 0.381 0.385 0.394 0.372 0.388 0.599 0.606 0.574 0.568 251.0 0.473 0.481 0.467 0.467 0.457 0.372 0.388 0.588 0.568 0.568 251.0 0.473 0.481 0.467 0.467 0.457 0.398 0.372 0.388 0.588 0.568 0.568 280.0 0.370 0.396 0.389 0.387 0.406 0.370 0.388 0.457 0.406 0.370 0.389 0.551 0.552 0.552 0.552 0.370 0.389 0.400 0.400 0.389 0.327 0.399 0.568 0.568 0.568 0.568 0.568 0.568 0.568 0.568 0.568 0.568 0.568 0.380 0.400 0.333 0.327 0.399 0.370 0.399 0.391 0.525 0.391 0.327 0.391 0.389 0.391 0.582 0.591 0.591 0.591 0.591 0.591 0.591 0.591 0.591 0.591 0.591 0.591 0.591 0.591 0.591 0.591 0.391	0.643 0.650 0.639 2245.0 0.454 0.501 0.461 0.462 0.464 0.501 0.462 0.462 0.464 0.501 0.463 0.650 0.643 0.640 0.640 0.640 0.640 0.650 0.640 0.660 0.640 0.660 0.640 0.660 0.640 0.660 0.640 0.660 0.640 0.660 0.640 0.660 0.640 0.660 0.640 0.660 0.640 0.660 0.640 0.660 0.640 0.660 0.640 0.660 0.640 0.640 0.660 0.640 0.660 0.640 0.660 0.640 0.660 0.640 0.660 0.640 0.660 0.640 0.660 0.640 0.660 0.640 0.660 0.640 0.660 0.640 0.660 0.640 0.660 0.640 0.660 0.640	641 0.6673 0.6639 0.639 2240 0.468 0.5619 0.461 0.402 0.462 0.462 0.462 0.462 0.462 0.462 0.463 0.462 0.663	99.	.663 0.	84 0.64	99.	.442 0.451 0.433 0.429 0	426 0.4	6 0.43
224.0         0.475         0.417         0.459         0.484         0.417         0.459           601         0.628         0.639         224.0         0.475         0.417         0.427         0.369         0.369         0.407           601         0.628         0.639         0.578         230.0         0.405         0.417         0.369         0.394         0.369         0.407           611         0.699         0.606         0.574         240.0         0.411         0.372         0.381         0.371         0.372           699         0.704         0.568         251.0         0.411         0.457         0.529         0.457         0.459         0.457         0.379         0.370         0.470           580         0.580         0.568         263.0         0.370         0.380         0.380         0.461         0.460         0.370         0.470           581         0.565         0.546         259.0         0.470         0.414         0.383         0.327         0.383         0.381         0.379           563         0.565         0.546         0.526         0.380         0.400         0.383         0.379         0.383         0.378	224.0 0.475 0.465 0.484 0.417 0.456 0.601 0.6028 0.639 230.0 0.407 0.412 0.427 0.369 0.394 0.369 0.401 0.601 0.619 0.578 230.0 0.407 0.412 0.427 0.369 0.394 0.369 0.401 0.599 0.599 0.606 0.574 240.0 0.411 0.372 0.381 0.385 0.388 0.371 0.381 0.599 0.699 0.704 0.568 0.568 251.0 0.473 0.481 0.467 0.457 0.529 0.457 0.402 0.580 0.586 0.568 0.568 263.0 0.370 0.396 0.389 0.387 0.406 0.370 0.380 0.581 0.582 0.568 0.568 280.0 0.441 0.383 0.377 0.406 0.370 0.380 0.599 0.694 0.568 0.568 280.0 0.454 0.382 0.387 0.406 0.370 0.380 0.599 0.695 0.651 0.525 3050 0.440 0.423 0.406 0.393 0.327 0.381 0.582 0.618 0.651 0.525 3050 0.440 0.423 0.406 0.390 0.430 0.333 0.379 0.999 0.950 0.964 0.918 312.0 0.440 0.423 0.406 0.390 0.431 0.708 0.708 0.999 0.950 0.951 0.551 330.0 0.782 0.758 0.760 0.653 0.756 0.653 0.756 0.556 0.556 0.551 0.574 0.392 0.411 0.356 0.466 0.356 0.356 0.356 0.356 0.356 0.358 0.359 0.390 0.414 0.395 0.389 0.389 0.381 0.389 0	601 0.601 0.628 0.839 224.0 0.445 0.412 0.427 0.369 0.344 0.369 0.417 0.466 0.484 0.369 0.349 0.549 0.601 0.601 0.601 0.628 0.639 0.639 0.400 0.417 0.369 0.394 0.369 0.394 0.369 0.394 0.599 0.606 0.574 0.574 0.405 0.417 0.384 0.371 0.391 0.391 0.391 0.391 0.599 0.606 0.574 0.568 0.606 0.407 0.481 0.467 0.487 0.386 0.372 0.386 0.372 0.398 0.699 0.704 0.568 0.568 0.568 0.568 0.481 0.473 0.481 0.467 0.497 0.	0.417 0.459 0.461 0.629 0.639 224.0 0.447 0.459 0.484 0.369 0.491 0.641	40.	.643 0.	50 0.63	15.	.428 0.464 0.503 0.451 0	482 0.4	8 0.46
10         10<	236.0 0.401 0.629 0.394 0.369 0.369 0.369 0.369 0.369 0.369 0.361 0.611 0.613	611 0.611 0.619 0.578 230.0 0.400 0.410 0.359 0.359 0.400 0.450 0.410 0.611 0.611 0.619 0.578 230.0 0.400 0.450 0.359 0.505 0.359 0.505 0.359 0.505 0.359 0.505 0.359 0.505 0.359 0.505 0.350 0.505 0.505 0.505 0.505 0.351 0.371 0.371 0.372 0.385 0.385 0.385 0.387 0.405 0.589 0.589 0.589 0.589 0.589 0.589 0.387 0.405 0.390 0.589 0.589 0.589 0.589 0.387 0.405 0.390 0.390 0.390 0.390 0.590 0.599 0.590 0.505 0.505 0.505 0.505 0.300 0.370 0.414 0.389 0.387 0.405 0.390 0.390 0.405 0.585 0.505 0.505 0.505 0.505 0.500 0.370 0.400 0.390 0.401 0.400 0.390 0.401 0.400 0.390 0.401 0.400 0.390 0.401 0.400 0.390 0.401 0.400 0.390 0.401 0.400 0.390 0.401 0.400 0.390 0.401 0.400 0.390 0.401 0.400 0.390 0.401 0.400 0.390 0.401 0.400 0.390 0.401 0.390 0.401 0.390 0.401 0.390 0.401 0.390 0.401 0.390 0.401 0.390 0.401 0.390 0.401 0.390 0.390 0.390 0.401 0.390 0.401 0.390 0.	240.0 0.407 0.417 0.428 0.599 0.600 0.605 0.407 0.417 0.427 0.427 0.359 0.409 0.409 0.409 0.409 0.409 0.409 0.409 0.409 0.409 0.599 0.606 0.574 2260.0 0.401 0.407 0.438 0.381 0.391 0.391 0.371 0.398 0.599 0.606 0.574 2260.0 0.401 0.401 0.467 0.401 0.40	9	.6/1/ 0.	99 0.63	24.	.475 0.417 0.459 0.460 0	484 0.4	7 0.46
1.59         0.51         0.391         0.371         0.39           1.59         0.599         0.606         0.574         240.0         0.411         0.372         0.381         0.372         0.38           1.599         0.599         0.606         0.574         240.0         0.411         0.372         0.381         0.372         0.382           1.580         0.580         0.568         251.0         0.370         0.389         0.467         0.459         0.466         0.370         0.380           1.688         0.568         0.568         280.0         0.414         0.389         0.401         0.401         0.401         0.401         0.401         0.401         0.401         0.401         0.380         0.401         0.402         0.384         0.392         0.392         0.393         0.393         0.393         0.393         0.393         0.393         <	236.0 0.556 0.556 0.574 240.0 0.411 0.372 0.381 0.371 0.391 0.371 0.399 0.599 0.606 0.574 240.0 0.411 0.372 0.381 0.385 0.388 0.372 0.381 0.589 0.704 0.568 251.0 0.473 0.481 0.385 0.385 0.388 0.372 0.381 0.580 0.589 0.704 0.568 251.0 0.473 0.389 0.387 0.457 0.457 0.457 0.457 0.458 0.589 0.568 0.568 253.0 0.370 0.389 0.387 0.459 0.457 0.406 0.380 0.401 0.400 0.380 0.401 0.400 0.381 0.387 0.558 0.563 0.565 0.546 293.0 0.477 0.414 0.383 0.327 0.393 0.327 0.38 0.387 0.581 0.582 0.565 0.546 293.0 0.470 0.414 0.383 0.379 0.433 0.327 0.388 0.401 0.402 0.389 0.404 0.588 0.559 0.555 0.561 0.571 0.383 0.399 0.411 0.356 0.466 0.389 0.411 0.356 0.466 0.389 0.391 0	599 0.599 0.704 0.568 0.411 0.372 0.381 0.386 0.377 0.395 0.377 0.395 0.377 0.395 0.599 0.599 0.606 0.574 240.0 0.411 0.372 0.381 0.386 0.377 0.375 0.395 0.599 0.699 0.704 0.568 0.568 260.0 0.471 0.491 0.467 0.467 0.457 0.457 0.481 0.589 0.699 0.704 0.568 0.568 0.568 0.644 0.382 0.389 0.387 0.395 0.389 0.599 0.599 0.598 0.568 0.568 0.545 0.389 0.387 0.392 0.387 0.395 0.569 0.565 0.565 0.565 0.565 0.546 0.392 0.387 0.392 0.387 0.399 0.491 0.400 0.339 0.327 0.399 0.491 0.400 0.339 0.327 0.399 0.491 0.582 0.561 0.541 0.582 0.565 0.545 0.551 0.541 0.582 0.380 0.400 0.431 0.392 0.399 0.491 0.400 0.399 0.492 0.399 0.491 0.399 0.490 0.490 0.490 0.490 0.490 0.490 0.490 0.490 0.490 0.490 0.490 0.490 0.390 0.490 0.490 0.490 0.490 0.390 0.490 0.490 0.390 0.490 0.490 0.390 0.490 0.490 0.390 0.490 0.490 0.390 0.490 0.490 0.390 0.490 0.390 0.490 0.390 0.490 0.490 0.390 0.490 0.490 0.390 0.490 0.390 0.490 0.490 0.390 0.490 0.490 0.390 0.490 0.490 0.390 0.490 0.390 0.490 0.390 0.490 0.390 0.490 0.390 0.490 0.390 0.490 0.390 0.490 0.390 0.390 0.490 0.390 0.390 0.490 0.390 0.490 0.390 0.390 0.490 0.390 0.490 0.390 0.490 0.390 0.490 0.390 0.490 0.390 0.390 0.490 0.390 0.490 0.390 0.490 0.390 0.490 0.390 0.490 0.390 0.490 0.390 0.490 0.390 0.490 0.390 0.490 0.390 0.490 0.390 0.390 0.490 0.390 0.490 0.390 0.490 0.390 0.490 0.390 0.390 0.490 0.390 0.490 0.390 0.490 0.390 0.390 0.490 0.390 0.490 0.390 0.390 0.490 0.390 0.490 0.390 0.390 0.490 0.390 0.390 0.490 0.390 0.390 0.490 0.390 0.390 0.490 0.390 0.390 0.490 0.390 0.	599 0.599 0.606 0.574 240.0 0.4412 0.372 0.381 0.391 0.371 0.395 0.572 0.599 0.599 0.606 0.574 0.450 0.474 0.372 0.372 0.391 0.372 0.391 0.372 0.391 0.372 0.391 0.372 0.391 0.372 0.599 0.606 0.574 0.568 0.568 0.606 0.370 0.473 0.481 0.372 0.381 0.385 0.386 0.372 0.391 0.372 0.391 0.590 0.606 0.589 0.606 0.589 0.606 0.589 0.606 0.589 0.606 0.390 0.495 0.485 0.386 0.406 0.390 0.390 0.490 0.588 0.568 0.568 0.606 0.406 0.392 0.380 0.400 0.390 0.490 0.390 0.490 0.390 0.490 0.390 0.490 0.590 0.590 0.590 0.590 0.590 0.490 0.390 0.490 0.390 0.390 0.390 0.390 0.390 0.990 0.991 0.525 0.525 0.918 0.320 0.400 0.390 0.490 0.700 0.390 0.390 0.490 0.991 0.390 0.991 0		.601	26 0.63	30.	.407 0.412 0.427 0.369 0	394 0.3	9 0.40
259         0.599         0.704         0.568         251.0         0.473         0.481         0.457         0.529         0.457         0.382         0.372         0.382           699         0.704         0.568         251.0         0.473         0.467         0.457         0.457         0.47           688         0.568         0.568         280.0         0.454         0.380         0.401         0.406         0.380         0.401           688         0.564         0.568         280.0         0.454         0.380         0.401         0.401         0.401           631         0.563         0.546         293.0         0.377         0.401         0.393         0.327         0.383           651         0.546         0.955         0.360         0.400         0.400         0.400         0.400         0.400         0.390         0.410         0.383         0.390         0.410           651         0.964         0.918         312.0         0.402         0.794         0.708         0.794         0.708         0.793           949         0.957         0.918         330.0         0.742         0.794         0.708         0.708         0.798 <t< td=""><td>251.0 0.472 0.385 0.388 0.372 0.38 </td><td>699 0.699 0.700 0.544 251.0 0.4411 0.435 0.481 0.465 0.372 0.388 0.372 0.388 0.699 0.699 0.700 0.594 0.568 251.0 0.441 0.435 0.481 0.465 0.599 0.704 0.568 0.568 280.0 0.441 0.456 0.389 0.387 0.406 0.340 0.589 0.599 0.704 0.568 0.568 0.568 0.568 0.568 0.568 0.569 0.372 0.399 0.400 0.431 0.405 0.389 0.387 0.400 0.387 0.400 0.431 0.559 0.559 0.555 0.556 0.546 0.594 0.397 0.393 0.337 0.400 0.372 0.399 0.559 0.559 0.555 0.546 0.541 0.393 0.393 0.337 0.399 0.414 0.388 0.399 0.430 0.390 0.390 0</td><td>699 0.699 0.704 0.564 251.0 0.471 0.475 0.481 0.467 0.457 0.537 0.538 0.377 0.538 0.599 0.699 0.704 0.568 251.0 0.473 0.481 0.467 0.457 0.529 0.457 0.598 0.598 0.704 0.568 251.0 0.473 0.481 0.467 0.457 0.459 0.387 0.599 0.704 0.568 0.568 0.568 0.573 0.414 0.481 0.461 0.400 0.437 0.400 0.582 0.562 0.568 0.568 0.570 0.474 0.383 0.327 0.499 0.582 0.561 0.552 0.562 0.544 0.392 0.401 0.</td><td></td><td>.0.110.</td><td>70.0 61</td><td>99</td><td>405 0.417 0.384 0.371 0</td><td>391 0.3</td><td>1 0.39</td></t<>	251.0 0.472 0.385 0.388 0.372 0.38	699 0.699 0.700 0.544 251.0 0.4411 0.435 0.481 0.465 0.372 0.388 0.372 0.388 0.699 0.699 0.700 0.594 0.568 251.0 0.441 0.435 0.481 0.465 0.599 0.704 0.568 0.568 280.0 0.441 0.456 0.389 0.387 0.406 0.340 0.589 0.599 0.704 0.568 0.568 0.568 0.568 0.568 0.568 0.569 0.372 0.399 0.400 0.431 0.405 0.389 0.387 0.400 0.387 0.400 0.431 0.559 0.559 0.555 0.556 0.546 0.594 0.397 0.393 0.337 0.400 0.372 0.399 0.559 0.559 0.555 0.546 0.541 0.393 0.393 0.337 0.399 0.414 0.388 0.399 0.430 0.390 0.390 0	699 0.699 0.704 0.564 251.0 0.471 0.475 0.481 0.467 0.457 0.537 0.538 0.377 0.538 0.599 0.699 0.704 0.568 251.0 0.473 0.481 0.467 0.457 0.529 0.457 0.598 0.598 0.704 0.568 251.0 0.473 0.481 0.467 0.457 0.459 0.387 0.599 0.704 0.568 0.568 0.568 0.573 0.414 0.481 0.461 0.400 0.437 0.400 0.582 0.562 0.568 0.568 0.570 0.474 0.383 0.327 0.499 0.582 0.561 0.552 0.562 0.544 0.392 0.401 0.		.0.110.	70.0 61	99	405 0.417 0.384 0.371 0	391 0.3	1 0.39
55.0         6.55.9         6.56.8         25.1.0         6.47.1         6.46.1         6.45.7         6.45.7         6.47.7         6.47.7         6.47.7         6.47.7         6.47.7         6.47.7         6.47.7         6.48.8         6.37.9         6.37.9         6.38.9         6.38.9         6.38.7         6.40.6         6.38.0         6.38.0         6.40.3         6.38.0         6.40.0         6.38.0         6.38.0         6.40.0         6.38.3         6.38.3         6.38.7         6.38.3 <td>25.0 0.580 0.585 0.568 263.0 0.370 0.387 0.405 0.457 0.477 0.477 0.580 0.580 0.586 0.568 263.0 0.370 0.380 0.387 0.406 0.370 0.380 0.589 0.589 0.568 0.568 280.0 0.370 0.380 0.401 0.400 0.380 0.401 0.380 0.401 0.380 0.401 0.380 0.387 0.401 0.380 0.401 0.380 0.387 0.401 0.380 0.380 0.401 0.380 0.380 0.401 0.380 0.380 0.390 0.380 0.390 0.380 0.390 0.380 0.390 0.401 0.580 0.590 0.401 0.551 0.551 0.551 0.551 0.360 0.402 0.380 0.392 0.392 0.390 0.414 0.389 0.395 0.395 0.390 0.401 0.380 0.390 0.401 0.380 0.390 0.401 0.380 0.390 0.401 0.380 0.390 0.401 0.380 0.390 0.401 0.380 0.390 0.401 0.380 0.390 0.401 0.380 0.390 0.401 0.380 0.390 0.401 0.380 0.390 0.401 0.380 0.390 0.401 0.380 0.390 0.401 0.380 0.390 0.390 0.401 0.390 0</td> <td>580 0.580 0.585 0.568 263.0 0.370 0.386 0.387 0.405 0.387 0.405 0.387 0.405 0.387 0.405 0.387 0.405 0.387 0.405 0.387 0.405 0.387 0.405 0.387 0.405 0.387 0.405 0.387 0.405 0.387 0.388 0.644 0.688 0.568 280.0 0.454 0.392 0.386 0.401 0.401 0.400 0.383 0.593 0.555 0.568 0.568 280.0 0.454 0.392 0.380 0.401 0.401 0.400 0.393 0.527 0.393 0.595 0.565 0.545 0.565 0.545 0.305 0.040 0.333 0.397 0.393 0.393 0.395 0.565 0.568 0.565 0.568 0.565 0.568 0.561 0.541 0.525 0.380 0.440 0.420 0.400 0.333 0.397 0.393 0.393 0.395 0.595 0.957 0.965 0.967 0.</td> <td>580 0.580 0.585 0.568 251.0 0.370 0.396 0.387 0.405 0.370 0.386 0.588 0.568 0.568 251.0 0.370 0.396 0.387 0.406 0.370 0.386 0.558 0.569 0.370 0.396 0.387 0.400 0.337 0.400 0.397 0.327 0.337 0.327 0.337 0.327 0.337 0.</td> <td>ָר ער היי</td> <td>. 0 666.</td> <td>70.0 90</td> <td>4 n</td> <td>473 6 464 6 465 6 467 6 467 6</td> <td>388 0.3</td> <td>2 0.38</td>	25.0 0.580 0.585 0.568 263.0 0.370 0.387 0.405 0.457 0.477 0.477 0.580 0.580 0.586 0.568 263.0 0.370 0.380 0.387 0.406 0.370 0.380 0.589 0.589 0.568 0.568 280.0 0.370 0.380 0.401 0.400 0.380 0.401 0.380 0.401 0.380 0.401 0.380 0.387 0.401 0.380 0.401 0.380 0.387 0.401 0.380 0.380 0.401 0.380 0.380 0.401 0.380 0.380 0.390 0.380 0.390 0.380 0.390 0.380 0.390 0.401 0.580 0.590 0.401 0.551 0.551 0.551 0.551 0.360 0.402 0.380 0.392 0.392 0.390 0.414 0.389 0.395 0.395 0.390 0.401 0.380 0.390 0.401 0.380 0.390 0.401 0.380 0.390 0.401 0.380 0.390 0.401 0.380 0.390 0.401 0.380 0.390 0.401 0.380 0.390 0.401 0.380 0.390 0.401 0.380 0.390 0.401 0.380 0.390 0.401 0.380 0.390 0.401 0.380 0.390 0.401 0.380 0.390 0.390 0.401 0.390 0	580 0.580 0.585 0.568 263.0 0.370 0.386 0.387 0.405 0.387 0.405 0.387 0.405 0.387 0.405 0.387 0.405 0.387 0.405 0.387 0.405 0.387 0.405 0.387 0.405 0.387 0.405 0.387 0.405 0.387 0.388 0.644 0.688 0.568 280.0 0.454 0.392 0.386 0.401 0.401 0.400 0.383 0.593 0.555 0.568 0.568 280.0 0.454 0.392 0.380 0.401 0.401 0.400 0.393 0.527 0.393 0.595 0.565 0.545 0.565 0.545 0.305 0.040 0.333 0.397 0.393 0.393 0.395 0.565 0.568 0.565 0.568 0.565 0.568 0.561 0.541 0.525 0.380 0.440 0.420 0.400 0.333 0.397 0.393 0.393 0.395 0.595 0.957 0.965 0.967 0.	580 0.580 0.585 0.568 251.0 0.370 0.396 0.387 0.405 0.370 0.386 0.588 0.568 0.568 251.0 0.370 0.396 0.387 0.406 0.370 0.386 0.558 0.569 0.370 0.396 0.387 0.400 0.337 0.400 0.397 0.327 0.337 0.327 0.337 0.327 0.337 0.	ָר ער היי	. 0 666.	70.0 90	4 n	473 6 464 6 465 6 467 6 467 6	388 0.3	2 0.38
688         0.568         280.0         0.454         0.387         0.406         0.310         0.38           563         0.564         0.568         0.568         280.0         0.454         0.380         0.401         0.406         0.387         0.414         0.383         0.327         0.380         0.400         0.401         0.401         0.383         0.327         0.380         0.401         0.401         0.383         0.327         0.380         0.401         0.383         0.387         0.383         0.383         0.387         0.383         0.383         0.383         0.387         0.383         0.383         0.387         0.380         0.410         0.402         0.406         0.390         0.431         0.390         0.413         0.390         0.413         0.390         0.423         0.406         0.406         0.760         0.653         0.756         0.766 <td>68 0.659 0.568 0.568 280.0 0.454 0.389 0.387 0.400 0.318 0.310 0.318 0.658 0.664 0.668 0.568 293.0 0.454 0.389 0.387 0.400 0.319 0.327 0.318 0.559 0.565 0.565 0.546 293.0 0.454 0.383 0.327 0.313 0.327 0.318 0.559 0.651 0.565 0.546 293.0 0.400 0.333 0.379 0.383 0.327 0.318 0.565 0.661 0.661 0.661 0.541 312.0 0.440 0.426 0.394 0.794 0.794 0.794 0.794 0.798 0.798 0.798 0.799 0.949 0.957 0.551 330.0 0.412 0.782 0.756 0.794 0.794 0.796 0.798 0.799 0.949 0.957 0.551 330.0 0.782 0.782 0.756 0.653 0.726 0.356 0.356 0.356 0.356 0.356 0.356 0.356 0.356 0.356 0.356 0.356 0.356 0.356 0.356 0.356 0.356 0.356 0.358 0.391 0.378 0.392 0.392 0.393 0.393 0.393 0.393 0.395 0.3</td> <td>688 0.644 0.688 0.568 280.0 0.579 0.379 0.379 0.387 0.400 0.387 0.400 0.386 0.464 0.688 0.568 280.0 0.387 0.414 0.388 0.464 0.688 0.568 280.0 0.387 0.414 0.389 0.401 0.401 0.401 0.389 0.387 0.414 0.389 0.401 0.</td> <td>688 0.644 0.688 0.568 280.0 0.357 0.357 0.357 0.357 0.357 0.357 0.358 0.568 0.564 0.568 0.568 0.568 0.568 0.568 0.568 0.357 0.357 0.357 0.357 0.358 0.357 0.358 0.357 0.358 0.357 0.358 0.357 0.358 0.357 0.358 0.357 0.358 0.357 0.358 0.</td> <td>ָ ֓֞֝֝֞֜֝֝֝֓֞֝֝֞֝֝֞֝֞֝</td> <td>. 0</td> <td></td> <td></td> <td>.4/3 U.481 U.46/ U.45/ U</td> <td>529 0.4</td> <td>7 0.47</td>	68 0.659 0.568 0.568 280.0 0.454 0.389 0.387 0.400 0.318 0.310 0.318 0.658 0.664 0.668 0.568 293.0 0.454 0.389 0.387 0.400 0.319 0.327 0.318 0.559 0.565 0.565 0.546 293.0 0.454 0.383 0.327 0.313 0.327 0.318 0.559 0.651 0.565 0.546 293.0 0.400 0.333 0.379 0.383 0.327 0.318 0.565 0.661 0.661 0.661 0.541 312.0 0.440 0.426 0.394 0.794 0.794 0.794 0.794 0.798 0.798 0.798 0.799 0.949 0.957 0.551 330.0 0.412 0.782 0.756 0.794 0.794 0.796 0.798 0.799 0.949 0.957 0.551 330.0 0.782 0.782 0.756 0.653 0.726 0.356 0.356 0.356 0.356 0.356 0.356 0.356 0.356 0.356 0.356 0.356 0.356 0.356 0.356 0.356 0.356 0.356 0.358 0.391 0.378 0.392 0.392 0.393 0.393 0.393 0.393 0.395 0.3	688 0.644 0.688 0.568 280.0 0.579 0.379 0.379 0.387 0.400 0.387 0.400 0.386 0.464 0.688 0.568 280.0 0.387 0.414 0.388 0.464 0.688 0.568 280.0 0.387 0.414 0.389 0.401 0.401 0.401 0.389 0.387 0.414 0.389 0.401 0.	688 0.644 0.688 0.568 280.0 0.357 0.357 0.357 0.357 0.357 0.357 0.358 0.568 0.564 0.568 0.568 0.568 0.568 0.568 0.568 0.357 0.357 0.357 0.357 0.358 0.357 0.358 0.357 0.358 0.357 0.358 0.357 0.358 0.357 0.358 0.357 0.358 0.357 0.358 0.	ָ ֓֞֝֝֞֜֝֝֝֓֞֝֝֞֝֝֞֝֞֝	. 0			.4/3 U.481 U.46/ U.45/ U	529 0.4	7 0.47
563         0.563         0.565         0.565         0.566         0.546         293.0         0.377         0.414         0.383         0.327         0.380         0.400         0.383         0.327         0.380         0.383         0.327         0.383         0.390         0.440         0.402         0.403         0.404         0.704         0.708         0.708         0.793         0.708         0.793         0.708         0.708         0.793         0.708         0	563 0.559 0.565 0.546 293.0 0.377 0.414 0.383 0.327 0.389 0.387 0.389 0.387 0.389 0.480 0.480 0.480 0.480 0.389 0.389 0.399 0.489 0.964 0.918 312.0 0.440 0.426 0.794 0.794 0.708 0.708 0.708 0.799 0.949 0.957 0.551 330.0 0.782 0.782 0.766 0.653 0.726 0.399 0.799 0.999 0.999 0.957 0.523 347.0 0.389 0.399 0.411 0.356 0.466 0.356 0.399 0.399 0.414 0.389 0.399 0.414 0.399 0.399 0.399 0.399 0.399 0.414 0.399 0.	563 0.559 0.565 0.546 293.0 0.377 0.414 0.383 0.327 0.393 0.327 0.389 0.327 0.389 0.565 0.565 0.546 293.0 0.377 0.414 0.383 0.327 0.393 0.327 0.389 0.327 0.389 0.565 0.565 0.565 0.546 0.541 0.525 30.5.0 0.340 0.430 0.337 0.393 0.337 0.398 0.327 0.398 0.565 0.561 0.561 0.561 0.541 312.0 0.440 0.423 0.439 0.397 0.393 0.399 0.400 0.399 0.950 0.967 0.967 0.963 0.390 0.430 0.726 0	563 0.559 0.565 0.546 293.0 0.737 0.414 0.383 0.327 0.393 0.327 0.486 0.559 0.565 0.546 293.0 0.737 0.414 0.383 0.327 0.393 0.337 0.395 0.546 0.395 0.	9 9	644		? «	.3/0 0.396 0.389 0.38/ 0	406 0.3	0 0.38
631         0.582         0.631         0.525         305.0         0.380         0.402         0.333         0.333         0.333         0.333         0.333         0.383         0.333         0.383         0.333         0.383         0.383         0.383         0.383         0.383         0.390         0.390         0.390         0.390         0.390         0.390         0.390         0.390         0.390         0.390         0.708         0.793         0.708         0.793         0.708         0.793         0.708         0.793         0.708         0.793         0.708         0.793         0.708         0.793         0.708         0.793         0.708         0.793         0.708         0.793         0.708         0.793         0.708         0.793         0.708         0.793         0.708         0.753         0.756         0.753         0.756         0	651 0.582 0.631 0.525 305.0 0.387 0.402 0.333 0.379 0.383 0.333 0.387 0.485 0.651 0.651 0.541 312.0 0.440 0.423 0.406 0.339 0.383 0.390 0.436 0.950 0.964 0.918 312.0 0.440 0.423 0.406 0.390 0.430 0.390 0.425 0.959 0.957 0.951 312.0 0.4819 0.726 0.794 0.794 0.708 0.708 0.795 0.394 0.957 0.951 330.0 0.782 0.782 0.756 0.794 0.794 0.708 0.708 0.795 0.394 0.594 0.628 0.523 347.0 0.363 0.399 0.411 0.356 0.466 0.356 0.395 0	631 0.582 0.631 0.525 305.0 0.380 0.400 0.333 0.379 0.383 0.389 0.400 0.381 0.525 0.531 0.525 0.531 0.525 0.531 0.525 0.531 0.525 0.541 0.541 0.541 0.541 0.440 0.423 0.406 0.390 0.430 0.393 0.389 0.950 0.954 0.918 0.312.0 0.440 0.423 0.406 0.390 0.430 0.390 0.420 0.9949 0.956 0.951 0.918 0.312.0 0.708 0.708 0.709 0.7	631 0.582 0.631 0.525 305.0 0.380 0.400 0.333 0.379 0.383 0.333 0.399 0.383 0.399 0.5090 0.500 0	. 56	.559 0.	55 0.54		0 1010 0010 7610 1110 0 1110 0 1110 0 1110 0 1110 0 1110 0 1110 0 1110 0 1110 0 1110 0 1110 0 1110 0 1110 0 11	400	0.4.0
651         0.618         0.651         0.541         312.0         0.440         0.423         0.406         0.390         0.430         0.390         0.430         0.430         0.430         0.430         0.430         0.430         0.430         0.430         0.430         0.430         0.430         0.443         0.708         0	.651 0.618 0.651 0.541 312.0 0.440 0.423 0.406 0.390 0.430 0.390 0.430 0.430 0.430 0.959 0.964 0.918 321.0 0.819 0.726 0.794 0.794 0.708 0.708 0.708 0.795 0.949 0.957 0.551 330.0 0.782 0.782 0.765 0.653 0.726 0.653 0.756 0.397 0.397 0.397 0.397 0.397 0.949 0.957 0.523 347.0 0.363 0.399 0.411 0.356 0.466 0.356 0.396 0.397 0.556 0.556 0.556 0.556 0.556 0.556 0.556 0.557 0.503 394.0 0.447 0.348 0.378 0.378 0.392 0.392 0.348 0.387 0.387 0.397 0	651 0.618 0.651 0.541 312.0 0.440 0.423 0.406 0.390 0.430 0.430 0.430 0.390 0.430 0.390 0.959 0.950 0.964 0.918 321.0 0.819 0.726 0.794 0.708 0.708 0.795 0.949 0.959 0.959 0.951 0.551 0.51 0.819 0.726 0.794 0.708 0.708 0.795 0.949 0.951 0.551 0.551 0.551 0.551 0.552 0.390 0.410 0.356 0.390 0.410 0.356 0.390 0.395 0.395 0.390 0.395 0.390 0.395 0.390 0.395 0.390 0.390 0.390 0.391 0.351 0.551 0.552 0.520 0.370 0.402 0.389 0.392 0.390 0.414 0.389 0.395 0.3	651 0.618 0.651 0.541 312.0 0.440 0.423 0.406 0.390 0.430 0.450 0.450 0.450 0.450 0.450 0.450 0.450 0.450 0.450 0.450 0.450 0.959 0.950 0.954 0.918 321.0 0.819 0.726 0.794 0.794 0.708 0.795 0.940 0.	. 63	.582 0.	31 0.52	05.	380 0.400 0.333 0.379 0	383	
.999       0.950       0.964       0.918       321.0       0.819       0.726       0.794       0.798       0.798       0.797         .949       0.957       0.551       330.0       0.782       0.758       0.760       0.653       0.75       0.756       0.756       0.756       0.756       0.756       0.756       0.756       0.756       0.395       0.766       0.395       0.395       0.395       0.395       0.396       0.389       0.392       0.390       0.414       0.389       0.392       0.390       0.414       0.389       0.392       0.392       0.392       0.389       0.389       0.392       0.392       0.389       0.389       0.389       0.389       0.389       0.389       0.389       0.389       0.389       0.389       0.389       0.389       0.389       0.389       0.389       0.389       0.39	321.0 0.819 0.726 0.794 0.708 0.708 0.795 0.795 0.949 0.794 0.708 0.708 0.797 0.798 0.799 0.949 0.957 0.551 330.0 0.782 0.758 0.756 0.653 0.726 0.653 0.75 0.75 0.594 0.594 0.628 0.523 347.0 0.363 0.399 0.411 0.356 0.466 0.356 0.395 0.395 0.395 0.395 0.395 0.395 0.596 0.556 0.556 0.556 0.520 371.0 0.402 0.389 0.392 0.390 0.414 0.389 0.395 0.395 0.395 0.395 0.395 0.395 0.395 0.395 0.556 0.556 0.556 0.556 0.557 0.503 331.0 0.447 0.348 0.378 0.382 0.392 0.348 0.338 0.398 0.388 0.398 0.388 0.398 0.388 0.398 0.	999 0.950 0.964 0.918 321.0 0.819 0.726 0.794 0.708 0.708 0.795 0.959 0.950 0.9551 330.0 0.782 0.758 0.760 0.653 0.726 0.653 0.755 0.759 0.975 0.551 330.0 0.782 0.758 0.760 0.653 0.726 0.653 0.755 0.759 0.518 0.528 0.529 0.520 369 0.411 0.356 0.466 0.356 0.556 0.550 0.550 0.511 383.0 0.402 0.363 0.400 0.496 0.368 0.363 0.400 0.496 0.368 0.353 0.400 0.402 0.358 0.391 0.378 0.358 0.392 0.398 0.398 0.398 0.398 0.358 0.356 0.556 0.556 0.572 0.503 394.0 0.447 0.348 0.378 0.382 0.392 0.394 0.388 0.3	999 0.950 0.964 0.918 321.0 0.819 0.726 0.794 0.708 0.708 0.799 0.999 0.995 0.995 0.995 0.995 0.997 0.551 330.0 0.782 0.750 0.653 0.726 0.759 0.997 0.995 0.	. 65	.618 0.	51 0.54	12.	.440 0.423 0.406 0.390 0	430 0.3	0 0.42
.949     0.957     0.551     330.0     0.782     0.758     0.760     0.653     0.75       .594     0.524     0.628     0.523     347.0     0.363     0.399     0.411     0.356     0.466     0.356     0.390       .596     0.551     0.574     0.520     371.0     0.402     0.363     0.400     0.496     0.368     0.363     0.40       .566     0.566     0.520     371.0     0.402     0.363     0.400     0.496     0.368     0.363     0.40       .556     0.556     0.511     383.0     0.358     0.391     0.378     0.392     0.392     0.348     0.338       .556     0.572     0.503     394.0     0.447     0.348     0.378     0.392     0.348     0.388	1594 0.949 0.957 0.551 330.0 0.782 0.758 0.760 0.653 0.726 0.653 0.755 0.755 0.594 0.628 0.523 347.0 0.363 0.399 0.411 0.356 0.466 0.356 0.395 0	949 0.949 0.957 0.551 330.0 0.782 0.758 0.760 0.653 0.726 0.653 0.75 594 0.594 0.628 0.523 347.0 0.363 0.399 0.411 0.356 0.466 0.356 556 0.551 0.574 0.520 359.0 0.402 0.389 0.411 0.356 0.466 0.389 556 0.546 0.556 0.511 383.0 0.363 0.400 0.496 0.363 0.40 556 0.556 0.513 383.0 0.358 0.391 0.378 0.447 0.395 0.395 556 0.556 0.572 0.503 394.0 0.447 0.348 0.378 0.382 0.392 0.398  ERIAL WAS REMAINING AT THAT LOCATION.  E CALCULATED USING THE PREFIRE THICKNESSES  RIAL WAS REMAINING	949 0.949 0.957 0.551 330.0 0.782 0.758 0.760 0.653 0.726 0.653 0.75 594 0.594 0.628 0.523 347.0 0.363 0.399 0.411 0.356 0.466 0.356 596 0.594 0.520 347.0 0.402 0.399 0.411 0.356 0.466 0.356 566 0.546 0.566 0.520 371.0 0.402 0.389 0.392 0.390 0.414 0.389 556 0.545 0.556 0.511 383.0 0.402 0.389 0.391 0.378 0.447 0.395 0.363 0.363 556 0.556 0.572 0.503 394.0 0.447 0.378 0.382 0.392 0.398 581AL WAS REMAINING AT THAT LOCATION.  RIAL WAS REMAINING THE PREFIRE THICKNESSES	.99	.950 0.	54 0.91	21.	.819 0.726 0.794 0.794 0	7.0 807	8 0.79
.594 0.594 0.628 0.523 347.0 0.363 0.399 0.411 0.356 0.466 0.356 0.39 .596 0.551 0.574 0.520 359.0 0.402 0.389 0.392 0.390 0.414 0.389 0.39 .566 0.546 0.566 0.520 371.0 0.402 0.363 0.400 0.496 0.368 0.363 0.40 .556 0.545 0.556 0.511 383.0 0.358 0.391 0.378 0.447 0.395 0.358 0.39 .556 0.556 0.572 0.503 394.0 0.447 0.348 0.378 0.392 0.348 0.38	.594 0.594 0.628 0.523 347.0 0.363 0.399 0.411 0.356 0.466 0.356 0.39 .596 0.551 0.574 0.520 359.0 0.402 0.389 0.392 0.390 0.414 0.389 0.39 .566 0.546 0.566 0.520 371.0 0.402 0.363 0.400 0.496 0.368 0.363 0.40 .556 0.545 0.556 0.511 383.0 0.358 0.391 0.378 0.395 0.358 0.39 .556 0.556 0.5572 0.503 394.0 0.447 0.348 0.378 0.382 0.392 0.348 0.38	594 0.594 0.628 0.523 347.0 0.363 0.399 0.411 0.356 0.466 0.356 0.359	594 0.594 0.628 0.523 347.0 0.363 0.399 0.411 0.356 0.466 0.356 0.359 0.594 0.574 0.550 359 0.574 0.551 0.574 0.552 359.0 0.402 0.389 0.392 0.392 0.414 0.389 0.395 0.546 0.556 0.510 371.0 0.402 0.358 0.395 0.396 0.368 0.368 0.363 0.400 0.496 0.556 0.511 383.0 0.358 0.391 0.378 0.378 0.378 0.395 0.395 0.395 0.395 0.395 0.395 0.395 0.395 0.395 0.395 0.395 0.395 0.388 0.39	9.	.949 0.	57 0.55	30.	.782 0.758 0.760 0.653 0	726 0.6	3 0.75
.596 0.551 0.574 0.520 359.0 0.402 0.389 0.392 0.390 0.414 0.389 0.39 .566 0.546 0.566 0.520 371.0 0.402 0.363 0.400 0.496 0.368 0.363 0.40 .556 0.545 0.556 0.511 383.0 0.358 0.391 0.378 0.447 0.395 0.358 0.39 .556 0.556 0.572 0.503 394.0 0.447 0.348 0.378 0.382 0.392 0.348 0.38	.596 0.551 0.574 0.520 359.0 0.402 0.389 0.392 0.390 0.414 0.389 0.39 .566 0.546 0.566 0.520 371.0 0.402 0.363 0.400 0.496 0.368 0.363 0.40 .556 0.545 0.556 0.511 383.0 0.358 0.391 0.378 0.447 0.395 0.358 0.39 .556 0.556 0.572 0.503 394.0 0.447 0.348 0.378 0.382 0.392 0.348 0.338	596 0.551 0.574 0.520 359.0 0.402 0.389 0.392 0.390 0.414 0.389 0.395 0.556 0.566 0.520 371.0 0.402 0.363 0.400 0.496 0.368 0.363 0.40 556 0.545 0.556 0.511 383.0 0.358 0.391 0.378 0.447 0.395 0.358 0.395 0.395 0.395 0.395 0.395 0.395 0.395 0.395 0.395 0.381 0.378 0.348 0.392 0.392 0.348 0.381 0.378 0.392 0.392 0.398 0.398 0.381 0.382 0.392 0.398	596 0.551 0.574 0.520 359.0 0.402 0.389 0.392 0.390 0.414 0.389 0.395 566 0.566 0.520 371.0 0.402 0.363 0.400 0.496 0.368 0.363 0.40 556 0.545 0.556 0.511 383.0 0.358 0.391 0.378 0.447 0.395 0.358 0.395 56 0.556 0.572 0.503 394.0 0.447 0.348 0.378 0.487 0.392 0.348 0.338  ERIAL WAS REMAINING AT THAT LOCATION.  E CALCULATED USING THE PREFIRE THICKNESSES  RIAL WAS REMAINING	. 59	.594 0.	28 0.52	47.	.363 0.399 0.411 0.356 0	466 0.3	6 0 39
.566 0.546 0.566 0.520 371.0 0.402 0.363 0.400 0.496 0.368 0.363 0.40 .556 0.545 0.556 0.511 383.0 0.358 0.391 0.378 0.447 0.395 0.358 0.39 .556 0.556 0.572 0.503 394.0 0.447 0.348 0.378 0.382 0.392 0.348 0.38	.566 0.546 0.566 0.520 371.0 0.402 0.363 0.400 0.496 0.368 0.363 0.40 .556 0.545 0.556 0.511 383.0 0.358 0.391 0.378 0.447 0.395 0.358 0.39 .556 0.556 0.572 0.503 394.0 0.447 0.348 0.378 0.382 0.392 0.348 0.38	566 0.546 0.569 0.353 0.400 0.405 0.363 0.406 0.368 0.363 0.400 0.545 0.556 0.511 383.0 0.358 0.391 0.378 0.447 0.395 0.358 0.395 0.	566 0.546 0.566 0.363 0.363 0.40 556 0.545 0.556 0.511 383.0 0.358 0.391 0.378 0.447 0.395 0.358 0.395 556 0.556 0.557 0.503 394.0 0.447 0.348 0.378 0.392 0.392 0.398 551 0.556 0.556 0.503 394.0 0.447 0.348 0.378 0.382 0.392 0.348 0.382  ERIAL WAS REMAINING AT THAT LOCATION.  E CALCULATED USING THE PREFIRE THICKNESSES  RIAL WAS REMAINING	9	.551 0.	74 0.52	59.	.402 0.389 0.392 0.390 0	414 0.3	9 0.39
.556 0.545 0.556 0.511 383.0 0.358 0.391 0.378 0.447 0.395 0.358 0.39 .556 0.556 0.572 0.503 394.0 0.447 0.348 0.378 0.382 0.392 0.348 0.38	.556 0.545 0.556 0.511 383.0 0.358 0.391 0.378 0.447 0.395 0.358 0.39 .556 0.556 0.572 0.503 394.0 0.447 0.348 0.378 0.382 0.392 0.348 0.38 TERTAL WAS BEMAINING AT THAT TOCAMION	DSG 0.545 0.556 0.511 383.0 0.358 0.391 0.378 0.447 0.395 0.358 0.395 0.358 0.395 0.356 0.556 0.556 0.572 0.503 394.0 0.447 0.348 0.378 0.382 0.392 0.348 0.388 0.	556 0.545 0.556 0.313 383.0 0.358 0.391 0.378 0.447 0.395 0.358 0.39 556 0.556 0.572 0.503 394.0 0.447 0.348 0.378 0.382 0.392 0.348 0.38  ERIAL WAS REMAINING AT THAT LOCATION.  E CALCULATED USING THE PREFIRE THICKNESSES  RIAL WAS REMAINING	95	.546 0.	56 0.52	71.	.402 0.363 0.400 0.496 0	368 0.3	3 0.40
.556 0.556 0.572 0.503 394.0 0.447 0.348 0.378 0.382 0.392 0.348 0.38	.556 0.556 0.572 0.503 394.0 0.447 0.348 0.378 0.392 0.348 0.38 TERIAL WAS REMAINING AT THAT TOCAMION	ERIAL WAS REMAINING AT THAT LOCATION.  E CALCULATED USING THE PREFIRE THICKNESSES  RIAL WAS REMAINING	ERIAL WAS REMAINING AT THAT LOCATION.  E CALCULATED USING THE PREFIRE THICKNESSES  RIAL WAS REMAINING	٠ د د	.545 0.	56 0.51	83.	.358 0.391 0.378 0.447 0	395 0.3	8 0.39
	THEORY PERSONAL PROPERTY.	ERIAL WAS REMAINING AT THAT LOCATION. E CALCULATED USING THE PREFIRE THICKNESSE. RIAL WAS REMAINING	ERIAL WAS REMAINING AT THAT LOCATION. E CALCULATED USING THE PREFIRE THICKNESSE. RIAL WAS REMAINING	5	. 556 0.	72 0.50	94.	.447 0.348 0.378 0.382 0	392 0.3	8 0:38
CALCULATED HAINS THE DREETOR THINKERS				RIAL	WAS REMAINI	41	accaustur.			
E CALCULATED USING THE PREFIRE THICKNESSE. RIAL WAS REMAINING	RIAL WAS REMAINING									
E CALCULATED USING THE PREFIRE THICKNESSER	RIAL WAS REMAINING									
E CALCULATED USING THE PREFIRE THICKNESSE.	RIAL WAS REMAINING									
E CALCULATED USING THE PREFIRE THICKNESSER	RIAL WAS REMAINING						·			
E CALCULATED USING THE PREFIRE THICKNESSE. RIAL WAS REMAINING	RIAL WAS REMAINING									
E CALCULATED USING THE PREFIRE THICKNESSE. RIAL WAS REMAINING	RIAL WAS REMAINING									
E CALCULATED USING THE PREFIRE THICKNESSERIAL WAS REMAINING	RIAL WAS REMAINING									
E CALCULATED USING THE PREFIRE THICKNESSERIAL WAS REMAINING	RIAL WAS REMAINING									
E CALCULATED USING THE PREFIRE THICKNESSERIAL WAS REMAINING	RIAL WAS REMAINING									

TABLE 16 RSRM-7A FORWARD SEGMENT NON-STAR TIP INSULATION PERFORMANCE

	CO	COMPLIANCE	S SAFETY		FACTOR (CSF	î				<	ACTUAL	SAFETY	FACTOR	(ASF)		
STATION (IN)	N 74.0	DEGREE 140.0 20	9	LOCATIONS	336.0	MIN.	PLANE	REQUIRED S.F.	STATIO (IN)	74.0	DEGRI	EE LOCA 206.0 2	ATIONS 270.03	136.0	MIM.	PLANE
	4.0	6.0	.72	. 28	6.4	9.72	. 90	2.0	٠	'n	77	60	22.59 2		12.09	9
13.0	11.61	12.50	9.42	7.74	30.95	7.74	270.0	1.5	13.0	S.	96.9	1.54	00.0	7.0	0.0	7
7.	+	+	+	+	+	+	4	•	27.0	+	+	+	+	+	+	4
	+	+	+	+	+	+	4	1.5	•	+	+	+	+	+	+	4
	+	+	+	+	+	+	4	٠	+	+	+	+	+	+	+	+
7.	+	+	+	+	+	+	4	٠	7.	+	+	+	+	+	+	+
-	+	+	+	+	+	+	•	•		+	+	+	+	+	+	74.0
	+	+	+	+	+	+	+	1.5	•	+	+	+	+	+	+	÷
4	+	+	+	+	+	+	÷	٠	94.7	+	+	+	+	+	+	÷
142.0	+	+	+	+	+	+	÷	•		+	+	+	+	+	+	74.0
•	+	+	+	+	+	+	-	•		+	+	+	+	+	+	÷
148.5	+	+	+	+	+	+	4	•	148.5	+	+	+	+	+	+	÷
2.	+	11.74	39.63	+	+	۲.	40.		5	+	٦.	۳.	+	+		40.
62.		0.	5	∞.	+	3	06.	•	62.	•	۲.	'n	7.86	+	'n	9
75.		۳.	. 2	α;	4.47	~	9	1.5	75.		. 2	7	4.56	5.35		. 90
87.		٦.		σ.	4.85	7	7		87.	4	σ.	9.	0	•	4.43	4
99.	.5	. 7	۲.	٣.			0	•	99.	٦.	σ.	°.	₩,	4.	ς.	
15.	٥.	9.		'n	5.	٥.	74.0	•	15.	7.	9.	m	۲.	O		4
224.0	5.56		4.20	5.56	5.03	3.69	40	1.5	224.0		3.98		6.26	•	3.98	40
30.	۲.	4	3	4	٠.	4	0	•	30.	₹.	۳.	4	٣.	S	'n	40.
36.	٦.		5.03	٦.	9.	'n	40	٠	36.	°.	∞.	7.	₹.	9	∞,	
40.	'n		٦.	٦.	8	8	36	•	40.	σ.	₩,	ō.	'n	-	٦.	36.
51.	6.	4.18	∞.	۳.	°.	σ.	4	•	51.	٦.	٦.	σ.	9.	4	٦.	4
63.	4.	7	~	m.	۲.	7.	4	•	63.	ŝ	m		5.56	6.	m	
80.	٠.	۲.	₹.	۰.	6.	4.	90	•	80.	4.	9.	σ.	ŗ.	9	٠.	90
93.	∞.	σ	€.	۰.	4.01	σ.	140.0	•	93.	6.	₹.	σ.	۲.	~	4	40.
05.	٦.		٥.	۰,	5.36	٥.	0	٠	05.	4.	۲.	9.	~	-	9.	206.0
12.		9.	۲.	∞.	∞.	9.	40.	٠	12.	. 2	٦.	۲.	۳.	7.		40.
21.	∹	۲.	۳.	+	٦.	٦.	40.	•	21.	6.	7		+	∞.	. 2	40.
30.	٥.		89.	٦.	٦.	°.	74.0	•	30.	4.	3	٥.	٥.	5.51	₹.	74.0
47.	6.	'n	9.	٥.	٥.	٦.	40.	•	47.	۳.	6.	6.	٦.	₹.	6.	40.
59.	3.94	6,	3.85	3.01	۲.	٠.	336.0	٠	59.	۳.	7.	۳.	3.46	7.		9
71.	∞.	Τ.	.5	'n.	4.13	٠.	206.0	1.5	371.0	°.	4.	₩.	٥.	4.76	∞.	90
83.	9.	9.	٥.	'n	7	٥.	90	٠	83.	6.	σ.	4		0	4.	90
94.	4.	8	₩,	7.	7	7.	m		٠	۲.	Τ.	۳.	ŝ	S	.5	36.
SEGMEN	NUMINIM IN	11	2.05 AT	THE	305.0 INCH	CH STATION	NO.		SEGMENT	NUKINIK EX	MUM #	2.45 A	AT THE	383.0 I	INCH STATION	NOI
+		EGL	GIBLE	100	000 s	Δ										

TABLE 16 RSRM-7A FORWARD SEGMENT NON-STAR TIP INSULATION PERFORMANCE

DECOMPOSITION RATE (MDR)	DEGREE LOCATIONS 0.0 206.0 270.0 336.0 AVE. TIME	6 6.3 3.4 3.7 4.3 34.5	3.6 4.3 1.1 2.9 19.	0 0 0 0	8.7 0 0 0 0	0 0 0 0 4.2	0 3.	. E 0	. E 0 0 0	0 0 .	0 0	0 0 0 2.	0 0 0 10.	0.4 0 0 0.3 2	2.2 2.1 0 1.6 44.	2.7 2.3 2.0 2.2 68.	.8 1.9 2.0 1.8 66.	2.0 1.0 1.8 1.9 66.	1.0 1.1 1.0 1.2 66.	2.3 1.7 1.9 2.0 66.	2.1 1.8 2.0 2.0 66.	1.7 2.1 1.9 2.0 66.	2.1 2.1 2.2 2.0 66.	1.8 1.6 1.7 1.9 66.	1.6 1.8 1.7 66.	3.4 3.2 1.7 2.5 6	1.4 1.8 2.0 1.9 66.	4 3.8 2.9 1.5 2.4 66.	2 1.7 1.2 1.2 1.5 66.	.9 0 1.6 1.2 71.	.1 1.3 2.5 2.0 7	1.9 2.3 2.4 2.3, 74.	1.7 2.2 2.3 1.9 80.	2.5 2.4 1.5 2.2 82.	.7 2.2 1.2 2.1 8	9 1.9 2.4 2.4 2.1 94.4
MATERIAL	DEG1	.6 5.	7	0	0	0	0.	_		0	0	0	_	1.	1.5 2.			<del>-</del> :		1.7 2.	.7 2	. 8	σ.	7.		.5	.7 2	.3	m.	. 8	7	•	•	٠	2.2 2.	•
2	STATION (IN) 74	ν.	•	7.0	30.7	4.2	۲.	41.2	4.0	94.7	۰.	145.7 (	8.5	•	2.0	.5	7.0	0.66	15.0	24.0	٥.	36.0	0.0	51.0	63.0	0.08	93.0	0.5.0	12.0	21.0	30.0	47.0	59.0	71.0	3.0	394.0
	DESIGN M+3S	0.103	0.101	0.044	0.033	. 03		.02	. 01		.01	. 08	. 13	٠		.32	.39	. 42	•	•	0.375	•	4	.3	. 33	. 35	m	30	m.	. 43	33	۳.	0.279	30	~	0.287
	MAX.		0.084	0	•	0	0	0	0	0	0	0	0	.02	.09	٦.	. 15	. 17	. 10	.17		. 16	. 15	. 14	. 13	. 22	~	?	. 14	. 13	.17	. 20	. 18			
(MDD)	MEDIAN	. 12	0.056	•	0	0	•	0	0	0	0	0	0	0	.09	. 14	.12	. 13	.07	. 12	0.136	. 12	. 13	. 11	. 10	. 17	. 11	. 16	.08	. 11	. 17	.17	. 13	. 18	. 19	. 20
MATERIAL DECOMPOSITION DEPTH INCHES	CON DEGREE LOCATIONS ) 74.0 140.0 206.0 270.0 336.0	.088 0.194<0.218<0.116<0.12	0.056 0.052 0.069 0.084 0	0 0 0 0	0 0 0 0	0 0 0	•	0 0 0 0	0 0 0	0 0 0	0 0 0 0	0 0 0	0 0 0	0 0.027 0.008 0	0.066 0.091 0.098 0.093 0.00	0.143 0.139 0.184 0.158 0.13	0.152 0.083 0.118 0.129 0.13	0.141 0.170 0.136 0.069 0.12	0.105 0.084 0.070 0.075 0.06	0.115 0.173 0.152 0.115 0.12	112 0.145 0.142 0.117 0.	0.123 0.163 0.115 0.139 0.12	0.126 0.122 0.137 0.138 0.15	0.145 0.136 0.118 0 107 0.11	0.105 0.134 0.109 0.106 0.11	0.099 0.179 0.228 0.211 0.11	0.112 0.186 0.094 0.118 0.13	0.085 0.160 0.256 0.195 0.09	0.087 0.149 0.114 0.079 0.07	0.128 0.136 0.064 0 0.11	0.179 0.171 0.081 0.089 0.17	0.177 0.208 0.145 0.170 0.17	0.132 0.133 0.135 0.173 0.18	0.184 0.168 0.207 0.201 0.12	0.196 0.194 0.244 0.201 0.10	0.205 0.176 0.175 0.224 0.22
	STATION (IN)		<u>ب</u>	7	•	4		_;	4.	94.		45.	89	52.	62.	75.	87.	99.	15.	24.	30.	36.	40.	51.	63.		93.	05.	12.	21.	30.	47.	59.	71.	83.	94.

" INDICATES THE PRECEDING MDD HAS EXCEEDED THE M + 3 SIGMA DESIGN CRITERIA

MOTOR ACTION TIME = 123.4 SECONDS

	I PERFORMANCE
	T NON-STAR TIP INSULATION
	TIP
	NON-STAR
LABLE 16	SEGMENT
1	RSRM-7A FORWARD SEGMENT
	RSRM-7A

		KSKM-/A F	* *	PUR HORI	SIAK IIF INS	BO1: V108 K1	4		1	;	
	PREFIRE MEASUREMENTS INCHES	PART NO SERIAL	. 14766 10. 000	66-01 0003			POSTFIRE INC	e measurembat NCHES		PART NO. SERIAL N	1076650-03 o. 00000003
STATION (IN) 74.0	DEGREE LOCATIONS 140.0 206.0 270.0 336.0	MIN.	MEDIAN	HDT	STATION (IN)	74.0	DEGREE 140.0 206	LOCATIO 6.0 270.	ONS .0 336.0	MIN.	MEDIAN
5 2.67	2.672 2.635 2.620 2.70	. 62	. 67	12		.582	78 2.	417 2.50	4 2.		. 50
3.0 0.87	0.830 0.796 0.840 0.77	.77	. 83	65	۳.	20	.778 0.	27 0.7	.09	. 72	2
0.00	0.601 0.605 0.613 0.57	.57	.60	45		.1		ı. L	.i	'n	9
0.7 0.41	0.411 0.405 0.424 0.41	.40	. 41	40		ı			יי	႕	41
1.2 0.44	0.431 0.438 0.444 0.43	. 43	. 43	0.380		.1	_	ı L	ם	ឯ	43
7.7 0.34	0.336 0.337 0.348 0.34	. 33	. 34	33	7.	1			יו	ŋ	. 34
1.2 0.28	0.284 0.282 0.294 0.28	. 28	. 28	. 28	ä	u			13	u	. 28
4.0 0.28	0.291 0.285 0.293 0.29	. 28	. 29	. 25	•	u			.1	J	. 29
4.7 0.10	0.109 0.106 0.109 0.11	.10	.10	.09	÷	LI.			.1	ı	10
42.0 0.16	0.167 0.168 0.170 0.17	.16	.16	0.113	ς.	J			u	בן	. 16
45.7 0.25	0.259 0.264 0.259 0.27	. 25	. 25	. 23	δ.	H			7		. 25
48.5 0.28	0.287 0.287 0.280 0.28	. 28	. 28	. 27		1	.317	-1		.31	. 28
52.0 0.34	0.356 0.339 0.345 0.36	. 33	. 34	m.		.36	.329 0.	31 0.3	9 0.44	0.32	.36
62.0 0.71	0.706 0.744 0.731 0.73	. 70	. 73	5	ς.	9.	.615 0.	46	8 0.73	0.61	. 64
75.5 0.72	0.724 0.776 0.720 0.72	.72	.72	9.	75.	s.	.585 0.	92 0.5	2 0.58	0.56	. 58
87.0 0.67	0.660 0.668 0.653 0.66	. 65	99.	.64	87.	. 52	.577 0.	50 0.5	4 0.52	0.52	. 52
79.0 0.69	0.678 0.690 0.676 0.66	99.	.67	. 64	99.	. 53	. 508 0.	54 0.6	7 0.54	0.50	. 54
15.0 0.65	0.645 0.654 0.658 0.66	. 64	. 65	. 63	15.		.561 0.	4	3 0.59	0.55	. 58
24.0 0.69	0.689 0.703 0.720 0.69	. 68	. 69	. 63	24.	. 57	.516 0.	51 0.6	5 0 .56	0.51	. 56
30.0 0.61	0.623 0.628 0.630 0.61	. 61	. 62	. 63	30.	. 50	.478 0.	86 0.5	3 0.48	0.47	. 4.8
36.0 0.61	0.633 0.604 0.620 0.61	9.	. 61	. 57	36.	. 49	.470 0.	489 0.4	0 . 48	0.47	. 48
40.0 0.62	0.597 0.624 0.623 0.62	. 59	. 62	. 57	40.	. 50	.475 0.	487 0.4	5 0.47	0.47	. 48
251.0 0.748	0.705 0.703 0.716 0	0.703	0.716	0.568	251.0	0.603	69 0.	585 0.6	9.0 6		0.603
63.0 0.58	0.581 0.602 0.589 0.58	. 58	. 58	. 56	63.	. 47	.447 0.	493 0.4	3 0 46	0 4 4	. 4.
80.0 0.08	0.655 0.675 0.709 0.64	. 63	. 65	. 56	80	. 53	.476 0.	447 0.4	8 0.53	0.44	9.
93.0 0.55	0.632 0.560 0.560 0.58	. 55	. 26	. 54	93.	44	.446 0.	466 0.4	9.4	44.0	4
05.0 0.54	0.605 0.684 0.625 0.60	. 54	9.	. 52	05.	. 46	.445 0.	428 0.4	0 0 50	0.42	4.
12.0 0.62	0.616 0.652 0.660 0.65	. 61	. 65	. 54	12.	. 54	.467 0.	538 0.5	1 0.57	0.46	.54
21.0 1.01	0.992 0.974 v 982 0.99	. 97	66.	. 91	21.	88	.856 0.	10 1.p	5 0 .88	0.85	∞ ∞ :
30.0 0.97	0.948 0.964 0.971 0.95	.94	96.	. 55	30.	. 79	.0 777.	830.8	2 0.78	0.77	67.
47.0 0.59	0.607 0.573 0.610 0.63	. 57	9.	. 52	47.	. 41	.399 0.	28 0.4	0 0.45	0.39	. 42
59.0 0.57	0.560 0.583 0.599 0.59	. 56	. 58	'n	9	4	.427 0.	48 0.4	6 0.41	0.41	4.2
71.0 0.55	0.571 0.593 0.588 0.60	. 55	. 58	. 52	71.	. 37	.403 0.	0	.47	0.37	m .
83.0 0.58	0.572 0.597 0.560 0.54	.54	. 57	. 51	m.	3		53 0.3	9 0.43	0.35	. 3
94.0 0.56	0.561 0.580 0.580 0.57	. 56	. 57	. 50	S)	. 35	85 0.	5 0.3	6 0.34	0.34	م

AN " L " INDICATES THAT LINER MATERIAL WAS REMAINING AT THAT LOCATION. THE MEDIAN AND MINIMUM VALUES WERE CALCULATED USING THE PREFIRE THICKNESSES AT THE LOCATIONS WHERE LINER MATERIAL WAS REMAINING

# RSRM-7B NOZZLE TO CASE JOINT PERFORMANCE

DEGREE LOCATION	PREFIRE (INCHES)	POSTFIRE (INCHES)	MDD	CSF	ASF
0.0 21.6 46.8 68.4 90.0 111.6 136.8 158.4 180.0 201.6 226.8 248.4 270.0 291.6 316.8 338.4	5.559 5.506 5.532 5.507 5.514 5.533 5.435 5.532 5.471 5.489 5.202 5.536 5.541 5.507 5.510	4.325 4.792 4.715 4.532 4.747 4.685 4.736 4.798 4.415 4.842 4.456 4.843 4.724 4.940 4.836 4.644	1.234 0.714 0.817 0.975 0.767 0.806 0.797 0.637 1.117 0.629 1.033 0.359 0.812 0.601 0.671 0.866	4.0 6.9 6.0 5.0 6.4 6.1 7.7 4.4 7.8 4.7 13.6 6.0 8.2 7.3	4.5 7.7 6.8 5.6 7.2 6.8 6.9 8.5 5.0 8.7 5.3 14.5 6.8 9.2 8.2 6.4
	MEDIAN 5.509	MEDIAN 4.730	MEDIAN 0.802	MINIMUM 4.0	MINIMUM 4.5

# RSRM-7B AFT FIELD JOINT PERFORMANCE

DEGREE LOCATION	PREFIRE (INCHES)	POSTFIRE (INCHES)	MDD	CSF	ASF
2.0 16.0 30.0 46.0 60.0 76.0 90.0 106.0 120.0 136.0 150.0 166.0 180.0 196.0 210.0 226.0 242.0 256.0 270.0 286.0 300.0 316.0 330.0	2.737 2.764 2.762 2.763 2.758 2.774 2.779 2.779 2.779 2.779 2.779 2.779 2.749 2.749 2.749 2.749 2.736 2.736 2.734 2.734 2.753 2.753	2.272 2.271 2.310 2.309 2.309 2.273 2.325 2.285 2.261 2.298 2.317 2.345 2.344 2.342 2.312 2.355 2.296 2.324 2.326 2.326 2.326 2.326 2.326 2.326 2.326 2.326	0.465 0.493 0.452 0.454 0.454 0.459 0.501 0.439 0.481 0.457 0.434 0.405 0.427 0.436 0.394 0.436 0.434 0.434 0.434 0.434	5.778293147041069300548 5.555555566665666555	5.6 6.1 6.1 6.1 6.1 6.1 6.1 6.1 6.1 6.1 6
340.0	2.760 MEDIAN	2.319 MEDIAN	0.441 MEDIAN	5.9 MINIMUM	6.3 minimum
	2.760	2.309	0.444	5.1	5.4

## RSRM-7B CENTER FIELD JOINT PERFORMANCE

DEGREE LOCATION	PREFIRE (INCHES)	POSTFIRE (INCHES)	MDD	CSF	ASF .
2.0 16.0 30.0 46.0 60.0 76.0 90.0 106.0 120.0 136.0 150.0 166.0 196.0 210.0 226.0 242.0	2.747 2.720 2.734	2.540 2.531 2.512 2.540 2.535 2.553 2.563 2.563 2.563 2.574 2.529 2.523 2.529 2.523 2.5557 2.5557 2.5557 2.5557 2.5543 2.508	0.207 0.189 0.222 0.195 0.215 0.189 0.157 0.163 0.207 0.1227 0.136 0.193 0.199 0.182 0.189 0.157 0.143 0.150 0.198 0.176 0.211	12.5 13.7 11.7 13.3 12.1 13.7 16.5 15.9 12.5 11.4 19.1 13.4 13.0 14.3 13.7 16.5 18.1 17.3 13.1 14.7 12.3	13.3 14.4 12.3 14.0 12.8 14.5 17.1 16.7 13.0 12.1 19.9 14.2 13.7 14.9 14.4 17.3 18.9 18.1 13.7
316.0	2.725	2.522	0.203	12.8	13.4
330.0	2.699	2.547	0.152	17.1	17.8
346.0	2.731	2.523	0.208	12.5	13.1
	MEDIAN	MEDIAN	MEDIAN	MINIMUM	MINIMUM
	2.720	2.535	0.191	11.4	12.1

# RSRM-7B FORWARD FIELD JOINT PERFORMANCE

DEGREE LOCATION	PREFIRE (INCHES)	POSTFIRE (INCHES)	MDD	CSF	ASF
2.0 16.0 30.0 46.0 60.0 76.0 90.0 120.0 136.0 150.0 166.0	2.746 2.756 2.785 2.775 2.771 2.744 2.723 2.741 2.731 2.769 2.765 2.764 2.743	2.561 2.580 2.593 2.611 2.610 2.615 2.603 2.597 2.562 2.546 2.600 2.630 2.611	0.185 0.176 0.192 0.164 0.161 0.129 0.120 0.144 0.169 0.223 0.165 0.134	14.0 14.7 13.5 15.8 16.1 20.1 21.6 18.0 15.4 11.6 15.7 19.4	14.8 15.7 14.5 16.9 17.2 21.3 22.7 19.0 16.2 12.4 16.8 20.6 20.8
196.0	2.745	2.634	0.111	23.4	24.7
210.0	2.720	2.597	0.123		22.1
226.0	2.724	2.590	0.134	19.4	20.3
242.0	2.747	2.636	0.111	23.4	24.7
256.0	2.745	2.600	0.145	17.9	18.9
270.0	2.730	2.574	0.156	16.6	17.5
286.0	2.724	2.600	0.124	20.9	22.0
300.0	2.725	2.594	0.131	19.8	20.8
316.0	2.743	2.610	0.133	19.5	20.6
330.0	2.727	2.614	0.113	23.0	24.1
346.0	2.731	2.591	0.140	18.5	19.5
	MEDIAN	MEDIAN	MEDIAN	MINIMUM	MINIMUM
	2.743	2.600	0.137	11.6	12.4

10. 3.79 3.57 3.30 3.01 3.40 4.02 3.32 2.91 2.52 111.6 11.5 3.32 3.10 2.52 2.53 2.50 2.40 2.40 2.40 2.40 2.40 2.40 2.40 2.4
19 2.85 2.83 2.23 2.51 2.68 2.68 2.46 2.99 90.0 16 2.88 2.48 2.06 2.40 2.46 2.55 2.32 2.06 2.88.4 16 2.88 2.48 2.06 2.40 2.46 2.55 2.32 2.06 2.88.4 19 3.06 2.31 1.84 2.37 2.21 2.29 2.16 1.94 90.0 10 3.06 2.31 1.84 2.37 2.21 2.29 2.16 1.94 90.0 10 3.25 2.31 2.01 2.36 2.24 2.35 2.16 1.94 90.0 10 3.21 2.63 2.01 2.36 2.62 2.50 2.58 2.32 2.34 1.99 90.0 10 3.21 2.03 2.34 2.32 2.62 2.50 2.52 2.32 2.34 1.99 90.0 10 3.21 2.91 2.32 2.62 2.52 2.62 2.50 2.53 2.23 2.48.4 1.52 2.30 2.34 2.23 2.42 2.93 2.70 2.53 2.23 2.23 2.48.4 1.52 2.30 2.34 2.23 2.42 2.92 2.70 2.75 2.91 2.91 2.91 2.91 2.91 2.91 2.91 2.91
1.6 2.88 2.48 2.06 2.40 2.48 2.55 2.32 2.00 2.48 2.68 4  1.16 2.81 2.06 2.41 1.84 2.36 2.40 2.48 2.55 2.32 1.87 248.4  1.21 3.06 2.31 1.84 2.37 2.42 2.36 2.16 1.94 90.0  1.22 3.15 2.43 2.01 2.36 2.28 2.36 2.36 2.36 1.94 90.0  1.23 3.27 3.04 2.32 2.52 2.62 2.50 2.58 2.32 248.4  1.23 2.30 2.34 2.23 2.42 2.52 2.62 2.50 2.53 2.23 2.48.4  1.25 2.30 2.34 2.23 2.42 2.93 2.36 2.39 2.44 1.99 90.0  1.25 2.30 2.30 2.34 2.23 2.42 2.93 2.36 2.50 2.53 2.23 2.48.4  1.25 2.30 2.30 2.34 2.23 2.42 2.93 2.30 2.40 1.2.75 136.8  1.25 2.30 2.30 2.30 2.30 2.40 2.40 2.40 1.11.6  1.25 2.30 2.30 2.30 2.30 2.40 2.40 2.40 1.11.6  1.31 3.29 3.68 3.89 3.75 3.44 3.22 2.70 2.49 1.11.6  1.32 3.54 4.32 4.73 4.14 4.08 4.27 3.54 3.13 180.0  1.33 3.54 4.32 5.40 2.40 2.40 2.40 3.64 3.18 2.75 1.11.6  1.34 3.35 2.39 2.39 2.40 2.40 2.40 2.40 3.64 3.18 2.75 1.11.6  1.35 3.29 2.40 2.40 2.40 2.40 2.40 3.64 3.18 2.75 1.11.6  1.30 3.20 2.40 2.40 2.40 2.40 2.40 3.64 3.18 2.75 1.11.6  1.31 3.32 2.39 2.39 2.40 2.40 2.40 2.40 3.64 3.18 2.75 1.11.6  1.34 3.35 2.30 2.40 2.40 2.40 2.40 2.40 2.40 3.64 3.18 2.75 1.11.6  1.35 3.37 3.08 2.67 2.04 2.70 2.40 2.40 2.40 2.40 2.40 2.40 2.40 2.4
91 3.06 2.31 1.84 2.37 2.21 2.29 2.16 1.84 248.4  82 3.15 2.43 2.01 2.36 2.24 2.35 2.16 1.99 90.0  83 2.21 2.63 2.14 2.39 2.15 2.39 2.24 1.99 90.0  7.9 3.27 3.04 2.32 2.52 2.62 2.50 2.58 2.22 248.4  8.5 2.30 2.34 2.23 2.42 2.93 2.30 2.51 2.52 2.24 1.99  8.6 2.30 2.34 2.23 2.42 2.93 2.90 2.53 2.10 2.52 2.23 2.48.4  8.5 2.63 2.69 3.29 2.39 2.69 2.30 2.70 2.77 2.75 136.8  8.5 2.49 2.40 2.48 2.66 2.81 2.81 2.67 2.77 2.77 2.24 136.8  8.3 2.44 2.46 2.61 2.81 2.67 2.78 2.77 2.24 136.8  8.3 2.44 2.46 2.61 2.81 2.67 2.78 2.77 2.24 136.8  9.1 3.29 3.68 3.89 3.75 3.34 3.22 3.20 2.49 111.6  9.0 2.1 3.29 3.68 3.89 3.75 3.34 3.22 3.20 2.49 111.6  9.1 3.29 3.68 3.89 3.76 4.40 4.27 3.54 3.33 180.0  8.0 2.01.6 2.26.8 248.4 2.70.0 2.91.6 316.8 338.4 MIN. PIAME  8.2 3.2 2.30 2.40 2.40 2.40 2.40 2.40 3.64 3.18 2.75 111.6  9.3 3.2 2.3 2.40 2.40 2.40 2.40 2.40 3.44 3.15 2.30 2.04 2.40 2.40 2.40 2.40 2.40 2.40 2.4
25 3.15 2.43 2.01 2.36 2.24 2.35 2.16 199 90.0  0.4 3.21 2.63 2.14 2.35 2.62 2.50 2.54 1.99 90.0  1.5 2.30 2.34 2.32 2.42 2.93 2.34 1.99 90.0  1.5 2.30 2.34 2.32 2.42 2.93 2.35 2.24 1.99 90.0  1.5 2.30 2.34 2.35 2.42 2.93 2.35 2.35 2.32 248.4  1.6 2.30 2.34 2.35 3.75 3.80 3.79 3.57 3.41 2.75 2.32 248.4  1.6 2.6 3.69 3.29 3.79 2.66 2.70 2.70 2.12 136.8  1.2 2.44 2.46 2.61 2.81 2.67 2.76 2.77 2.77 2.74 136.8  1.3 3.2 3.6 3.8 3.8 3.75 3.34 3.2 2.30 2.49 111.6  1.3 3.2 3.6 3.8 3.8 3.75 3.34 3.2 2.70 2.12 136.8  1.3 3.2 4.3 4.3 4.2 2.6 2.6 2.6 2.70 2.70 2.12 136.8  1.3 3.5 4.3 4.2 2.6 2.6 2.6 2.6 2.70 2.70 2.12 136.8  1.3 3.5 4.3 4.2 2.6 2.6 2.6 2.7 2.7 2.7 2.2 2.4 111.6  1.3 3.5 2.4 2.4 2.4 2.4 2.4 2.4 2.4 2.4 2.4 2.4
2.53 2.30 2.34 2.32 2.52 2.62 2.50 2.53 2.32 248.4 2.53 2.30 2.34 2.33 2.42 2.93 2.30 2.53 2.23 248.4 2.53 2.30 2.34 2.23 2.42 2.93 2.30 2.53 2.91 2.52 2.81.6 2.45 2.67 2.97 2.94 2.66 2.70 2.77 2.77 2.72 136.8 2.45 2.63 2.67 2.48 2.66 2.76 2.77 2.77 2.42 136.8 2.25 2.39 2.29 2.39 2.69 2.39 2.66 2.70 2.49 111.6 2.31 3.24 3.48 3.89 3.75 3.44 2.77 2.77 2.74 116.8 2.31 3.24 4.32 4.73 4.14 4.08 4.27 3.54 3.33 180.0 2.31 3.24 4.32 4.73 4.14 4.08 4.27 3.54 3.33 180.0 2.31 3.54 4.32 4.73 4.14 4.08 4.27 3.54 3.33 180.0 2.31 3.54 4.32 2.64 2.70.0 291.6 316.8 338.4 MIN. PLAME 5.71 5.40 4.83 4.22 5.64 5.32 4.62 4.51 3.49 111.6 3.53 3.54 2.55 2.65 2.65 2.67 2.67 2.47 2.20 248.4 3.50 3.13 2.80 2.67 2.81 2.81 2.95 2.67 2.36 2.02 2.48.4 3.50 3.13 2.80 2.67 2.02 2.65 2.67 2.36 2.02 2.48.4 3.50 3.13 2.80 2.67 2.02 2.65 2.67 2.36 2.03 2.00 2.00 3.35 2.44 2.03 2.67 2.36 2.03 2.00 2.00 3.35 2.00 2.00 2.00 2.00 2.00 2.00 2.00 2.0
2.53 2.30 2.34 2.23 2.42 2.93 2.30 2.53 2.23 248.4 2.62 3.69 3.29 2.97 2.97 2.97 2.91 2.75 2.16 2.45 2.63 2.67 2.48 2.66 2.76 2.77 2.77 2.42 136.8 2.32 2.44 2.6 2.89 2.89 2.69 2.39 2.66 2.70 2.12 136.8 2.32 2.44 2.46 2.89 2.69 2.39 2.66 2.77 2.77 2.77 2.42 136.8 2.33 2.44 2.46 2.89 2.69 2.39 2.66 2.77 2.77 2.77 2.42 136.8 2.33 3.54 4.32 4.73 4.14 4.08 4.27 3.54 3.33 180.0 3.33 3.54 4.32 4.73 4.14 4.08 4.27 3.54 3.33 180.0  ERACTOR (ASF)  COATIONS  60.0 201.6 226.8 248.4 270.0 291.6 316.8 338.4 MIN. PLANE 61.3 3.93 3.6 3.29 2.6 5.64 5.32 4.62 4.51 3.49 111.6 4.13 3.93 3.6 3.29 2.76 3.10 3.44 3.15 3.21 2.55 90.0 3.50 3.13 2.80 2.67 2.02 2.65 2.76 2.47 2.20 248.4 3.50 3.13 2.80 2.67 2.02 2.65 2.67 2.36 2.69 2.90 3.31 3.24 3.39 3.44 2.64 2.02 2.65 2.76 2.77 2.36 2.02 2.48.4 3.24 3.39 2.57 2.77 2.74 2.55 2.70 2.44 2.23 90.0 3.30 3.31 3.34 3.41 3.07 3.12 3.16 3.37 2.93 111.6 4.51 4.44 4.44 4.45 4.43 4.43 4.43 3.44 2.44 2.44 4.44 2.44 2
2.62 2.97 2.97 2.98 2.69 2.70 2.75 2.91 2.52 21.6 3.65 3.65 3.25 3.75 3.80 3.79 3.41 2.75 136.8 3.65 2.62 2.6 2.70 2.77 2.77 2.72 136.8 2.25 2.39 2.29 2.39 2.69 2.39 2.66 2.70 2.12 136.8 2.25 2.34 2.46 2.61 2.81 2.67 2.77 2.77 2.74 136.8 2.91 3.29 3.68 3.89 3.75 3.34 3.22 3.20 2.49 111.6 2.91 3.29 3.68 3.89 3.75 3.34 4.27 2.77 2.74 111.6 3.33 3.54 4.32 4.73 4.14 4.08 4.27 3.54 3.33 180.0  EACTION (ASF)  CCATIONS  60.0 201.6 226.8 248.4 270.0 291.6 316.8 338.4 MIN. PLAME  80.0 201.6 226.8 248.4 270.0 291.6 316.8 338.4 MIN. PLAME  80.0 201.6 226.8 248.4 270.0 291.6 316.8 338.4 MIN. PLAME  80.0 201.6 226.8 248.4 270.0 291.6 316.8 338.4 MIN. PLAME  81.3 3.93 3.66 3.29 2.76 3.10 3.44 3.15 3.21 2.55 90.0 3.50 3.13 2.80 2.45 2.81 2.93 2.96 2.69 2.69 2.00 3.50 3.13 2.80 2.45 2.81 2.93 2.96 2.69 2.00 2.48.4 3.20 3.23 2.99 2.76 2.00 2.65 2.67 2.36 2.07 2.48.4 3.20 3.23 3.29 2.57 2.04 2.70 2.45 2.57 2.36 2.04 2.48.4 3.20 3.23 3.24 3.39 2.87 2.04 2.70 2.45 2.57 2.36 2.03 2.04 2.48.4 3.20 3.55 2.75 2.77 2.74 2.55 2.70 2.44 2.73 3.01 2.71 2.48.4 4.51 4.64 4.04 3.04 2.05 3.14 2.97 3.01 2.71 2.48.4 4.51 4.64 4.04 3.04 2.05 3.14 2.97 3.01 2.71 2.48.4 4.51 4.64 4.64 4.74 4.75 4.70 4.43 4.31 3.44 136.8 3.47 3.86 2.55 2.65 3.01 2.74 2.98 3.14 3.13 3.44 3.13 3.44 3.16 3.19 3.19 2.76 136.8 3.47 3.86 2.57 2.06 2.52 2.55 3.01 2.74 3.03 3.10 2.74 3.03 3.14 3.15 3.83 3.14 3.99 4.67 5.12 4.74 4.71 4.79 3.99 3.64 180.0
3.65 3.69 3.25 3.75 3.80 3.79 3.57 3.41 2.75 136.8 2.45 2.39 2.25 2.39 2.66 2.70 2.17 2.77 2.42 136.8 2.25 2.39 2.65 2.70 2.77 2.77 2.42 136.8 2.25 2.39 2.64 2.65 2.39 2.26 2.77 2.77 2.77 2.42 136.8 2.31 3.29 3.68 3.89 3.75 3.34 3.22 3.20 2.49 111.6 3.33 3.54 4.32 4.73 4.14 4.08 4.27 3.54 3.33 180.0 0.0 CATIONS (ASF)  5.71 5.40 4.83 4.22 5.64 5.32 4.62 4.51 3.49 111.6 6.0.0 2.01.6 2.26.8 248.4 2.76 3.19 3.68 3.29 3.76 3.29 2.66 2.47 2.20 2.48.4 3.59 3.23 2.99 2.76 3.10 3.44 3.15 3.21 2.50 2.48.4 3.25 3.23 2.99 2.76 3.10 3.44 3.15 2.80 2.47 2.20 2.48.4 3.25 3.25 2.75 2.75 2.76 2.47 2.20 2.48.4 3.20 2.57 2.30 2.00 2.48.4 3.20 2.57 2.30 2.00 2.48.4 3.20 2.57 2.30 2.00 2.48.4 3.20 2.57 2.30 2.60 2.47 2.20 2.48.4 3.20 2.57 2.30 2.60 2.47 2.20 2.48.4 3.20 2.57 2.30 2.40 2.48 2.57 2.30 2.50 2.48 2.40 2.45 2.50 2.40 2.45 2.50 2.40 2.45 2.50 2.40 2.40 2.40 2.40 2.40 2.40 2.40 2.4
TACTOR (ASF)  FACTOR (ASF)  COATIONS  5.71 5.45 2.64 2.46 2.89 2.89 2.66 2.70 2.71 2.12 136.8  2.91 3.29 3.68 3.89 3.75 3.34 3.22 3.20 2.49 111.6  3.33 3.54 4.32 4.73 4.14 4.08 4.27 3.54 3.33 180.0  EACTOR (ASF)  COATIONS  60.0 201.6 226.8 248.4 270.0 291.6 316.8 338.4 MIN. PLANE  5.71 5.40 4.83 4.22 5.64 5.32 4.62 4.51 3.49 111.6  4.13 3.93 3.68 3.29 3.76 4.40 3.64 3.18 2.75 111.6  3.59 3.23 2.99 2.76 3.10 3.44 3.15 2.75 111.6  3.50 3.13 2.80 2.65 2.62 2.65 2.76 2.40 2.69 2.00  3.35 3.24 3.39 2.67 2.04 2.70 2.45 2.57 2.30 90.0  3.36 3.37 3.34 3.04 2.70 2.45 2.57 2.36 2.02 248.4  3.20 3.55 2.64 2.02 2.69 2.55 2.70 2.44 2.23 90.0  3.30 3.31 3.34 3.04 3.04 3.01 2.71 2.48.4  2.99 2.66 2.74 2.63 2.87 2.74 2.95 2.58 2.35 90.0  3.30 3.31 3.34 3.41 3.07 2.45 2.76 2.45 2.35 2.04 248.4  2.99 2.66 2.74 2.63 2.87 2.45 2.58 2.38 2.04 248.4  2.99 2.66 2.74 2.63 2.87 3.48 2.74 2.95 2.63 2.48.4  2.99 2.66 2.74 2.63 2.87 3.48 2.74 2.95 2.63 2.48.4  2.99 2.66 2.74 2.63 2.87 3.48 2.74 2.95 2.63 2.63 2.48.4  2.99 2.66 2.74 2.63 2.87 3.48 2.74 2.95 2.63 2.83 136.8  2.59 2.66 2.74 2.70 2.91 3.17 3.13 3.10 2.38 136.8  2.59 2.66 2.74 2.70 2.91 3.17 3.18 3.19 2.76 136.8  2.59 2.66 2.75 2.75 2.77 2.74 3.13 3.13 2.48 4.31 3.68 3.47 3.85 3.82 2.96 111.6
FACTOR (ASF)  FACTOR (ASF)  FACTOR (ASF)  CCATIONS  5.79 2.64 2.70 2.70 2.77 2.74 136.8 3.33 3.54 4.32 4.73 4.14 4.08 4.27 3.54 3.33 180.0 2.49 111.6 4.00 4.27 3.54 3.33 180.0 2.49 111.6 4.00 201.6 226.8 248.4 270.0 291.6 316.8 338.4 MIN. PLANE BES 0.0 201.6 226.8 248.4 270.0 291.6 316.8 338.4 MIN. PLANE BES 0.0 201.6 226.8 248.4 2.76 4.40 3.64 3.18 2.75 111.6 4.13 3.93 3.66 3.29 3.76 4.40 3.64 3.18 2.75 111.6 3.29 2.76 2.76 2.47 2.20 248.4 3.15 3.23 2.99 2.76 2.67 2.96 2.69 2.20 248.4 3.15 3.23 2.99 2.76 2.67 2.96 2.00 2.48.4 3.20 3.24 3.24 3.25 2.64 2.00 2.46.4 2.20 2.65 2.70 2.44 2.23 90.0 3.30 3.55 2.75 2.70 2.44 2.23 90.0 3.30 3.55 2.75 2.70 2.44 2.23 90.0 3.30 3.55 2.75 2.70 2.44 2.23 90.0 3.30 3.88 3.58 2.71 3.05 3.14 2.97 3.01 2.71 2.48.4 2.20 2.48.4 2.20 2.60 2.80 2.80 2.80 2.80 2.80 2.80 2.80 2.8
FACTOR (ASF)  FACTOR (ASF)  CCATIONS  5.73 3.54 4.32 4.73 4.14 4.08 4.27 3.54 3.32 180.0  FACTOR (ASF)  CCATIONS  5.71 5.40 4.83 4.22 5.64 5.32 4.62 4.51 3.49 111.6  6.71 5.40 4.83 4.22 5.64 5.32 4.62 4.51 3.49 111.6  4.13 3.93 3.66 3.29 3.76 4.40 3.64 3.18 2.75 111.6  3.59 3.53 2.99 2.76 3.10 3.44 3.15 3.21 2.55 90.0  3.37 3.08 2.67 2.02 2.65 2.76 2.47 2.20 248.4  3.26 3.25 2.64 2.02 2.65 2.76 2.47 2.20 248.4  3.26 3.25 2.64 2.02 2.65 2.76 2.47 2.20 248.4  3.26 3.25 2.64 2.02 2.65 2.76 2.47 2.23 90.0  3.37 3.08 2.67 2.04 2.70 2.45 2.57 2.38 2.04 2.48.4  3.26 3.25 2.64 2.70 2.45 2.57 2.38 2.04 2.48.4  2.99 2.66 2.74 2.63 2.86 2.80 2.82 2.58 2.35 90.0  3.30 3.88 3.58 2.71 3.05 3.14 2.95 2.63 2.48.4  2.97 3.74 3.04 2.47 2.75 4.70 4.43 4.31 3.44 136.8  2.97 3.74 3.04 2.75 4.77 4.70 4.43 4.31 3.44 136.8  2.98 2.66 2.55 2.65 3.01 2.74 3.03 3.10 2.38 136.8  2.58 2.66 2.55 2.65 3.01 2.74 3.13 2.48 136.8  2.58 2.66 2.55 2.65 3.01 2.74 4.01 3.85 3.82 2.96 111.6  3.47 3.86 4.26 4.67 4.71 4.01 3.85 3.82 2.96 111.6
FACTOR (ASF)  CCATIONS  60.0 201.6 226.8 248.4 270.0 291.6 316.8 338.4 MIN. PLAME  5.71 5.40 4.83 4.22 5.64 5.32 4.62 4.51 3.49 111.6  4.13 3.93 3.66 3.29 3.76 4.40 3.64 3.18 2.75 111.6  3.59 3.23 2.99 2.76 3.10 3.44 3.15 3.21 2.55 90.0  3.50 3.13 2.80 2.45 2.81 2.93 2.96 2.69 2.30 90.0  3.50 3.13 2.80 2.45 2.81 2.93 2.96 2.69 2.30 90.0  3.50 3.13 2.80 2.45 2.85 2.76 2.47 2.22 2.48.4  3.20 3.55 2.75 2.04 2.70 2.45 2.57 2.36 2.04 2.48.4  3.20 3.55 2.75 2.04 2.70 2.45 2.57 2.36 2.04 2.48.4  3.20 3.55 2.75 2.04 2.70 2.45 2.57 2.36 2.03 2.48.4  3.20 3.55 2.75 2.77 2.74 2.55 2.77 2.97 3.01 2.73 2.48.4  2.99 2.66 2.74 2.63 2.87 3.48 2.97 3.01 2.77 2.93 111.6  4.51 4.64 4.02 4.75 4.75 4.70 4.43 4.31 3.44 136.8  2.59 2.66 2.55 2.65 3.01 2.78 3.04 3.13 3.13 2.46 136.8  2.59 2.66 2.55 2.65 3.01 2.74 2.98 3.10 2.74 3.13 3.14 3.13 2.46 136.8  2.59 2.67 2.70 2.91 3.17 2.98 3.19 2.76 136.8  2.59 2.67 2.70 2.91 3.17 2.98 3.19 2.76 136.8  3.47 3.86 4.26 4.60 4.47 4.01 3.85 3.82 2.96 111.6
PACTOR (ASF)  OCATIONS  80.0 201.6 226.8 248.4 270.0 291.6 316.8 338.4 MIN. PLANE  5.71 5.40 4.83 4.22 5.64 5.32 4.62 4.51 3.49 111.6  4.13 3.93 3.66 3.29 3.76 4.40 3.64 3.18 2.75 111.6  3.59 3.23 2.99 2.76 3.10 3.44 3.15 3.21 2.55 90.0  3.50 3.13 2.80 2.45 2.81 2.93 2.96 2.69 2.30 90.0  3.51 3.08 2.67 2.02 2.69 2.56 2.65 2.75 2.30 248.4  3.26 3.25 2.67 2.04 2.70 2.45 2.57 2.36 2.02 248.4  3.20 3.55 2.75 2.27 2.74 2.55 2.70 2.44 2.23 90.0  3.59 2.66 2.74 2.62 2.86 2.80 2.82 2.58 2.35 90.0  3.59 2.66 2.74 2.63 2.87 3.48 2.74 2.95 2.63 2.48.4  2.99 2.66 2.74 2.63 2.87 3.48 2.74 2.95 2.63 2.48.4  2.97 3.37 3.34 3.41 3.07 3.12 3.16 3.37 2.93 111.6  4.51 4.64 4.02 4.72 4.75 4.70 4.43 4.31 3.44 136.8  2.59 2.67 2.70 2.91 3.17 2.98 3.14 3.13 3.13 3.13 3.14 3.35.8  3.47 3.86 4.26 4.60 4.47 4.01 3.85 3.82 2.96 111.6  3.64 3.99 4.67 5.12 4.50 4.47 4.79 3.97 3.64 180.0
PACTOR (ASF)  OCATIONS  80.0 201.6 226.8 248.4 270.0 291.6 316.8 338.4 MIN. PLANE  5.71 5.40 4.83 4.22 5.64 5.32 4.62 4.51 3.49 111.6  4.13 3.93 3.66 3.29 2.76 4.40 3.64 3.18 2.75 111.6  3.59 3.23 2.99 2.76 3.10 3.44 2.95 2.69 2.35 90.0  3.37 3.08 2.67 2.20 2.62 2.65 2.76 2.47 2.20 248.4  3.26 3.25 2.64 2.02 2.69 2.56 2.67 2.47 2.20 248.4  3.26 3.25 2.64 2.02 2.69 2.56 2.67 2.36 2.04 248.4  3.20 3.55 2.75 2.77 2.74 2.55 2.70 2.44 2.23 90.0  3.30 3.88 3.58 2.71 2.74 2.55 2.70 2.44 2.75 3.01  2.99 2.66 2.74 2.63 2.87 3.48 2.74 2.95 2.63 248.4  2.99 2.66 2.74 2.63 2.87 3.48 2.74 2.95 2.76 136.8  2.99 2.66 2.74 2.63 2.87 3.48 2.74 2.95 2.76 136.8  2.99 2.66 2.74 2.63 2.87 3.48 2.74 2.95 2.76 136.8  2.59 2.66 2.75 2.05 3.01 2.74 3.03 3.10 2.38 136.8  3.47 3.86 4.26 4.67 4.01 3.85 3.82 2.96 111.6  3.64 3.99 4.67 5.12 4.50 4.47 4.01 3.85 3.82 2.97 3.64 180.0
PROTOR (ASF)  OCATIONS  80.0 201.6 226.8 248.4 270.0 291.6 316.8 338.4 MIN. PLANE  5.71 5.40 4.83 4.22 5.64 5.32 4.62 4.51 3.49 111.6  4.13 3.93 3.66 3.29 3.76 4.40 3.64 3.18 2.75 111.6  3.59 3.23 2.99 2.76 3.10 3.44 3.15 3.21 2.55 90.0  3.50 3.13 2.80 2.45 2.81 2.93 2.96 2.69 2.30 90.0  3.50 3.13 2.80 2.45 2.81 2.93 2.96 2.69 2.30 90.0  3.26 3.25 2.64 2.02 2.65 2.65 2.67 2.36 2.02 248.4  3.26 3.39 2.57 2.04 2.70 2.45 2.57 2.38 2.04 248.4  3.29 2.56 2.57 2.74 2.55 2.70 2.44 2.23 90.0  3.30 3.88 3.58 2.71 3.05 3.14 2.97 3.01 2.71 248.4  2.99 2.66 2.74 2.63 2.87 3.48 2.74 2.95 2.63 248.4  2.99 2.66 2.74 2.63 2.87 3.48 2.74 2.95 2.63 248.4  2.99 2.66 2.74 2.63 2.87 3.48 2.74 2.95 2.63 111.6  4.51 4.64 4.02 4.72 4.75 4.70 4.43 4.31 3.44 136.8  2.79 2.96 2.67 2.70 2.91 3.17 2.98 3.14 3.13 2.48 136.8  3.47 3.86 4.26 4.60 4.47 4.01 3.85 3.82 2.96 111.6  3.64 3.99 4.67 5.12 4.50 4.47 4.79 3.97 3.64 180.0
BERELAIDNS         60.0 201.6 226.8 248.4 270.0 291.6 316.8 338.4 MIN. PLANE         5.71 5.40 4.83 4.22 5.64 5.32 4.62 4.51 3.49 111.6         4.13 3.93 3.66 3.29 3.76 4.40 3.64 3.18 2.75 111.6         4.13 3.93 2.80 2.45 2.81 2.93 2.96 2.69 2.75 111.6         3.50 3.23 2.80 2.45 2.81 2.93 2.96 2.69 2.80 2.80 2.47 2.20 2.48.4         3.24 3.39 2.57 2.04 2.70 2.45 2.77 2.36 2.04 2.48.4         3.26 3.25 2.64 2.02 2.65 2.65 2.70 2.47 2.23 90.0         3.27 3.08 2.57 2.74 2.55 2.70 2.44 2.23 90.0         3.29 3.74 3.04 2.70 2.45 2.57 2.38 2.04 2.48.4         3.20 3.55 2.75 2.77 2.74 2.55 2.70 2.44 2.23 90.0         3.30 3.88 3.58 2.71 3.05 3.14 2.97 3.01 2.71 2.48.4         2.97 3.37 3.34 3.41 3.07 3.12 3.16 3.37 2.93 111.6         4.51 4.64 4.02 4.02 4.75 4.70 4.43 4.31 3.19 2.76 136.8         2.58 2.66 2.55 2.65 3.01 2.74 3.03 3.10 2.78 136.8         2.59 2.66 2.74 2.02 2.87 3.01 2.74 3.03 3.10 2.76 136.8         2.97 3.37 2.95 2.65 3.01 2.78 3.04 3.16 3.13 3.19 2.76 136.8         2.59 2.66 2.55 2.65 3.01 2.74 3.03 3.10 2.78 136.8         2.59 2.67 2.70 2.91 3.17 2.79 4.77 4.79 3.03 3.10 2.78 136.8         2.59 2.67 2.70 2.91 3.17 2.79 4.77 4.79 3.03 3.10 2.76 136.8         2.59 2.67 2.70 2.91 3.17 2.79 4.77 4.79 3.03 3.10 2.76 136.8
80.0 201.6 226.8 248.4 270.0 291.6 316.8 338.4 MIN. PLAME 5.71 5.40 4.83 4.22 5.64 5.32 4.62 4.51 3.49 111.6 4.13 3.93 3.66 3.29 3.76 4.40 3.64 3.18 2.75 111.6 3.59 3.23 2.99 2.76 3.10 3.44 3.15 3.21 2.55 90.0 3.37 3.08 2.67 2.02 2.65 2.65 2.76 2.47 2.20 248.4 3.26 3.25 2.64 2.02 2.69 2.56 2.67 2.36 2.02 248.4 3.24 3.39 2.57 2.04 2.70 2.45 2.57 2.38 2.04 248.4 3.20 3.55 2.75 2.27 2.74 2.55 2.70 2.44 2.23 90.0 3.54 3.74 3.04 2.49 2.86 2.80 2.82 2.58 2.35 90.0 3.54 3.74 3.04 2.49 2.86 2.80 2.82 2.58 2.35 90.0 3.54 3.74 3.64 3.63 2.87 3.14 2.97 3.01 2.71 248.4 2.99 2.66 2.74 2.63 2.87 3.14 2.97 3.01 2.71 248.4 2.97 3.37 3.34 3.41 3.07 3.12 3.16 3.37 2.93 111.6 2.59 2.66 2.55 2.65 3.01 2.74 3.03 3.10 2.38 136.8 2.59 2.67 2.70 2.91 3.17 2.98 3.14 3.13 2.48 136.8 3.47 3.86 4.26 4.60 4.47 4.01 3.85 3.82 2.96 111.6 3.64 3.99 4.67 5.12 4.50 4.47 4.79 3.97 3.64 180.0
7.1 3.940 4.05 3.22 3.76 4.40 3.16 3.18 2.75 111.6 3.29 3.26 3.29 3.76 4.40 3.16 3.18 2.75 111.6 3.29 3.29 3.76 4.40 3.16 3.18 2.75 111.6 3.29 3.29 3.76 4.40 3.16 3.21 2.25 90.0 3.41 3.13 2.80 2.45 2.81 2.93 2.96 2.69 2.30 90.0 3.37 3.08 2.67 2.02 2.69 2.65 2.76 2.47 2.20 248.4 2.2 3.39 2.57 2.04 2.70 2.45 2.57 2.36 2.04 248.4 2.0 3.55 2.75 2.27 2.74 2.55 2.70 2.44 2.23 90.0 2.4 3.74 3.04 2.49 2.86 2.80 2.82 2.58 2.35 90.0 3.30 3.88 3.58 2.71 3.05 3.14 2.97 3.01 2.71 2.48.4 3.97 3.37 3.34 3.41 3.07 3.12 3.16 3.37 2.93 111.6 3.19 3.37 2.93 111.6 3.19 2.76 2.55 2.66 2.55 2.66 2.55 2.67 3.01 2.74 3.03 3.10 2.38 136.8 3.68 2.67 2.70 2.91 3.17 2.98 3.14 3.13 2.48 136.8 3.64 3.86 4.26 4.60 4.47 4.01 3.85 3.82 2.96 111.6 3.99 4.67 5.12 4.50 4.47 4.79 3.97 3.97 3.64 180.0
4.13 5.93 5.00 5.29 5.70 4.40 5.04 5.10 7.10 1.10 1.10 1.10 1.10 1.10 1.10 1
3.59 3.23 2.99 2.76 3.10 3.44 3.15 3.21 2.55 90.0 3.50 3.13 2.80 2.45 2.81 2.93 2.96 2.69 2.30 90.0 3.51 3.08 2.67 2.02 2.65 2.65 2.47 2.20 248.4 3.26 3.25 2.64 2.02 2.69 2.56 2.67 2.36 2.02 248.4 3.26 3.25 2.64 2.02 2.69 2.56 2.67 2.36 2.02 248.4 3.20 3.55 2.75 2.27 2.74 2.55 2.70 2.44 2.23 90.0 3.54 3.74 3.04 2.49 2.86 2.80 2.82 2.58 2.35 90.0 3.30 3.88 3.58 2.71 3.05 3.14 2.97 3.01 2.71 248.4 2.99 2.66 2.74 2.63 2.87 3.48 2.74 2.95 2.63 248.4 4.51 4.64 4.02 4.72 4.75 4.70 4.43 4.31 3.44 136.8 2.97 3.37 3.34 3.41 3.07 3.12 3.16 3.19 2.76 136.8 2.58 2.66 2.55 2.65 3.01 2.74 3.03 3.10 2.38 136.8 3.47 3.86 4.26 4.60 4.47 4.01 3.85 3.82 2.96 111.6 3.64 3.99 4.67 5.12 4.50 4.47 4.79 3.97 3.64 180.0
3.50 3.13 2.80 2.45 2.81 2.93 2.96 2.69 2.30 90.0 3.37 3.08 2.67 2.20 2.65 2.76 2.47 2.20 2.48.4 3.25 3.25 2.64 2.02 2.69 2.56 2.76 2.47 2.20 2.48.4 3.24 3.39 2.57 2.04 2.70 2.45 2.57 2.38 2.04 2.48.4 3.20 3.55 2.75 2.77 2.77 2.55 2.70 2.44 2.23 90.0 3.54 3.74 3.04 2.97 2.82 2.55 2.70 2.44 2.35 90.0 3.54 3.04 2.49 2.86 2.80 2.82 2.58 2.59 2.66 2.74 2.65 2.80 2.82 2.58 2.58 2.35 90.0 2.97 3.31 3.34 3.41 3.05 3.14 2.97 3.01 2.71 2.48.4 2.97 3.37 3.34 3.41 3.05 3.14 2.97 3.01 2.71 2.48.4 136.8 4.51 4.64 4.02 4.72 4.75 4.70 4.43 4.31 3.44 136.8 2.59 2.66 2.55 2.65 3.01 2.74 3.03 3.10 2.38 136.8 2.59 2.67 2.70 2.91 3.17 2.98 3.14 3.13 2.48 136.8 3.47 3.86 4.26 4.67 4.77 4.01 3.85 3.82 2.96 111.6 3.64 3.99 4.67 5.12 4.50 4.47 4.01 3.85 3.82 2.96 111.6
.37         3.08         2.67         2.62         2.65         2.76         2.47         2.20         248.4           .26         3.25         2.64         2.02         2.69         2.56         2.67         2.36         2.02         248.4           .20         3.55         2.77         2.46         2.57         2.33         248.4           .20         3.55         2.77         2.74         2.55         2.70         2.44         2.23         90.0           .54         3.74         2.55         2.74         2.55         2.35         90.0           .30         3.88         3.58         2.74         2.95         2.71         248.4           .99         2.66         2.74         2.63         2.81         3.74         2.95         2.63         248.4           .97         3.37         3.34         3.41         3.07         3.15         3.19         3.19         3.74         136.8           .51         4.40         4.75         4.75         4.75         4.74         3.03         3.19         2.76         136.8           .58         2.66         2.55         2.65         3.01         2.74         3.03
26         3.25         2.64         2.02         2.69         2.56         2.67         2.36         2.02         248.4           20         3.55         2.75         2.70         2.45         2.57         2.38         2.04         248.4           20         3.55         2.75         2.77         2.70         2.45         2.57         2.38         2.04         248.4           30         3.64         3.04         2.49         2.86         2.80         2.82         2.35         90.0           30         3.68         2.80         2.87         2.97         3.01         2.71         248.4           30         3.68         2.80         3.14         2.95         2.71         248.4           97         3.37         3.34         3.41         3.34         311.6         3.31         3.44         136.8           93         3.01         2.74         3.03         3.19         3.19         2.76         136.8           19         2.65         3.01         2.74         3.03         3.10         2.38         136.8           19         2.65         3.01         2.74         3.03         3.13         2.48
24     3.39     2.57     2.04     2.70     2.45     2.57     2.38     2.04     248.4       .20     3.55     2.75     2.27     2.74     2.55     2.70     2.44     2.23     90.0       .54     3.74     3.04     2.80     2.82     2.58     2.35     90.0       .30     3.88     3.58     2.71     3.05     3.14     2.97     3.01     2.71     248.4       .99     2.66     2.74     2.63     2.87     3.16     3.37     2.93     111.6       .91     3.37     3.34     4.31     3.44     136.8       .79     2.96     3.01     2.74     3.03     3.10     2.74     136.8       .58     2.66     2.55     2.65     3.01     2.74     3.03     3.10     2.38     136.8       .59     2.67     2.70     2.91     3.17     2.98     3.14     3.13     2.48     136.8       .47     3.86     4.57     4.67     4.01     3.85     3.82     2.96     111.6       .64     3.99     4.67     5.12     4.50     4.47     4.79     3.97     3.64     180.0
.20     3.55     2.75     2.27     2.74     2.55     2.70     2.44     2.23     90.0       .30     3.88     3.58     2.71     3.05     3.14     2.97     3.01     2.71     248.4       .99     2.66     2.74     2.63     2.87     3.48     2.74     2.95     2.63     248.4       .97     3.37     3.34     3.41     3.07     3.12     3.16     3.37     2.93     111.6       .51     4.64     4.02     4.75     4.70     4.43     4.31     3.44     136.8       .78     2.66     2.55     2.65     3.04     3.16     3.19     2.76     136.8       .59     2.67     2.70     2.91     3.17     2.98     3.14     3.13     2.48     136.8       .59     2.67     2.70     2.91     3.17     2.98     3.14     3.13     2.48     136.8       .47     3.86     4.26     4.60     4.47     4.01     3.85     3.82     2.96     111.6       .64     3.99     4.67     5.12     4.50     4.47     4.79     3.97     3.64     180.0
.54         3.74         3.04         2.49         2.86         2.80         2.82         2.58         2.35         90.0           .30         3.88         3.58         2.71         3.05         3.14         2.97         3.01         2.71         248.4           .99         2.66         2.74         2.63         2.87         3.48         2.74         2.95         2.63         248.4           .97         3.37         3.34         3.41         3.07         3.12         3.16         3.37         2.93         111.6           .79         2.96         3.01         2.78         3.04         3.16         3.19         2.76         136.8           .59         2.67         2.95         2.65         3.01         2.74         3.03         3.10         2.38         136.8           .59         2.67         2.95         2.65         3.01         2.74         3.03         3.14         3.13         2.48         136.8           .47         3.86         4.26         4.60         4.47         4.01         3.85         3.82         2.96         111.6           .64         3.99         4.67         5.12         4.57         4.4
.30         3.88         3.58         2.71         3.05         3.14         2.97         3.01         2.71         248.4           .99         2.66         2.74         2.63         2.87         3.48         2.74         2.95         2.63         248.4           .97         3.37         3.34         3.41         3.07         3.12         3.16         3.37         2.93         111.6           .51         4.64         4.02         4.72         4.75         4.70         4.43         4.31         3.44         136.8           .79         2.96         3.01         2.74         3.03         3.19         2.76         136.8           .58         2.65         2.65         3.01         2.74         3.03         3.10         2.38         136.8           .59         2.67         2.70         2.91         3.17         2.98         3.14         3.13         2.48         136.8           .47         3.86         4.60         4.47         4.01         3.85         3.82         2.96         111.6           .64         3.99         4.67         5.12         4.50         4.47         4.79         4.79         3.97         3.
.99     2.66     2.74     2.63     2.87     3.48     2.74     2.95     2.63     248.4       .97     3.37     3.34     3.41     3.07     3.12     3.16     3.37     2.93     111.6       .51     4.64     4.02     4.72     4.75     4.70     4.43     4.31     3.44     136.8       .79     2.96     3.01     2.78     3.04     3.16     3.19     2.76     136.8       .59     2.66     2.55     2.65     3.01     2.74     3.03     3.10     2.38     136.8       .59     2.67     2.70     2.91     3.17     2.98     3.14     3.13     2.48     136.8       .47     3.86     4.56     4.60     4.47     4.01     3.85     3.82     2.96     111.6       .64     3.99     4.67     5.12     4.50     4.47     4.79     3.97     3.64     180.0
.97 3.37 3.34 3.41 3.07 3.12 3.16 3.37 2.93 111.6 .51 4.64 4.02 4.72 4.75 4.70 4.43 4.31 3.44 136.8 .79 2.96 3.01 2.78 3.04 3.16 3.19 3.19 2.76 136.8 .58 2.66 2.55 2.65 3.01 2.74 3.03 3.10 2.38 136.8 .59 2.67 2.70 2.91 3.17 2.98 3.14 3.13 2.48 136.8 .47 3.86 4.26 4.60 4.47 4.01 3.85 3.82 2.96 111.6 .64 3.99 4.67 5.12 4.50 4.47 4.7 4.79 3.97 3.64 180.0
.51 4.64 4.02 4.72 4.75 4.70 4.43 4.31 3.44 136.8 .79 2.96 3.01 2.78 3.04 3.16 3.19 3.19 2.76 136.8 .58 2.66 2.55 2.65 3.01 2.74 3.03 3.10 2.38 136.8 .59 2.67 2.70 2.91 3.17 2.98 3.14 3.13 2.48 136.8 .47 3.86 4.26 4.60 4.47 4.01 3.85 3.82 2.96 111.6 .64 3.99 4.67 5.12 4.50 4.47 4.79 3.97 3.64 180.0
.79 2.96 3.01 2.78 3.04 3.16 3.19 3.19 2.76 136.8 .58 2.66 2.55 2.65 3.01 2.74 3.03 3.10 2.38 136.8 .59 2.67 2.70 2.91 3.17 2.98 3.14 3.13 2.48 136.8 .47 3.86 4.26 4.60 4.47 4.01 3.85 3.82 2.96 111.6 .64 3.99 4.67 5.12 4.50 4.47 4.79 3.97 3.64 180.0
.58 2.66 2.55 2.65 3.01 2.74 3.03 3.10 2.38 136.8 .59 2.67 2.70 2.91 3.17 2.98 3.14 3.13 2.48 136.8 .47 3.86 4.26 4.60 4.47 4.01 3.85 3.82 2.96 111.6 .64 3.99 4.67 5.12 4.50 4.47 4.79 3.97 3.64 180.0
.59 2.67 2.70 2.91 3.17 2.98 3.14 3.13 2.48 136.8 .47 3.86 4.26 4.60 4.47 4.01 3.85 3.82 2.96 111.6 .64 3.99 4.67 5.12 4.50 4.47 4.79 3.97 3.64 180.0
.47 3.86 4.26 4.60 4.47 4.01 3.85 3.82 2.96 111.6 .64 3.99 4.67 5.12 4.50 4.47 4.79 3.97 3.64 180.0
.64 3.99 4.67 5.12 4.50 4.47 4.79 3.97 3.64 180.0
0.004 POIN 1614 PIN DOIN 1810 1018 NOT BOIN

TWR-17546 Vol. III

	¥+3	•	٠	•	•	٠	σ.	9.	•	٧		•	•	•	? (		•	7	•	'n			٠																					
	•	9	m	<b>6</b>	m	-4	æ	7	80	_			4 6	<b>,</b>	n 1	m	4	7	~						URE	ы							æ											
	MAX	4.	∞.	6.	٥.	€.	٥.	6.		4	. ~	. ~		•		•	7	Ξ.	0	1.01					EXPOS	T	22	6	1 4	7	11	0 8	105.	03	10	~	m	m	g	7	9	Ω	-	4
	EDIAM	. 12	. 47	. 64	.70	. 65	. 58	. 55	. 45	-	1 2	7	•		? ;	. 94	. 0 4	00.	. 78	.803						AVE.		_	. ~	. 4	. 4	4	14.3	س	2	Ξ.	7	س	φ.	5	ë.	m	<b>:</b>	
	<b>=</b>								Ų											9						4	_					. ~	7	_	_			~	۱,0		10			_
	338.4	. 18	.61	. 53	. 75	. 76	.72	. 65	. 55	4.0	4			7	9 7	. 93	96.	.93	. 8 1	0.95						338.	•	,	. ~	` '		9	15.	Š.	ش	_;	?	۳.	9.	۲,		٠	<b>:</b>	5
	16.8	. 14	. 41	. 57	.60	.60	. 54	. 55	. 42	-	-		•		71.	. 94	.97	.93	8 0	.791						16.8	•	_	. ~	• •	4	4	14.7	ص	m	7	m.	m	ę.	۲,	7	7	<b>-</b>	
	91.6 3	966	168	437	909	653	009	614	503	323	122		) 0		9 9	943	060	973	778	.828 0						91.63	•				. 4	4	15.3	4	m.	Ξ.		4	<b>.</b>	ζ.	4.	٠	。	급.
	0.0	32 0	84 1	20 1	11 1	07 1	59 1	02 1	21 1	16.1	67 1	17	•	7 4	9	79 0	68 1	24 0	94	816 0						0.0					, m	*	4.3	89.	0.	6.	۰.	7.	9.	٠	٠	٠	٠	•
	.4 27	8 0.	3 1.	8 1.	6 1.	1.1.	3<1.	7<1.	5<1.	4		; -			, ,	0	. 0 9	5 0.	8 0.	15 0.	1	TERIA	_			.4 27		-	•	۰-	1 6	7 1	.4 1	2 1	6 1	0	1 1	9 1	7	5 1	2 1	3 1	4	6 1
	8 248	1.2	1.5	1.7	1.9	1.9	2.0	1.9	1.6	1 4	1 2		•	7	٠ ٠	1.0	1.0	6.0	9.0	3 0.7		CRIT	(MDR			8 248	-	-	• -	•	٠.	-	6 18			-	-	~		-	7	-		
	226.	.09	. 42	99.	. 70	. 65	. 55	. 54	. 38	2.0	96	, ,	, ,	5	۷,	. 97	. 13	. 05	. 70	0.78		ESIGN	AATE			226.	•	_	. 4	. 4	. 4	4	14.	۳.	Ξ.	9.	س	7	。	5.	•	4.	٠	
SNC	201.6	96.	.31	. 54	. 50	. 42	. 25	.16	90.	9		, ,	• •	<u> </u>	? :	66.	.09	90.	. 79	0.954		GMA D	ITION		ONS	201.6	•	_	: ~	· ~		; ;	11.0		σ.	ď	۳.	۲,	•	;	4.	•	<b>:</b>	7.
OCATI	80.0	.926	.239	.376	.347	. 299	.260	. 225	.191	037	0.54	191	4 6		. / 1.3	.062	.153	.122	. 892	.015		3 81	OMPO	SECOND	OCATI			_	; <u>-</u>				11.6	Ξ.	0	。	۲,	4	9	m.	Ŋ.	Š.	ς.	m.
GREE L	8 4.	992	236	165	890	015	949	906	876	113	796	7 7 6	, c	701	706	883	900	0 2 0	706	.881 1		T W	I DE	\	REE	4	•		•	•		•	9.8	•	•	•	ij	4.	≓	ij	•	۳.	٠	•
DE	6.8 1	0.1	33	55	62	632	475	423	267	1 1 8	0 4 6	9,0	, ,	70	4 t	73	224	162	55	719 0		DED T		Ĭ	DE	6.8	•	^			4	, m	3.5	2	Ξ.	。	m,	m	≓		ģ	δ.	٠	•
	.6 13	96	63	8 2	36	77 1	55 1	24 1	89	57.1		1 -	• •	0 0	٠.	62	66	1 90	43	20 0.		EXCEE	~			.6 13		ď	· -	• •	. 0	. ~	4.	4.	₹.	٠.	۳.	٥.	<b>-</b> :	٦.	4.	٠.	٠	
	0 111	-	H	-	-	-	-	:	1.	-	: <u>-</u>			; ,			<b>.</b> ;	Ξ.	-	6.0 6		HAS				0 111	-	_	-	٠-	٠.	ı <del>-</del>	6 15	-	-	-		-		_	1	-	-	-
	06	. 32	.74	. 93	. 05	96.	.89		.72	ď		: :		9 1		. 91	.07	.03	60	0.83		G MDD				90.			, 4	, α	-	-	17.	9	S	~	0	~	6	-	4		~	
	68.4	. 99	. 33	. 47	. 49	.38	. 25	. 28	. 22	1.2			•	- :	?	. 78	. 93	.02	. 8 7	0.662		CEDIN				68.4		_	•	. ~	. 2		12.2	1.	_;	0	۲,	ن	•		۲,	٠	5.	•
	46.8	195	578	730	169	089	673	560	479	5.5	142		3 6	7 1	7 3 0	992	974	980	647	. 697		E PRE				46.8		~	. 4	. 4			14.8	4	د	_;		4.	6	7	۲,	س	•	•
	1.6	974 1	519 1	753 1	754 1	653 1	617 1	553 1	495 1	167 1	127 1	737	• •	7 7/7	804 040	8360	8900	925 0	625 0	729 0		ES TH				1.6	•	7 7	. c	. 4	. 6.	6.	4.7	4.5	3.5	1.5	3.1	5.2	0.2	8.0	1.6	2.3	•	•
	.0 2	72 0	94 1	54 1	49 1	27 1	55 1	97<1	23<1	5.7	20 1	, -	•	7 0 0	4 5 0 -	78 0	46 0	800	89.0	37 0.		DICAT				2 0.0		-		. ~		. 7	1.1	89.	4.	5.	0.	6.	₹.	۳.	₹.	٦.	•	•
NO	•	•	٠	٠		٠	•	•	•		•	•	•	•	•	٠	•	•		0.7		Z H			NO		-	-	- ۱	• -	-	1	16	1	-	-	7	-		7	7	₩.	7	
	$\vdash$	•		7	د	4.	9	7	8			•			:		7	δ.	~	53.0		~ = !			H	(II)		_		. ~	. 4	9	17.3	٠.	6	_;	4	س	7.		2	S.	•	m.

MOTOR ACTION TIME = 122.9 SECONDS

	PERFORMANCE
LE 21	INSULATION
TABLE	DOME
	AFT
	RSRM-7B

PREFIRE MEASUREMENTS INCHES

### STATE OF THE PROPERTY OF T	HOM	4 4 4 4 4 6 8 8 8 8 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	
THE PART OF THE PART OF THE PART PROPRETE LOCATIONS  10. 2.1.6 46.6 46.6 46.7 4 90.0 111.6 136.4 180.7 6 126. 226.8 124.4 270.0 291.6 116.8 338.4 HWAS LOCATIONS S. 2.2 2.2 2.2 2.2 2.2 2.2 2.2 2.2 2.2	Ω Ω	8 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	8
### PARTION  10. 1 5.05 5.14 6.14 6.14 6.14 6.11 6.10 6.15 6.15 1.10 6.10 6.10 6.10 6.10 6.10 6.10 6.10	NH		H
PARTION  0.0 21.6 46.8 68.4 90.0 111.6 136.8 158.4 180.0 201.6 226.8 248.4 270.0 291.6 316  9.3 5.225 5.214 6.314 5.314 5.314 5.315 5.103 5.131 5.115 5.115 5.103 5.105 5.205 5.305 5.205  10.7 5.029 5.036 5.106 5.125 5.008 5.123 5.135 5.103 5.118 5.115 5.103 5.103 5.205 5.308 5.205  10.1 6.919 4.300 4.301 4.301 4.301 4.301 4.301 5.131 5.101 5.101 5.101 5.003 5.205 5.301 4.301  10.1 6.919 4.301	338.	R	8 8 7 1 L 8 7 4 2 8 1 1 2 8 1 2 4 2 8 1 1 L 8 1 2 4 2 1 L 1 L 1 L 1 L 1 L 1 L 1 L 1 L 1 L 1
9. 3 5. 225 5. 214 5.114 5.125 5.208 5.123 5.123 5.113 5.175 5.286 5.103 5.135 5.208 5.100 5.100 7.0 5.065 5.065 5.106 5.126 5.226 5.100 5.125 5.208 5.123 5.123 5.123 5.123 5.123 5.123 5.125 5.208 5.120 5	6 316	7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00	6 1100000000000000000000000000000000000
TATTON  O. 21.6 46.8 68.4 90.0 111.6 136.8 158.4 186.0 201.6 226.8 246.4 2  10.7 5.065 5.065 5.166 5.180 5.125 5.208 5.125 5.115 5.115 5.115 5.105 5.139 5.135 5.135 5.101 5.115 5.105 5.115 5.105 5.130 5.135 5.135 5.101 5.115 5.105 5.105 5.135 5.135 5.101 5.115 5.105 5.105 5.135 5.135 5.105 5.105 5.135 5.135 5.105 5.105 5.135 5.135 5.105 5.105 5.135 5.135 5.105 5.105 5.135 5.135 5.105 5.105 5.135 5.135 5.105 5.105 5.105 5.135 5.135 5.105 5.105 5.135 5.135 5.105 5.105 5.135 5.135 5.105 5.105 5.135 5.135 5.105 5.105 5.135 5.135 5.105 5.105 5.135 5.135 5.105 5.105 5.135 5.135 5.105 5.105 5.135 5.135 5.105 5.105 5.135 5.135 5.105 5.105 5.135 5.135 5.105 5.105 5.135 5.135 5.105 5.105 5.135 5.135 5.105 5.105 5.135 5.135 5.105 5.105 5.135 5.105 5.135 5.105 5.105 5.135 5.105 5.105 5.105 5.135 5.105 5.1	0.0 29	260 2000 0027 4 8 116 109 116 117 127 128 139 139 139 139 139 139 139 139 139 139	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
FTATION  9. 3 5.225 2.14 6.16 68.4 90.0 111.6 136.8 158.4 180.0 201.6 226.  9. 3 5.225 2.14 6.14 90.0 111.6 136.8 158.4 180.0 201.6 226.  10. 3 5.225 2.14 6.14 9.10 4.91 4.91 9.10 11.15 9.128 5.131	48.4.2	2	8
FIATON  9.3 5.252 5.214 5.314 5.324 5.301 5.219 5.278 5.211 5.288 5.18 15.0 201.  9.4 5.252 5.214 5.314 5.324 5.301 5.219 5.278 5.211 5.288 5.18 15.0 2 5.28 5.18 5.38 5.38 5.38 5.38 5.38 5.38 5.38 5.3	226.	R R 4 4 4 4 8 8 8 8 8 8 8 8 8 8 8 8 8 8	R N S S S S S S S S S S S S S S S S S S
9.3 5.252 5.214 5.314 5.324 5.371 5.219 5.278 5.211 5.2 10.7 5.069 5.056 5.160 5.125 5.208 5.123 5.133 5.103 5.1 11.4 4.331 4.392 4.356 4.302 4.912 4.912 4.913 4.915 4.911 4.4 4.910 4.910 4.951 4.952 4.907 4.911 4.910 4.910 4.953 4.925 4.907 4.911 4.910 4.911 4.910 4.912 4.911 4.910 4.911 4.910 4.911 4.910 4.911 4.910 4.911 4.910 4.911 4.910 4.911 4.910 4.911 4.910 4.911 4.910 4.911 4.910 4.911 4.910 4.911 4.910 4.911 4.910 4.911 4.910 4.911 4.911 4.910 4.911 4.911 4.910 4.911 4.911 4.910 4.911 4.91	TIONS 0 201.	8 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	EASURE 110 NS URE 2 2 3 4 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
TTATION  0.0 21.6 46.8 68.4 90.0 111.6 136.8 1  9.3 5.252 5.214 5.314 5.324 5.371 5.219 5.278 5  10.7 5.069 5.056 5.160 5.125 5.208 5.123 5.133 5  11.0 4.919 4.930 4.961 4.940 4.953 4.925 4.607 4  114.4 4.331 4.392 4.356 4.382 4.374 4.308 4.335 4  116.0 4.117 4.142 4.085 4.097 4.112 4.028 4.046 4  116.0 4.117 4.142 4.085 4.097 4.112 4.028 4.046 4  116.0 4.117 4.142 4.085 4.097 4.112 4.028 4.046 4  116.1 3.1 4.392 4.356 4.382 3.985 3.946 3.916 4  116.2 3.168 3.613 3.623 3.916 3.955 3.946 3  116.3 3.468 3.479 3.516 3.523 3.452 3  121.3 3.501 3.518 3.479 3.516 3.523 3.452 3  121.3 3.10 3.311 3.361 3.913 3.516 3.551 3.452 3  121.3 3.468 3.793 2.932 2.937 2.993 2.917 2.908 2  45.0 2.970 2.948 3.918 3.516 3.503 3.651 3.661 3.664 3  10.0 3.9140 3.618 3.618 3.516 3.263 3.218 3.551 3.034 3  10.1 3.1 3.1 3.1 3.1 3.1 3.1 3.1 3.61 3.1 3.62 3  10.2 3.970 2.948 2.952 2.932 2.993 2.993 2.907 2.908 2  48.0 3.311 3.788 3.618 3.619 3.609 3.657 3.711 3  PART NO. 1U76658-01  2.772 3.368 3.31 3.33 4.049 3.723 4.077 4  10.7 3.352 3.342 3.	REE LO 8.4 18	1011 1011 1012	NTT CHE C IN C I
FTATION  (IN)  9.3 5.252 5.214 5.314 5.324 5.371 5.21  10.7 5.069 5.056 5.160 5.125 5.208 5.12  12.0 4.919 4.930 4.961 4.940 4.953 4.37  13.1 4.697 4.710 4.744 4.712 4.715 4.66  14.4 4.331 4.392 4.356 4.382 4.374 4.30  16.0 4.107 4.000 3.968 3.968 3.983 4.36  18.5 3.864 3.865 3.813 3.856 3.79  19.5 3.708 3.703 3.672 3.710 3.718 3.65  21.3 3.864 3.865 3.813 3.832 3.856 3.79  19.5 3.708 3.703 3.672 3.710 3.718 3.65  21.3 3.861 3.983 3.516 3.985 3.985  24.0 0 2.998 2.988 3.983 2.993 2.994  25.0 2.970 2.998 2.982 2.993 2.993 2.994  45.0 2.970 2.998 2.922 2.932 2.993 2.994  45.0 2.970 2.998 2.926 2.936 3.963 3.085  24.0 0 2.970 2.998 2.963 3.069 3.65  PART NO. 1076658-01  STATION  (IN) 0.0 21.6 46.8 68.4 90.0 111.  9.3 3.880 4.240 4.119 4.333 4.049 3.72  10.7 3.353 3.373 3.582 3.786 3.014 3.36  14.4 2.604 2.739 2.676 2.993 2.15 2.37  16.0 2.362 2.352 2.412 2.789 2.215 2.215  24.1 3 2.381 2.370 2.334 2.610 2.128 2.215  24.2 3.38 2.216 2.473 2.662 2.845 2.789  25.7 2.57 2.57 2.57 2.57 2.57 2.57 2.57	DE 36.8 1	7.2.2 9.00.3	36
STATION  (IN)  9.3 5.252 5.214 5.314 5.324 5.37  10.7 5.069 5.056 5.160 5.125 5.20  12.0 4.919 4.710 4.744 4.712 4.715  14.4 4.331 4.392 4.356 4.382 4.37  16.0 4.117 4.142 4.085 4.097 4.11  11.3 3.854 3.865 3.813 3.832 3.85  19.5 3.708 3.703 3.672 3.710 3.71  21.3 3.501 3.783 3.473 3.51 3.85  42.0 2.970 2.948 3.968 3.985 3.98  42.0 2.970 2.948 3.965 3.310 3.75  42.0 2.970 2.948 2.926 2.948 2.92  42.0 2.970 2.948 2.926 2.948 2.92  42.0 2.970 2.948 2.926 2.948 2.92  42.0 2.970 2.948 2.926 2.948 2.92  45.0 2.970 2.948 2.926 2.948 2.92  45.0 2.970 2.948 2.926 2.948 2.92  45.0 2.970 2.948 2.926 2.948 2.92  45.0 3.317 3.361 3.569 3.119 3.08  55.0 3.610 3.659 3.059 3.139 3.08  55.1 3.3 3.5 3.3 3.3 3.3 3.3 3.2 3.0  55.1 3.3 3.5 3.3 3.3 3.3 3.3 3.3 3.3 3.3 3.3	111.	R R A A A A E E E E E E E E E C C C E E C C C C	11 1 2 2 2 2 2 3 3 3 3 4 2 2 2 2 2 2 2 2 2 2
FIRTION  9.3 5.252 5.214 5.314 5.31  10.7 5.069 5.056 5.160 5.11  12.0 4.919 4.930 4.961 4.991  14.4 4.331 4.392 4.356 4.3  16.0 4.117 4.142 4.085 4.091  17.3 4.004 4.000 3.968 3.9  18.5 3.704 3.703 3.703 3.75  24.3 3.468 3.448 3.479 3.5  24.3 3.468 3.448 3.479 3.5  24.3 3.468 3.448 3.479 3.5  24.3 3.468 3.468 3.5  37.0 2.979 2.952 2.932 2.9  42.0 2.979 2.952 2.932 2.9  42.0 2.979 2.952 2.932 2.9  42.0 2.979 2.952 2.932 2.9  42.0 3.317 3.361 3.58 3.7  37.0 3.317 3.361 3.68 3.610 3.6  PART NO. 1U76658-01  STATION  0.0 21.658-01  STATION  0.0 21.658-01  10.7 3.165 3.177 3.231 3.4  11.3 2.3375 3.537 3.537 2.311 3.4  11.3 2.337 2.447 2.408 2.7  11.3 2.337 2.447 2.408 2.7  11.3 2.337 2.447 2.408 2.7  12.0 3.165 3.177 3.231 3.4  14.4 2.604 2.739 2.676 2.9  16.0 2.352 2.316 2.317 2.331 2.337 2.4  24.3 3.30 2.331 2.331 2.331 2.337 2.4  24.3 2.331 2.331 2.331 2.331 2.337 2.4  24.3 2.331 2.331 2.331 2.331 2.337 2.4  24.3 2.331 2.331 2.331 2.331 2.337 2.4  24.0 0 2.120 2.102 1.997 2.1  42.0 2.033 2.062 1.958 1.9  48.0 2.251 2.434 2.412 2.2  5.959 2.913 2.99	90.	2 2 3 3 3 5 5 6 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	4 8 8 8 8 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9
FTATION  (IN)  9.3 5.252 5.214 5. 12.0 4.919 4.930 4. 13.1 4.697 4.710 4. 14.4 4.331 4.392 4. 16.0 4.117 4.142 4. 17.3 4.004 4.000 3. 18.5 3.764 3.865 3. 19.5 3.706 3.468 3.468 3. 33.0 3.71 3.518 3. 42.0 2.998 2.938 2.938 2. 45.0 2.979 2.952 2. 45.0 2.979 2.952 2. 45.0 2.979 2.952 2. 45.0 3.317 3.361 3. 10.7 3.375 3.537 3. 11.0 3.165 3.177 3. 12.0 3.165 3.177 3. 13.1 2.948 2.956 3. 14.4 2.604 2.739 2. 16.0 2.362 2.525 2. 16.0 2.362 2.525 2. 17.3 2.307 2.447 2. 18.5 2.331 2.370 2. 18.5 2.331 2.370 2. 18.5 2.331 2.370 2. 21.3 2.338 2.216 2. 24.3 3.0 2.571 2.508 2. 24.3 3.0 2.571 2.508 2. 24.3 3.0 2.571 2.508 2. 24.0 2.120 2.102 1. 24.0 2.120 2.102 1. 24.0 2.251 2.334 2.	<b>89</b>	14 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	8
PTATION  (IN)  9.3  10.7  12.0  4.919  14.4  14.6  14.	1.6 4	0214 03130 03130 0410	88-01 002 1.6 4 240 4. 5347 3. 5347 3. 5340 2. 336 2. 336 2. 216 2. 102 1. 062 1. 062 1.
A A A A A A A A A A A A A A A A A A A	0.0	252 0690 09199 06919	. 10766 NO. 0000 3.880 4 3.375 3 3.948 2 2.948 2 2.9604 2 2.362 2 2
	TATIO (IN)	900 W 4 6 L 8 9 H 4 W L 0 Z Z 8 8 W	SEART A C C C C C C C C C C C C C C C C C C

PART NO. 1U76668-03 SERIAL NO. 0000006

	PERFORMANCE	
4	INSULATION	
41051	CYLINDER	
	AFT	
	RM-7B	

COMPLIANCE SAFETY FACTOR (CSF)

STATION	•	3 1 6	4	4.8	0	111.6	DE	EGREE 1 158.4	LOCATIONS 180.0 201	٠	226.8 2	248.4	270.0	291.6	316.8 3	338.4	HIN.	PLANE	REQUIRED S.F.
	•	•	,	,	,	)	) , )	•	! !		 								
9	4	. 7	m.	٦.	6	٦.	∞.	'n	6.	9.	m.	m.	'n	۲.	٦.	4.	ď	٠	
χ.	80	₩.	0	٥.	80	0	7.	9.	'n	~	~	۲.	0	€.	٦.	7	'n	80.	
	2	4.	4	7	S	۲.	0	7	'n		σ.	۲.	•	٥.	٠.	m.	4	₩.	
	٦	4	4		6	~	7	∞.	0	٥.	6	7	5	•	$\sim$	Š	۲.	8.4	
	! -!		ī	~	m	3.12	ī,	3.95	0	3.76	٦.	3.22	'n	3.64	9.	7.87	•	。	•
'n	7	6	~	٦.	~	٦.	~	7	0	٠.	m	٦.	. 2	∞.	7	٠.	۲.		
	,	9	'n	٦.	6		6	∞.	•	٦.	٦.		0	٥.	7	7	9.		•
0.86	2.07	2.57	2.73	2.37	2.81	4	2.29	4.	2.28		2.53	6.	2.70	۳.	2.59	٦.	2.07	0.0	1.5
	7		4		6		7		٣.		4		9		'n		~	36.	
91	4		60		0		3		7		7		9		'n		4.	26.	
24	4		4		7		4,		0	•	~		5		7		7.	26.	
	E.		9	1	€0		٣.			•	7		7.		٦.		7	•	•
5	7		7		0		7		7		7		w.		0		٠.	16.	
89	m		4		7		٣.		Ψ,		۳.		7		7		~		•
89	0		80		0		9.		7		۲.		'n		6.		۰.	9	•
77.	۳.		4		٣.		۳.		۳.		9		۲.		r,		m,		
92.	7		6.		s.		۰		۲,		9.		9.		4.		₹.	16.	•
02	٥.		4		9.		6.		7		S		₩.		۲.		₹.	Ö	•
14.	∞.		9		m.		4		7		.5		9.		۳.		۳.	16.	•
27.	٦.		۲.		4		9.						6		σ,		۰.	36.	•
80	m		6		.5		6.		9.		€.		6.		9.		۳.	•	•
50	8		ε.		8		8		4		٣.		'n		4.	٠	٣.	26.	•
67.	∞.		٦.		9.		4.		9.		۳.		*		7		۳.	Ġ.	•
80	Τ.		S		8		8		9.		٥.		9.		٠.		ĸ.	•	•
99	٦.		7		۰		9.		٦.		٦.		٠.		7.		≈.	ö	•
22.	S.		٥.		7	•	٦.		6.		∞.		Ľ.		~		₩,	•	•
39.	4		Ψ.		٥.		٦.		٦.		7		*		S.	•	ĸ.	16.	•
44.	4		۳.		.5		. 2		٥.		۳.		7		'n		ς.	ġ	•
58.	4		٥.		∞.		8		٦.		≈.		٥.		σ.		∹	80.	•
63.	8						٠.		9.		∞,		7		'n.		'n.	16.	•
67.	٥.		5.6		+		٦.		₹.		7.		'n		7		ĸ;	70.	•
72.	+		80		۲.		+		∹		۲.		S.		7		Ξ.	16.	•
'n	00.09		8.7		9.80		13.71		4		٥.		'n		ς.		Γ.	316.8	•
77.	+		+		+		+		٥.		+		+		'n		ς.	80.	•

SEGMENT MINIMUM = 2.04 AT THE 145.5 INCH STATION A " + " MEANS NEGLIGIBLE MDD HAS OCCURRED

TWR-17546 Vol. III

PERFORMANCE
INSULATION
CYLINDER
AFT
RSRM-78

ACTUAL SAFETY FACTOR (ASF)

REQUIRED	k. v)	2.0								1.5																										
	PLANE		80.		68.	180.0	<del>.</del>	Ξ.	Ö	136.8	26.	26.	Ġ	16.	16.	36.	36.	16.	80	Ö	ė	o	26.	Ö	8	90		16	4 6	8	16	70	16	9	0	
	MIN.	9	~	7	6	7	4	0	7	2.30	4	4	S	0	~	-	•	σ,	₹.	₹.				٦.	٠.	٠:	Ξ.	۳.	٦.	~.	٠;	٦.	٦.	•	-:	
	338.4	4.2	5.7	6.1	9.3	8.79	8.3	4.8	5.3																											
	316.8	~	9	7	7	g	9	9	~	2.60	9	•	S	0	~	•	•	9	•	•	7		٠:	-:	٠:	Ξ.	٦.	~	∹	٦,	٠;	•	٦.	٠,	٦.	
	291.6	4.5	4.3	4.4	4.2	4.11	4.6	4.0	3.0																											
	270.0	m	m	-	40	40	9	4	4	2.80	0	9	•	m	m	_	_	'n	•	•	w,	٥.	W)	7.	۳.	17	-:	١.	٠;	٧:	٦.	٦.	٠:	٦.	+	
	248.4	۳.	0	ς.	S	3.48		٦.	80																											
	226.8	~		m	7	~	0	4		2.50	4	4	9	N	4	~	0	0	41		۳,	5		٠,	''	٠.	Ξ.	-:	۳.	٠;	٦.	6	٦,	٠.	+	
SNO	9.	5	'n	6	'n	4.08	9	4	. ~	,																										
COCATION	180.0	9	,	•	, 4	. 7	S	-	. «	2.45	-	0	. "	~	_ m	-	9		-	4	. 4				•	٣.	Ξ.	``.	٦.	~	٠.	~ &	-:	٠.	9	
GREE	4	~		٧	. ~	4.32	0		•	:																										
ē		•	•	ľ	ď		•	, ~	ו מ	200	9	4			· ~	-		•	6				×	4		ف	4	4	0	0		21.33	+	14.63	+	
	111.6	•	. "	? <	•	3.46	. «	•	: <																											
	0.06	۲	٠,	1 0	> 4	•	, (	4 <	* 4		•	1 7	• -		. ~		•		, 4		: -	•		. •	. –					. 4	: -	. 4		10.59	; ; ;	,
	68.4	•	<b>.</b> .		•	4 . 3 e	•	, [	•	?																										
	46.8	•	7 .	9	0 0	0 0	•	- 0	י ת		9	9 4	0	י ר	4 5	r v	, ,			! 4					. "	: -	. 1	` ''	: -		: -		: -			•
	21.6	,	۰ ۹	? 9	,	99.5	•	•	•	₹.																										
	0.0	•	7	٠,	ν.	4. 1	U :	n ·	- 1	7.71	0 4	nı	חים	•	• •	4.6	•	•			יית		7.	, ,	, 4			; •	: -	;		: -	: .	٠,	. 4	٠
1	STATION (IN)	,	۰, ۰				٠.	•	۰.		ب م	ء د م	n e		n .	0.0	7 1		0.7	6.71	. t	٠.٠	5.0	) c		y	1.0		) · ·	) (	20.00	20.0		2.4	3/5.6	

SEGMENT MINIMUM = 2.04 AT THE 145.5 INCH STATION A " + " MEANS NEGLIGIBLE MDD HAS OCCURRED

# TABLE 22 RSRM-7B AFT CYLINDER INSULATION PERFORMANCE

MATERIAL DECOMPOSITION DEPTH (MDD) INCHES

DESIGN M+3S	1.369	.77	.71	. 68	. 61	. 57	. 58	. 55	. 52	. 52	. 51	. 49	. 49	. 45	. 45	. 40	.37	. 35	. 31	.33	. 28	.30	. 25	. 25	. 19	.19	. 18	. 18	.17	.17	. 22	. 23	. 23
MAX.	0.951	. 51	. 58	. 46	. 47	. 48	. 54	. 48	. 43	. 44	. 46	. 45	. 39	. 31	. 42	.31	. 29	.30	. 24	.27	. 23	. 21	. 18	. 23	. 13	. 15	. 08	. 12	90.	90.	.07	.08	90.
MEDIAN	0.758	. 44	. 46	. 38	. 40	. 41	. 44	. 43	. 39	. 42	. 41	. 42	.37	. 28	. 42	. 25	. 26	. 28	. 22	. 22	. 21	. 18	.16	. 21	11.	.10	90.	. 08	.04	. 0 4	.03	. 0 4	0
16.8 338.4	.666 0.807	440 0.33	381 0.18	386 0.17	395 0.19	396 0.30	439 0.27	43	41	43	46	45	39	29	42	31	26	30	22	23	22	20	17	7	11	5	m	0	9	4	~	08	m
291.6 33	0.752 0	.444 0	.412 0	.385 0	.339 0	.355 0	.479 0																						•	0			0
.4 270.0	36 0.798 29 0.490	8 0.47	1 0.45	5 0.39	3 0.39	8 0.41	8 0.42	. 40	. 36	. 41	. 40	. 40	. 38	. 24	. 36	. 13	. 25	. 26	. 22	. 21	. 21	. 20	.17	. 22	. 11	. 10	. 0 4	.07	.04	.06	.03	. 05	0
26.8 248.	.526 0.63	451 0.4	406 0.4	341 0.4	384 0.4	408 0.4	448 0.3	44	43	44	42	41	37	31	37	29	28	27	23	22	m	21	14	71	13	11	0	07	03	04	0	04	. 0
10NS 201.6 2	0.764 0	.327	.397	.372	. 434	. 403	. 436	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	•	0	
EE LOCAT . 4 180.0	91 0.951 29 0.558	23 0.50	14 0.53	54 0.46	03 0.42	33 0.43	60 0.49	. 45	.37	. 25	. 26	. 42	.37	. 26	. 42	. 18	. 29	. 28	. 23	. 23	. 22	. 18	.17	. 21	. 12	.09	90.	. 12	.03	. 05	. 0 4	. 04	90.
DEGR 136.8 158	0.579 0.7 0.346 0.4	.440 0.	.511 0.	.396 0.	.406 0.	.430 0.	.495 0.	. 48	. 40	. 42	. 41	. 41	.37	.31	. 42	. 27	. 25	. 28	. 24	. 21	. 19	. 14	. 15	. 18	. 11	0.09	90.	.07	90.	.02	00.	.03	0
111.6	5 0.892	0.47	0.48	0.44	0.41	0.46	0.47		_		_	_		_	_	_	_	_	_		_	_	_	_		_	_	_	10		1	•	
0.06 4.	16 0.705 98 0.416	8 0.40	5 0.40	2 € 32	8 0.30	8 0.42	9 0.40	36	. 21	.31	. 34	. 44	. 39	.27	. 42	. 21	.27	. 29	. 18	. 24	. 19	. 18	. 15	. 23	. 11	0.09	. 04	60.	. 05	0	4	. 04	0
89	28 0.6 99 0.4	05 0.5	71 0.5	90 0.3	91 0.4	60 0.3	16 0.4	m	7	~	7	0	S	6	0	9	6	9	S	-	$\sim$	7	œ	0	7	0	œ	6		9	~	S	_
1.6 46	736 0.8 527 0.4	516 0.	469 0.	423 0.	448 0.	484 0.	442 0.	•	٠	•	•	٠		•	٠	٠	•	•	٠	•	٠	•	٠	•	•	٠	•	٠	•	٠	٠	•	
0.0	.807 0.	.502 0	.516 0	.439 0	.474 0	.469 0	.547 0	. 44	. 42	. 42	. 42	. 44	.36	. 28	. 42	. 24	. 24	. 24	. 20	. 27	. 19	. 17	. 14	. 21	. 10	. 10	.07	. 05	. 0 4	.03	0	-	•
STATION (IN)	56.0 0	5.0	8.0	1.0	5.0	0.0	8.0	05.8	16.0	24.5	33.0	45.5	58.5	68.3	17.7	92.5	02.5	14.0	27.3	38.3	50.0	67.0	83.9	99.1	22.0	39.0	44.0	58.0	63.0	67.0	72.	ď.	77.

TWR-17546 Vol. III Page 111

STATION							ã	DEGREE	LOCATIONS	ONS								EXPOSURE
(NI)	0.0	21.6	46.8	68.4	0.06	111.6	136.8	158.4	180.0	201.6	226.8	248.4	270.0	291.6	316.8	338.4	AVE.	TIME
			_			12.0	7.8	10.6	12.8	10.3	7.1	<b>89</b>	10.7	10.1	9.0	10.8	10.0	•
	6	•	•				6.1	7.6	6.6	•	80 4.	9.4	8.7	0.6	٠	•	•	56.5
				0			8.7		10.0	•		89	9.3	<b>8</b> 0	8.7	•		
		•		•			11.0		11.4	•	_	•	7.6	ø.	8.2		9.5	46.5
		6				6	∞.		0	•		٠	8.7	8.4	٠	•		45.7
	0	6,		0.6		9.1	0.6	8.9	6	9.6		9.5	eo ••	7.5	<b>8</b> 0	4.3	•	•
						0	7.6		8.6	•		•	9.3	8.0	8.9	•	9.5	•
` _	'n	•		•			11.4	•	11.4	•		٠	9.7		10.1		•	43.5
5.	10.3	,	10.2		80		11.4		10.7		10.3		9.4		10.1		10.1	•
9	0		8						9.0				9.8		9.8		6.8	
4	0		10.3				10.3		6.2		-				10.5		9.5	
	0		0				10.4		9.9		10.8		10.3		11.6		8.6	39.7
5			10.8						4		-		0		12.1		11.3	۲.
8 6	0		•								0		10.7		10.9		10.4	œ.
89	8		.5		-				7.		6		9				8.2	34.7
77.			11.8				12.3		12.3				10.7		~		11.9	<b>.</b>
2	7		8		_		8.9		6.1				4.4		10.1		7.8	31.1
0.7			6						٠.		9.7	٠	8.7		& &		9.1	6
4			9.6				10.3		10.3				9.6		10.8		10.0	7
27.			6.1		_		9.5				9.0				8.6		8.2	'n
80			· •				8.7				9.1		8.7		8.6		9.5	4
50			10.2				9.8		9.9		10.5		9.4		•		9.4	۲.
67.			9				7.4						10.5		•		9.1	6
83			0				6.6				8.7		10.2		10.0		9.6	۲.
99			11.9				10.6						12.6		•		12.2.	7
22.	ω,		8.6				9.3				10.3		<b>∞</b>		٠		9.3	7
39.			8.2				7.5						8.9		٠		<b>∞</b>	5
44			7.1				5.0		5.2		5.8		•		3.0		4.8	7
58.			8.2				8.9								٠		٠	11.4
63.			1.6				5.5		5.6		3.1				9		о. В	
67.			6.1		0		1.9				•				3.7		ж. Ж	11.0
72.			•		5.6		0.1				2.9				4.9		2.2	15.8
375.0	0.4		2.9				1.8		2.2		2.3		5.9		4.3		2.4	19.2
77.			0		0		0				•		•		1.7		9.0	20.4

MOTOR ACTION TIME = 122.9 SECONDS

PREFIRE MEASUREMENTS INCHES

PART NO. 1U76668-03

SERIAL NO. 0000006

POSTFIRE MEASUREMENTS

PART NO. 1U76658-01

SERIAL NO. 0000002

A

TWR-17546 Vol. III Page 114

TABLE 23 RSRM-7B AFT CENTER SEGMENT INSULATION PERFORMANCE

COMPLIANCE SAFETY FACTOR (CSF)

NOTE CE			080	GREE LO	CATIONS	<b>5</b>					REQUIRED
(II)	0.0	46.0	90.0	•	80.0	0.9	270.0	316.0	MIN.	PLANE	
3.5	Ś	€.	<b>40</b>	ς.	∞.	6.	۲.	₹.	'n		2.0
-	7	۲.	٦.	7	6.	0	0	~	ō	•	
7 0 5	2.50	2.14	2.27	2.40	2.44	2.23	2.57	2.55	2.14	Ġ	
· ve	-	4	s.	'n	٦.	₹.	۲.		4	Ġ	
•	9	"	4.	₹.	€0	Ξ.	٠.	9.	٦.	26.	
4	7	9	٦.		'n	۰.	7	*	9.	ė	٠
. 60	٦.	₹.	5	٥.	ď	٥.	9.		•	Ġ	•
, ,	6	•	٣.	. 7	٦.	۳.	₩.	₩.	m.	26.	
26	'n	0	٠.	9.	≈.	۲.	٩.	۲.	۲.	26.	•
י ה	, m		٠	7	٥.	٥.	۳.	۳.	°.	26.	•
	4		4		7		۲,	•	7	80.	•
7	+	-	٠	+	+	+	9.	+	۲.	•	•
. 8		. +	+	+	+	+	+	+	+	•	•
, ,	٠ -	٠ +	+	+	+	+	+	+	+	•	•
,	- 4	- 4	- 4		. +	+	+	+	+	•	•
, .	٠ -	+ +	. 4	٠ ٦	. 4	+	+	+	+	•	•
-, -	+ -	٠ -	<b>⊦</b> ⊣	٠ ٠		- 4	. 4	. +	+	•	•
	-			•	-	F-0 10 10 10 10 10 10 10 10 10 10 10 10 10	# C F # 4 # 0				
SECRENT	MINIMOR N	T TOUR T	GTRIE WOD HAS	HDD HA	4						
•		1									
		⋖	CTUAL	SAPETY	FACTOR	R (ASF	_				
NOTEATO			DE	GREE L	u	SNS					REQUIRED
( IN )	0.0	46.0	0.06	136.	180.0 22	226.0	270.0	316.0	HIN.	PLANE	S. F.
	٧	a	0	rt.	0	0	,	9	'n	9	
n -	9 0	•	•	) «	٠ «	۹	6	7	•		
			, ,		4.0	2 2 6	2 0 1	2 90	2.44		
<b>-</b>	٠,	* .		•	: `	•	<b>`</b> «	•	. 4	90	
•	ņ	י.	ŗ.		•	•	. ·	•	. 4		
σ.	7	•	` '	`. '	•	•	<b>Y</b> (	, (	• •		•
4	٠.	~	'n	7	7.	•	, (	7.	• •		
8	ŝ	٠.	∞.	7	٠,	7	7 (				
7	7	v.	σ.	7	٠.		٠. ا	7	•		
5	∞.	9.9	'n	7	4	7		4 . I U	፣ '		
2	₹.	۳.	9.	ø.	σ.		*** **1		``		•
9	₹.		7	'n	٠.	₩.	~	₹.	•	90	
214.1	+	80	7.	+	+	+	₩.	+	m.	46.0	1.5
8	+	+	+	+	+	+	+	+	+		•
86	+	+	+	+	+	+	+	+	+	•	•
6	+	+	+	+	+	+	+	+	+	٠	•
-	+	+	+	+	+	+	+	+	+	•	٠
. 4	. 4	+	+	+	+	+	+	+	+	•	•
P	٠	•		•							
SEGMENT		11	2.44 AT	r THE	0	INCH S.	STATION				
. + . Y	MEANS	S NEGLI	IGIBLE	MDD HA	S	OCCURRED					

TWR-17546 Vol. III

Page 115

TABLE 23 RSRM-7B AFT CENTER SEGMENT INSULATION PERFORMANCE

(MDD)	
DEPTH	
DECOMPOSITION	INCHES
MATERIAL	

DESIGN M+3S	90.	0.829	. 3	. 20	. 09	.08	.08	.07	. 05	.08	. 02	00.	00.	00.	00	00.	CRITERIA			e.	_																		
HAX.	80 6	0.956	. 24	. 20	.09	. 09	.07	. 05	. 04	.07	.01	0	0	0	•	0	DESIGN			EXPOSITE	A F C 3 C F	E H	7	•	7.	~	~	~	4	٥.	•	•	•	•		٠	2.0	•	•
MEDIAN	7.	0.310	. 22	. 16	.08	.08	.04	.03	.02	90.	0	0	0	0	0	0	3 SIGMA					AVE.	•	٠	٠	•	•	•	٠	•	•	3.7	•		•	•	0	0	0
316.0	609.	0.294	2.1	. 16	.09	.08	90.	.04	. 04	.04	0	0	0	0	•	0	THE M +	(MDR)	•		•	316.0	•	•	٠	٠	•	•		•	٠	5.4	•	0	0	0	0	0	0
0 270.0	0.76	9 0	0.22	0.16	0.08	<0.07	0.04	0.04	0.04	90.0	. 01	0	0	0	0	0	CEEDED	RATE (M			•	2 / 0 . 0	9	6	9	9	7.	7.	9	4	ď.		9	•	0	0	0	0	0
s 26.	36 0.727	7 0.33	0 0.24	9 0.20	5 0.09	2 0.09	3 0.07	1 0.05	8 0.04	3 0.05	0	0	0	0	0	0	HAS EX	SITION	SECOND	NOI		7 0	2 6	8	4 7.	8 7.	7 9.	4 7.	3 8.	2 7.	5 6.	6 5.	3 5.	•	0	0	0	0	0
LOCA 0 180	823 0.73	12 0.3	33 0.1	74 0.1	0.0>96	95<0.0	46 0.0	32 0.0	17 0.0	50 0.0							DING MDD	DE	\	E LOCAT		. 0 180.	.3 6	. 2	9 9.	.1	8.	.0	.4 7	.5	9.	. 2	. 0				•		
DEGREE 90.0 136.	736 0.	31 0.	237 0.	177 0.	087 0.	082 0.	039 0.	037 0.	024 0.	0 690	012						E PRECEI		MILS	DEGRE		90.0		σ.	0	m.	0.	m.	٣.	<b>.</b>	7.	<b>-</b> .	6.	٥.			0		
46.0	0.757 0	.351 0	.242 0	.181 0	.098<0	.083 0	.035 0	.025 0	.013 0	.0630	.016 0	0	0	0	0	0	TES TH	MA			•	0.0	6.7	•	•	٠	٠	•		•		1.7	٠		0	0	0	0	0
0.0	0.819 (	300	.192	.162	.050	.092<	.058	.033	.019	.068		0	•	0	0	0	" INDICA			_	•		7.3	٠	٠	٠	•	•	٠	٠	٠	•	٠	0	•	•	•	0	0
STATION (IN)	3.5		9	6	4	α	71.		53	61.	14.	80.	98.	07.	11.	14.				STATION	( T M )	(N.1.)	3.5				6	4.	•	71.	26.	53.	61.	14.	80	98	•	11.	14.

0.0 SECONDS

MOTOR ACTION TIME =

TABLE 23 RSRM-7B AFT CENTER SEGMENT INSULATION PERFORMANCE

PREFIRE MEASUREMENTS INCHES

PART NO. 1U76667-01 SERIAL NO. 0000006

•	00		0 0	, 0	• •	0	0	0	9	0		0	0	0																								
MOM	2.12	. 75	.60		. 28	.17	.15	. 14	. 23	. 13	.09	.09	.09	.09	. 09																						SES	
MEDIAN	2.898	. 8	. 85	40	. 40	. 19	. 16	. 16	. 63	. 13	60.	60.	. 10	. 10	. 10			•	MEDIAN	15	٠77	. 54	. 61	. 49	. 31	0.321	* 1 -		.57	. 13	.09	.09	.10	. 10	. 10	LOCATION.	THICKNES	
MIN.	2.811	48	. ea.	9 6	. 39	. 18	. 16	. 16	.61	. 13	0.	.09	. 09	0.0	.09			;	N	. 0 5	.68	. 50	. 60	.47	90	90.70	7 7 -	11.	. 55	.11	1	'n	ŋ	u	J	THAT	PREFIRE	
316.0	~ ~	0.85	0.83	0.39	0.39	0.19	0.16	0.16	0.61	0.13	0.09	0.09	0.09	0.09	0.09				316.0	2.20	1.79	0.55	0.61	0.47	0.30	0.317	1.0	0.11	0.56	u	נו	יו	ם	J	'n	NING AT	ING THE	ING
0 270.0	5 2.812	0.85	0.85	0.41	0.41	0.19	0.16	0.16	0.64	0.13	0.09	0.09	0.11	0.11	0.11	ENTS		•	.0 270.0	2.05	1.81	0.55	0.63	0.52	0.32	8 0.334		0.11	0.58	0.11	נו	'n	ŋ	u	ŋ	S REMAININ	ATE	REMAIN
ONS 226.	93 2.88	2 0.86	3 0 .85	3 0.40	8 0.40	7 0.20	9 0.17	7 0.17	8 0.64	9 0.14	9 0.10	01.09	0 0.11	2 0.11	0 0.11	EASUREME	TONS	2 6	.0 226.	7 2.15	8 1.77	5 0.52	3 0.60	3 0.48	8 0.31	26 0.30	77.0	9 0.12	5 0.59	,1	73			'n	ני	ERIAL WA	CALCUL	IAL WAS
LOCA:	44 2.8	64 0.8	50 0.8	04 0 4	06 0.4	94 0.1	69 0.1	64 0.1	27 0.6	35 0.1	00 0.1	0.0 00	00 0.1	00 0.1	05 0.1	TFIRE ME		4777	.0 180	21 2.1	81 1.7	52 0.5	17 0.6	76 0.5	08 0.3	11 0.3	7.00 C.	47 0.1	77 0.5	ч						MAT	WER	IATER
DEGREE 0.0 136.0	03 2	. 0	49 0.	. 0	96 0.	93 0.	.0 69	.0 09	36 0.	35 0.	980.	99 0.	5 0.	.0 60	07 0.	POST	1 44 C	40.00	0.0 136	67 2.	83 1.	00	12 0.	.0 68	080	314 0.3			67 0.	23				נ			VAL	_
6 0.9	903 2.	858 0.	850 0.	413 0.	416 0.	193 0.	167 0.	161 0.	641 0.	133 0.	0 660	100 0.	0990.	097 0.	097 0.	2-02	,	,	6 0.9	46 2.	87 1.	07 0.	080	. 0 60	15 0.	.333		48	78 0.	17 0.						TES THAT	N	()
0.0	960 2	.851	.870	380 0	.417 0	.187 0	.161 0	.161 0	.640 0	.130 0	.097 0	.094 0	.108 0	.095 0	.091 0	107665			0.0	.141 2	.769 1	.551 0	.678 0	.522 0	.330 0	0 625.	1 28 0	142 0	.572 0	0						INDICATE	AN AND MI	OCATION
STATION (IN)	m -	٠,	7.5	4	8.0	1.5	26.0	53.5	1.4	14.1	80.0	98.0	07.8	11.8	14.0	PART NO.	NOT TAT	NOT 1410	( N I )	٥.	1.0	0.7	6.2	7.6	9.6	48.0	0.17		61.4	14.	80.	98.	07.	11.	14.	AN " L	HEA	AT THE L

TABLE 24 RSRM-7B FORWARD CENTER SEGMENT INSULATION PERFORMANCE

COMPLIANCE SAFETY FACTOR (CSF)

REQUIRED S.F.	ខណៈស្រស់ស្សសស្សសស្ស ស្រស់ស្រស់ស្រស់ស្រស់ ស្រស់ស្រស់	R B B B B B B B B B B B B B B B B B B B
PLAHE	1 4 6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 1 8 1 1 1 8 1 1 1 8 1 1 1 8 1 1 1 1 8 1
MIM.		M
316.0	125 125 136 146 147 177 177 177 177 177 177 177	316. 20.24. 20.24. 1224. 14.16. 16.95. 19.09. 19.09. 19.09.
270.0	2 15.25 2 14.71 1 3.8.87 1 7.54 0 27.69 7 12.52 7 12.52 7 12.52 7 14.54 6 4.54 6 4.54 7 14.54 7 15.67 8 17.10N	270.0 18.19 15.37 11.68 10.96 28.46 16.00 6.40 6.58 12.46 + + + + + + + + + + + + + + + + + + +
ONS 226.0		ATIONS 0.0 226.0 270.0 146 16.47 18.19 171 64.70 14.7 11 15.18 11.68 173 8.54 10.96 173 45.62 28.46 10 28.31 16.00 11 16.00 6.40 11 16.00 6.40 11 14.4 11 16.00 6.40 11 16
LOCATION 180.0 2		L 10 0 10 10 10 10 10 10 10 10 10 10 10 1
EGREE 136.0	19.45 11 10.4.81 11 10.4.81 11 10.7.18 16.36 11 10.7.18 12.50 10.7.37 14 + + + + + + + + + + + + + + + + + +	EGREE 136.0 31.11 31.11 10.33 117.23 117.23 113.42 113.43 114.13
90.06	84.8 11.96 11.96 14.96 21.11 21.11 22.8.8 7.0 7.0 10.0 3.32 4 + + + + + + + + + + + + + + + + + + +	11.14 12.1.16 13.1.16 13.1.16 14.17 14.17 15.18 17.18
46.0	14.55 89.55 80.55 32.73 10.29 80.29 60.67 60.67 7 + + + + + + + + + + + + + + + + + +	46.0 11.94 11.94 11.94 11.94 13.39 13.39 10.21 7.32 7.32 7.57 17.74 17.7
0.0	19.39 14.758 89.37 69.37 69.37 69.37 69.37 69.37 69.37 69.37 89.39 99.37 89.39 99.39	0.0 4.24.95 17 23.07 11 7.86 8 12.16 9 9.25 7 18 8.30 33 9.89 13 6.86 10 4.15 7 4 4.15 7 4 6.33 9 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
STATION (IN)	3.5 11.0 30.7 36.7 39.7 44.6 71.5 71.5 71.5 71.5 71.5 71.5 71.5 71.5	STATION (IN) (IN) (IN) (IN) (IN) (IN) (IN) (IN

TWR-17546 Vol. III

TABLE 24 RSRM-7B FORWARD CENTER SEGMENT INSULATION PERFORMANCE

	DESIGN W+3S		. 48	. 20	.08	.08	.05	80.	70.	00	00.	00.	00.	Gi																			
	HAX.		. 15	.03	.03	.04	.02	.07			•	0	0	1 0 0 0 X 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	3000	H	5	€0	•	٠.	~	٠.	12.1	; ,	•	•				•	. W	•	SECONDS
	MEDIAN	0.124 0.105	.08	.06	. 0 2	.02	0	0.034	<b>-</b>		• •	0	0			>	٠	•	٠	٠	•	٠	2.1	•	•				• •	0	0	0	122.9
(MDD)	316.0	0.084	.08	.04	.02	.00	0	0.035	<b>-</b>		•	0	0	(MDR)		•		٠	٠	•	٠	٠	«	•	٠	۰ ۳	•		. 0	•	0	0	TIME
DEPTH (	270.0	0.13	0.0	0.05	0.05	0.03	0		<b>-</b> c		•	0		RATE (M		270.		0	<del>.</del>	7	~		<b>⊣</b> (	, ,	•					•	0	•	ACTION
NOILIS	TONS ) 226.0		0.08	0.07	0.01	0.0	0	7 0.023		0	0	0	0	NOITI	)	226.	٠		_;	<del>.</del>	m	•	1.1	÷	<b>-</b>	,		0	0	0	0	0	MOTOR
DECOMPOSITION INCHES	LOCATION 180.0	9 0.15	6 0.08 4 0.07	2 0.04	7 0.03	6 0.01 2 0	0	7 0.06	- 0	0	0	0	0	64		180.	<del>.</del>		2 1.	2 .	2 2.	7		;	<b>4</b> (			0	•	0	0	0	
MATERIAL D	DEGREE.	25 0.10 39 0.07	3 0.1 1 0.0	9 0.0 7	0.0	4 6 0.0	4 0.	0.	•	0	0	0	0	ERIAL D MILS / DEGREE	•	13	7	9	w .	88	w .		». «	* -	<b>.</b>	• ^		0	•	•		0	
MAT	06 0.9	46 0.0 99 0.1	93 0.0 86 0.0	82 0.0 11 0.0	28 0.0	19 0.0 22 0.0	21 0.0	₩.	# -1					HAH		о. О	.3	0.	6.	9.	9.	5.	. r	•	7 -	•	6				•		
	0.0 46	010	099 0. 064 0.	067 0. 020 0.	037 0.	028 0. 039 0.	0	71 0.	>							0.	σ,	• ·	- <del>-</del>	σ,	ن تح	٠ .	-: "		<del>:</del>	9	4				0		
	STATION (IN)	3.5	. 2.	9.7	8.0	71.5 026.0	3.5	61.4	1.4.1	86	07.	11.	14.	STATION		Z	۳. ن		9	9	<u>ب</u>	4 (		1 0	9 6	1 5	4	8	8	0.7		14	

TABLE 24 RSRM-7B FORWARD CENTER SEGMENT INSULATION PERFORMANCE

PREFIRE MEASUREMENTS INCHES

PART NO. 1U76667-01 SERIAL NO. 0000008

HOT	10.000 10.000 10.000 10.000 10.000 10.000 10.000 10.000	თ
MEDIAN	2.496 2.382 0.790 0.800 0.600 0.372 0.192 0.160 0.157 0.157 0.109 0.109	I. MEDIAN  10 2.382  15 2.296  19 0.707  14 0.737  13 0.357  13 0.140  13 0.140  13 0.140  14 0.140  10 0.109  10 0.109  10 0.109  10 0.109  10 0.109
MIN.	2.438 0.778 0.778 0.611 0.191 0.153 0.153 0.107 0.109 0.106	MIN. 2.290 2.1590 2.1550 6.0149 6.7149 6.333 6.333 6.153 6.153 7HAT LOC
316.0	2.477 2.267 0.785 0.799 0.623 0.371 0.191 0.160 0.160 0.160 0.107 0.109	316.0 2.393 2.155 0.579 0.331 0.186 0.186 0.139 0.633 1.1NG AT
270.0	2.528 0.784 0.784 0.794 0.370 0.368 0.192 0.158 0.157 0.112 0.112 0.109	NTS 270.0 270.0 2.389 2.464 0.726 0.726 0.345 0.134 0.134 0.134 0.134 1.00 0.596 0.134 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.0
IONS 0 226.0	2.438 2.3948 2.3948 2.0.7894 2.0.7898 2.0.368 2.0.192 2.0.193 2.0.110 2.110 2.110	SS 26.0 26.0 26.0 26.0 26.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25
LOCATI 0 180.0	5 2.519 8 2.3819 9 0.7389 10 0.811 10 0.374 10 0.374 2 0.192 2 0.105 2 0.109 0 0.109 0 0.109 0 0.109	HES ME LOCAT 1 80 - 1 2 2 3 6 2 2 2 3 6 0 3 4 6 0 0 1 7 7 8 0 0 1 7 8 0 0 1 8 1 1 8 1 8 1 8 1 8 1 1 8 1 8 1 8 1 8 1 1 1 8 1 8 1 8 1 8 1 1 1 8 1 8 1 8 1 8 1 1 1 8 1 8 1 8 1 8 1 8 1 8 1 8 1 8 1 8
DEGREE 0 136.	2 2 3 3 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	POSTFI INC INC INC INC INC INC INC INC INC IN
. 06 0	9 2 . 5 0 0 . 7 9 8 0 . 6 3 0 . 7 9 8 0 . 7 9 8 0 . 7 9 8 0 . 7 9 9 0 . 1 9 9 0 . 1 1 0 0 . 1 1 1 0 0 . 1	3 3 2 9 0 0 9 0 0 9 0 0 9 0 0 0 9 0 0 0 0 0
0 46.	2 3 4 8 8 9 9 8 8 9 9 8 9 9 9 9 9 9 9 9 9 9	76651- 000000 0000000 000000000000000000000
юм 0.	2.52 2.75 0.77 0.36 0.36 0.19 0.11 0.11 0.11 0.10	NO. 1U NO. 1U NO. 0 2.41 2.167 0.34 0.34 0.34 0.15 0.15 0.15 0.15 0.15 0.15 0.15 0.15 0.15 0.15 0.15 0.15 0.17 0.17 0.18
STATION (IN)	3.5 30.7 30.7 30.7 30.7 44.6 48.0 711.5 711.5 161.4 280.0 2980.0 307.8 311.8	STATIO (IN) (IN) (IN) 30.7 30.7 36.2 39.7 44.6 44.6 44.6 11.5 11.5 126.0 153.5 161.4 161.4 214.1 280.0 307.8 311.8 311.8

TABLE 25 RSRM-7B FORWARD SEGMENT STAR TIP. INSULATION PERFORMANCE

		PLANE	286.0	54.			Ġ				ö	90.	86.	9	52.	86.	52.	52.	90.	86.	52.		54.	86.	54.	86.	86.	54.	90.		90.	54.	86.	ά.	52.	ö	ά.	54.	STATION
_		MIM.	•	4.48	+	+	+	+	+	+	+		15.29	0	₹.	•	3	۳.	9.	۲.	m.	2.53	m.	ď.	m.	٠.	₹.	'n	۳.	ď.	s.	9.	∞.	4	۰.	ŝ	ĸ.	7	IMCH ST
R (ASF)		352.0	+	8.45	+	+	+	+	+	+	+	+	+	۲.	4.	7.	'n	۳.	٥.	7	۳.	2.89		٥.	٥.	7	٥.	۲.	€.	σ.	ŝ	٥.	7	₹.	٠.	7	۲.	۳.	394.0
Y FACTOR	CAT	286.0	26.54	۳.	+	+	+	+	+	+	+	+	15.29	•	12.2	ж 8	4.2	2.8	2.7	2.7	2.9	2.53	2.7	2.5	2.4	2.5	2.4	7.6	2.8	3.3	6.8	5.6	2.8	2.8	3.3	3.0	2.4	5.2	AT THE
L SÄFETY	GREE LO	0 222.0	+	8 5.44	+	+	+	+	+	+	+	+	+	2 16.1	2 10.8	1 5.1	3 . 4.0	5 3.0	5 3.0	8 3.4	9 3.1	6 2.89	4 3.0	9 2.8	9.76	4 2.8	0 3.1	6 2.8	6 3.1	8 3.7	9 6.5	6 3.1	6 3.5	3 3.9	9 5.2	5 2.8	1 2.3	2 5.5	<b>2.31</b>
ACTUAL	DE	.0 154.	40.1	29 4.4	+	+	+	+	+	+	+	+	+	98 7.	73 6.	59 4.	90 3.	04 2.	63 3.	21 3.	66 3.	72 2	47 2.	65 2.	82 2.	88 3.	78 2.	15 2.	33 2.	98 3.	55 4.	86 2.	96 3.	14 2.	04 3.	54 3.	33 2.	59 5.	HINIHOM
	TATION	90	+ 5.1	3.0 7.	:	:	_:	:	_:	_:	4.7 +	∴		1.5 7.	2.0 8.	2.0 5.	5.5 3.	7.0 3.	9.0 2.	5.0 3.	1.0 2.	0.0 2.	5.0 2.	0.0 2.	4.0 2.	3.0 2.	2.0 2.	3.0 3.	5.0 2.	2.0 3.	1.0 4.	9.0 3.	0.0	2.0 4.	1.0 3.	3.0 2.	4.0 2.	3.0 5.	EGMENT M
	ST	C	•••	=	5	ĕ	Ř	m	7	Ť	ŏ	•	•	14	S	9	~	•	O	-	~	23(	m	4	S	9	40	O	0	-	~	~	S	9	7	•	Q)	40	v
	REQUIRED	. M.						•			1.5				•		•		•	•	•	•	•	•		•	•	•	•	•	•	•	•	•	•	•	•	•	
		PLANE		54.			ď				0.06	Ö	86.	86.	52.	86.	52.	52.	86.	86.	52.	9	54.	86.	86.	86.	86.	54.	90.	9	90.	54.	86.	۲,	52.	。	۲,	54.	TION
F)		MIN.	22.55	°.	+	+	+	+	+	+	+	+	13.76	4	~	4	6	7	۳.	9	۲.	2.42	7	۳.	۳.	₹.	7	۳.	6.	۲.	٥.	٣.	∞.	σ.	٦.	٦.		9.	I STA
ACTOR (CSF		352.0	+	6.44	+	+	+	+	+	+	+	+	+	٥.	7	89	6	7	9	6.	٦.		٠.	9.	9.	٦.	٦.	.5	s.	٦.	6.	٥.	٥.	6.	٦.	۲.	۳.	٠,	394.0 INCE
ETY F	5	286.0	22.55	3.7	+	+	+	+	+	+	+	+	13.76	3.4	10.2	2.4	3.4	2.6	2.3	2.6	2.6	7	2.4	2.3	2.1	2.4	2.2	2.4	2.4	2.7	6.4	2.3	2.8	2.5	3.0	2.7	1.8	4.6	T THE MDD H
CE SAF	GREE LO	222.0	+	4 3.55	+	+	+	+	+	+	+	+	+	13.8	9.0	3.4	3.4	2.9	2.8	3.2	2.8	4 2.83	2.8	2.6	2.4	2.6	2.9	2.5	2.8	3.0	5.9	2.9	3.4	ж 8.	5.0	2.4	-	4.8	= 1.76 A GLIGIBLE
COMPLIAN	DEC	0 154.	9	4 3.0	+	+	+	+	+	+	+	+	+	7 6.5	0 5.5	5 3.4	8 3.0	3 2.7	6 2.7	9 3.2	8 2.7	3 2.6	4 2.1	2 2.6	1 2.2	0 2.8	6 2.6	0 2.3	4 2.0	8 2.7	9.4.9	0 2.3	8 3.0	0 2.5	9 2.7	6 3.0	5 1.8	4.6	I MUM NS NE
υ	NC	90.	+	5.2	+	+	+	+	+	+	+	+	+		7.	M	<u>س</u>	2	7	m	2.	2.6	7	2.	2.	7	7	7	-	m.	4	m	5.	4	۶.	2.	-	4	F :
	STATION	(IN)			7.		•	7.	Ξ.	4	4	42.	45.		52.	62.	75.	87.	66	2	24.	230.0	36.	40.	54.	63.	82.	93.	05.	12.	21.	39.	50.	62.	71.	83.	94.	03.	₩ ±

A

	EXPOSURE	,		٠	4. 80.	<b>4</b> .	4.2	3.6	•	3.0	٠		ن	5	•	ς.	٠.	01.		01.	101.8	01.	01.	01.	01.	01.		5	5	01.	03		00	6	₹.	0.96	97.	7
) B)	AVE.	•		8 . 2	•	0	0	0	0	0	0	0	0.3	2.1	•	3.1	2.2		•		•	•			٠	2.1	٠	2.0	•	٠	•	٠	1.5	٠	•	7.0	٠	7.6
RATE (MDR)	352.0	•	n ·	5.2	•	0	0	0	0	0		0	•	•	1.9		2.3		•	•			•	٠	٠	.8	•	•	•	•	•	•	1.7	٠	٠	1.7	1.6	1.6
	LOCATIONS .0 286.0	•	7 . 7	٠	0	0	0	0	0	0	0	0	•	٠	1.0	٠	2.0		٠.	•	•		•	•	•	2.3	•	•		٠	•	٠	•	•	•		2.7	1.7
APO /	~ ~		٠ •	4.	0	0	0	0	0	0	0	•	0	•	•	2.7	•	٠	2.3	•	٠	٠	•	•	•	2.1	٠	٠	٠	1.7	•	9.	1.5	•	•	•	5.9	•
	DEGREE 54.0 22		7 · 8	٠	0	0	•	•	0	0	0	0	0	1.9	٠.	2.8				٠	٠	•	•	•	•	7.0	•	٠	٠	1.9		•		٠	•		2.7	1.7
MATERIAL	90.0		6.9	6.4	0	•	0	0	0	0	•	0	0	1.9	1.4	5.6	2.2	٠	2.7	•	5.6	•		٠		2.1	•	•	٠	•	•	1.5	6.0	٠		•	5.6	1.6
	STATION (IN)			'n.	7.		4		4	4	94.7	7	145.7	48.	152.0	62.	7	87.	99.	15.	24.	230.0	36.	40.	54.	263.0	82.	93.	05.	12.	21.	39.	50.	62.	71.	83.	•	403.0
	DESIGN M+3S		0.103	10	0.044	.03	.03	0	.02	. 01	00.	0	.08	.13	. 12	. 22	.32	.39	0.427	. 42	. 42	.37	. 32	. 34	.31	m	. 34	. 33	0.309	30	m	0.319	. 30	. 28	0.304	7	. 28	. 28
	MAX		ō	0.214	0	0	0	•	•	0	0	•	0.017	0.079	0	22	0	29	_	24	0	9	26	24	7	0.236	S	3	7	6	0.226	S.	18	7	24	m	0.286	0
(MDD)			0	٦.		0	0	• •	•	0	0	•	0	4	. 0 4	16	. 19	. 23	. 24	. 20	. 24	. 24	. 23	. 22	. 23	0.210	. 21	. 21	. 21	.17	.15	. 18	. 17	. 20	. 18	.18	. 26	. 19
SITION DEPTH	TIONS		94 0.01	٦.	0	_	_			0			017 0.00	079 0.05	031 0.06	226 0.19	176 0.20	.242 0.29	274 0.24	.242 0.21	.245 0.30	.264 0.22	.237 0.19	.244 0.15	.270 0.21	.236 0	.256 0.20	.222 0.15	.211 0.20	.195 0.13	.143 0.11	.234 0.18	.186 0.17	.201 0.27	.170 0.24	.185 0.16	.266 0.15	.206 0.19
L DECOMPOSITION INCHES	GREE LOCATION 286	7	0.012 0	4<0.183<0	•	•	• •		0	• •	0	•		0.020	7 0.035	0 0.157	1 0.177	7 0.220	4 0.230	5 0.195	9 0.226	2 0.226	8 0.206	8 0.221	6 0.237	2 0.215 0	4 0.194	1 0.211	1 0.184	4 0.177	8 0.155	5 0.189	0 0.151	8 0.137	8 0.104	6 0.207	8 0.286	6 0.196
MATERIAL	15 DE	· • • • • • • • • • • • • • • • • • • •	012 0.06	124<0.21	0									42 0.04	044 0.05	150 0.16	196 0.20	226 0.23	273 0.23	207 0.19	269 0.22	243 0.24	258 0.26	237 0.21	226 0.25	.210 0.20	222 0.21	188 0.23	271 0.26	165 0.19	226 0.19	153 0.23	089 0.17	130 0.20	193 0.18	237 0.16	258 0.26	191 0.20
	STATION		Ś	3.0	7.0		. 4				. 4	42	, in	48.5	52.0 0	62.0	75.5 0	87.0 0	0 0 66	15.0 0	24.0 0	30.0	36.0 0	40.0	54.0 0	0	82.0 0	93.0 0	05.0	12.0 0	21.0 0	39.0	50.00	62.0 0	71.0 0	83.0 0	94.0 0	03.0 0

" INDICATES THE PRECEDING MOD HAS EXCEEDED THE M + 3 SIGMA DESIGN CRITERIA

MOTOR ACTION TIME = 122.9 SECONDS

Vol. III TWR-17546

TABLE 25 RSRM-7B FORWARD SEGMENT STAR TIP INSULATION PERFORMANCE

		RSRM-7B	FORWARD S	EGMENT STAR TIP	INSULATI	ION PERFORMAN	IANCE			
	PREFIRE MEASUREMENTS INCHES	PART NO SERIAL	O. 1U7666 NO. 0000	6-01 005		90 d	STFIRE MEAS	SUREMENTS	PART NO. SERIAL NO	1U76650-04
STATION (IN)	DEGREE LOCATIONS 90.0 154.0 222.0 286.0 352.0	MIN.	MEDIAN	MDT	STATION (IN)	D 90.0 154	EGREE LOCA	TIONS 86.0 352.0	HIM.	MEDIAN
3.5	.554 2.532 2.444 2.495 2.45	. 44	. 49	. 12	•	.542 2.4	9 2.432	.401 2.43	2.40	4.3
3.0	.904 0.958 0.995 0.923 0.85	. 85	.92	. 65	w.	0.780 0.74	14 0.812 0	1.751 0.752	0.7	. 75
7.0	.594 0.622 0.585 0.626 0.62	. 58	. 62	. 45	7.			ני	ы	.62
0.7	.461 0.445 0.428 0.455 0.44	. 42	. 44	. 40	٥.	I.	ı	I.	L	. 44
4.2	.482 0.487 0.474 0.491 0.49	.47	. 48	. 38	4		.7		ų	. 48
7.7	.400 0.392 0.375 0.398 0.36	. 36	. 39	. 33	۲.		.,		ы	.39
1.2	.293 0.294 0.292 0.283 0.29	. 28	. 29	. 28	Ξ.		ü		u	. 29
4.0	.286 0.295 0.289 0.281 0.29	. 28	. 28	. 25	4.		ы		H	. 28
94.7	.110 0.109 0.111 0.107 0.10	. 10	. 10	.09	4.		u		J	. 10
42.0	.156 0.156 0.164 0.157 0.15	. 15	. 15	. 11	42.		u		u	.15
45.7	.336 0.258 0.266 0.260 0.26	. 25	. 26	. 23	45.			.243 0.25	0.24	. 25
. 5	.335 0.316 0.323 0.323 0.31	.31	. 32	. 27	48.	.293 0.2	4 0.303	.244 0.26	0.24	.27
52.0	.384 0.383 0.381 0.380 0.39	. 38	. 38	. 31	52.	.340 0.	6 0.346	.349 0.33	0.32	. 34
62.0	.839 0.797 0.8~7 0.858 0.83	. 79	. 83	. 54	62.	9.0 689.	7 0.650	.632 0.64	0.63	. 64
75.5	.765 0.729 0.712 0.748 0.73	. 71	. 73	. 60	75.	.569 0.5	8 0.535	.572 0.52	0.52	. 53
87.0	.686 0.676 0.671 0.680 0.67	. 67	. 67	. 64	87.	.460 0.4	9 0.451	.438 0.38	0.38	. 43
0.66	.717 0.713 0.704 0.744 0.71	. 70	. 71	. 64	99.	.444 0.4	9 0.474	.470 0.46	0.44	.47
15.0	.665 0.660 0.678 0.672 0.67	99.	. 67	. 63	15.	.458 0.4	5 0.483	.430 0.45	0.43	. 45
24.0	.715 0.707 0.721 0.710 0.71	. 70	. 71	. 63	24.	.446 0.4	8 0.495	.465 0.41	0.41	.46
30.0	.662 0.669 0.653 0.669 0.65	. 65	99.	. 63	30.	.419 0.4	7 0.427	.405 0.42	0.40	. 42
36.0	.638 0.626 0.627 0.650 0.62	. 62	. 62	. 57	36.	.380 0.3	8 0.421	.413 0.43	0.35	. 41
40.0	.627 0.631 0.633 0.626 0.63	. 62	. 63	. 57	40.	.390 0.4	0.412	.382 0.47	0.38	. 41
54.0	.637 0.613 0.637 0.673 0.63	. 61	. 63	. 56	54.	.411 0.3	7 0.400	.403 0.42	0.35	. 40
0.50	.605 0.614 0.603 0.599 0.58		9.	. 56	63.	.395 0.4	2 0.388	.363 0.40	0.36	. 39
0.78	.61/ 0.599 0.609 0.622 0.61	. 59	.61	. 56	82.	.395 0.3	5 0.415	.366 0.40	0.36	.39
	.592 0.591 0.600 0.586 0.57	. 57	. 59	. 5.	93.	.404 0.	0 0.389	.364 0.41	0.36	. 38
0.60	.631 0.616 0.572 0.603 0.57	. 57	9.	. 52	05.	.360 0.3	5 0.388	.392 0.36	0.35	.36
12.0	.657 0.656 0.665 0.648 0.65	. 64	. 65	. 54	12.	.492 0.4	2 0.488	.453 0.52	0.45	. 48
21.0	.029 0.988 1.012 0.977 0.98	. 97	.98	. 91	21.	.803 0.7	0 0.857	.834 0.87	0.79	.83
39.0	.591 0.625 0.590 0.630 0.58	. 58	. 59	. 55	39.	.438 0.3	0 0.401	.396 0.39	0.39	.39
20.0	.530 0.538 0.540 0.536 0.54	. 53	. 53	. 52	50.	.441 0.3	8 0.389	.350 0.37	0.35	.37
0.79	.538 0.547 0.536 0.566 0.67	. 53	. 54	. 52	62.	.408 0.3	9 0.399	.365 0.40	0.33	.39
71.0	.586 0.580 0.547 0.570 0.65	4	. 58	. 52	71.	.393 0.	2 0.443	.400 0.40	0.39	.40
383.0	0.601 0.540 0.595 0.564 0.529	0.529	0.564	0.511	383.0	4 0.3	4 0.38	.379 0.3	0.364	0.374
94.0	.601 0.619 0.660 0.638 0.57	. 57	. 61	. 50	94.	.343 0.	1 0.374	.372 0.41	0.34	.37
03.0	.068 1.075 1.079 1.085 1.04	. 0 4	. 07	. 95	03.	877 0.8	9 0.883	.879 0.84	0.84	.87

AN " L " INDICATES THAT LINER MATERIAL WAS REMAINING AT THAT LOCATION. THE MEDIAN AND MINIMUM VALUES WERE CALCULATED USING THE PREFIRE THICKNESSES AT THE LOCATIONS WHERE LINER MATERIAL WAS REMAINING

TABLE 26 RSRM-7B FORWARD SEGMENT NON-STAR TIP INSULATION PERFORMANCE

DEGREE LOCATIONS.  10. 16. 1.0 10.0 10.0 10.0 10.0 10.0 10.	DEGREE LOCATIONS  1.00 31.64 11.92 21.66 18.33 270.0 2.0 3.5 36.40 62.80 37.12 21.91 25.67 21.91 270.419 5.56 7.56 2.60 2.60 336.0 11.5 31.0 4.10 26.0 270.0 336.0 11.5 31.0 4.10 2.0 4.10 20.0 37.12 21.91 25.67 21.91 270.419 5.56 7.56 2.60 2.60 336.0 11.5 31.0 4.10 4.10 20.0 37.12 21.91 25.67 21.91 370.419 5.56 7.56 2.60 2.60 336.0 11.5 31.0 4.76 5.91 7.51 10.30 3.99 3.99 3.96 3.05 4.10 4.10 4.10 4.10 4.10 4.10 4.10 4.10	0.0 1.6 d 18.93 21.06 18.93 270 0 2 0 3.5 d 18.0	BEE LOCATIONS  21.64 18.93 21.86 18.93 270.0 2.0 5.56 7.56 2.60 2.60 336.0 1.5 + + + + + + 74.0 1.5 + + + + + + 74.0 1.5 + + + + + + 74.0 1.5 + + + + + + 74.0 1.5 + + + + + + 74.0 1.5 + + + + + + 74.0 1.5 + + + + + + 74.0 1.5 + + + + + + 74.0 1.5 + + + + + + 74.0 1.5 + + + + + + 74.0 1.5 + + + + + + 74.0 1.5 + + + + + 174.0 1.5 + + + + + 174.0 1.5 + + + + + 174.0 1.5 + + + + + 174.0 1.5 + + + + + 174.0 1.5 + + + + + 174.0 1.5 + + + + + 174.0 1.5 + + + + + 174.0 1.5 + + + + + 174.0 1.5 + + + + + 174.0 1.5 + + + + + 174.0 1.5 + + + + + 174.0 1.5 + + + + + 174.0 1.5 + + + + + 174.0 1.5 + + + + + 174.0 1.5 + + + + + 174.0 1.5 + + + + + 174.0 1.5 + + + + + 174.0 1.5 + + + + 174.0 1.5 + + + 174.0 1.5 + + 18.9 4.92 4.01 4.01 336.0 1.5 + + 174.0 3.19 2.68 2.06.0 1.5 + + 174.0 3.19 2.68 2.06.0 1.5 + + 174.0 3.19 2.68 2.06.0 1.5 + + 174.0 3.19 2.68 2.06.0 1.5 + + 174.0 3.19 2.68 2.06.0 1.5 + + 174.0 3.19 2.06.0 1.5 + + 174.0 3.19 2.06.0 1.5 + + 174.0 3.19 2.06.0 1.5 + + 174.0 3.19 2.06.0 1.5 + + 174.0 3.19 2.06.0 1.5 + + 174.0 3.19 2.06.0 1.5 + + 174.0 3.19 2.06.0 1.5 + + 174.0 3.19 2.06.0 1.5 + + 174.0 3.19 2.06.0 1.5 + + 174.0 3.19 2.06.0 1.5 + + 174.0 3.19 2.06.0 1.5 + + 174.0 3.19 2.06.0 1.5 + + 174.0 3.19 2.06.0 1.5 + + 174.0 3.19 2.06.0 1.5 + + 174.0 3.19 2.06.0 1.5 + + 174.0 3.19 2.06.0 1.5 + + 174.0 3.19 2.06.0 1.5 + + 174.0 3.19 2.06.0 1.5 + + 174.0 3.19 3.19 2.06.0 1.5 + + 174.0 3.19 3.19 2.06.0 1.5 + + 174.0 3.19 3.19 2.06.0 1.5 + + 174.0 3.19 3.19 2.06.0 1.5 + + 174.0 3.19 3.19 3.19 3.19 3.19 3.19 3.19 3.19	######################################	1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	7	2	22 22 23 24 25 25 25 25 25 25 25 25 25 25 25 25 25
19 5.56 7.76 2.60 2.60 37.12 21.91 25.67 21.91 27.0 19 5.56 7.75 2.60 37.12 21.91 25.67 21.91 27.0 19 5.56 7.75 2.60 37.12 21.91 25.67 21.91 27.0 19 5.56 7.75 2.60 37.12 21.91 25.67 21.91 27.0 19 5.56 7.75 2.60 1.5 10.30 1.99 1.99 1.99 1.99 1.99 1.99 1.99 1.9	1.0   1.0	10   11.64   18.93   21.86   18.93   270.0   2.0   2.0   2.0   2.0   2.1   2.0   2	31.64 18.93 21.86 18.93 270.0  5.56 7.56 2.60 336.0  1		5.0 8.2 8.0 3.7	121 101 10.91	20 00 00 00 00 00 00 00 00 00 00 00 00 0	00000000000000000000000000000000000000
1.9         5.56         7.56         2.60         336.0         1.5         37.0         4.76         5.91         7.51         10.30         3.99 <td< th=""><th>1.5         5.6         7.6         2.6         3.6         1.5         1.5         1.0         4.76         5.91         7.51         10.3         3.99<th>  1.5   5   5   7   5   2   6   2   6   3   5   0   1   5   3   3   3   3   3   3   3   3   3</th><th>5.56 7.56 2.60 336.0 1.  + + + + + + + + 74.0 1.  + + + + + + + 74.0 1.  + + + + + + + 74.0 1.  + + + + + + + 74.0 1.  + + + + + + + 74.0 1. </th><th></th><th>5</th><th># # # # # # # # # # # # # # # # # # #</th><th>0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0</th><th>8 6 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7</th></th></td<>	1.5         5.6         7.6         2.6         3.6         1.5         1.5         1.0         4.76         5.91         7.51         10.3         3.99 <th>  1.5   5   5   7   5   2   6   2   6   3   5   0   1   5   3   3   3   3   3   3   3   3   3</th> <th>5.56 7.56 2.60 336.0 1.  + + + + + + + + 74.0 1.  + + + + + + + 74.0 1.  + + + + + + + 74.0 1.  + + + + + + + 74.0 1.  + + + + + + + 74.0 1. </th> <th></th> <th>5</th> <th># # # # # # # # # # # # # # # # # # #</th> <th>0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0</th> <th>8 6 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7</th>	1.5   5   5   7   5   2   6   2   6   3   5   0   1   5   3   3   3   3   3   3   3   3   3	5.56 7.56 2.60 336.0 1.  + + + + + + + + 74.0 1.  + + + + + + + 74.0 1.  + + + + + + + 74.0 1.  + + + + + + + 74.0 1.  + + + + + + + 74.0 1.		5	# # # # # # # # # # # # # # # # # # #	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	8 6 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7
+         +	4         4         4         74.0         1.5         30.7         4         4         4         74.0         1.5         30.7         4         4         4         74.0         1.5         30.7         4         4         4         74.0         1.5         30.7         4         4         4         74.0         1.5         30.7         4         4         4         4         74.0         1.5         41.2         4         4         4         4         74.0         1.5         41.2         4	1.	+ + + + + + + + + + + + + + + + + + +		6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	**************************************	+ + + + + + + + + + + + + + + + + + +	
+         +	4         4	+ + + + + + + + + + + + + + + + + + +	+ + + + + + + + + + + + + + + + + + +		4 + + + + + + + + + + + + + + + + + + +	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	+ + + + + + + + + + + + + + + + + + +	
+         +	+         +	+ + + + + + + + + + + + + + + + + + +	+ + + + + + + + + + + + + + + + + + +		## ## ## ## ## ## ## ## ## ## ## ## ##		+ + + + + + + + + + + + + + + + + + +	
+         +         +         74.0         1.5         31.7         +	+         +	+ + + + + + + + + + + + + + + + + + +	+ + + + + + + + + + + + + + + + + + +		## # # # # # # # # # # # # # # # # # #	# 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	++++++++++++++++++++++++++++++++++++++	6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6
41.2         41.2         41.2         +	4.1.         4.1. <td< td=""><td>+ + + + + + + + + + + + + + + + + + +</td><td>+ + + + + + + + + + + + + + + + + + +</td><td></td><td># # # # # # # # # # # # # # # # # # #</td><td># 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4</td><td>+ + + + + + + + + + + + + + + + + + +</td><td>44444 4444 4444 4444 4444 4444 4444 4444</td></td<>	+ + + + + + + + + + + + + + + + + + +	+ + + + + + + + + + + + + + + + + + +		# # # # # # # # # # # # # # # # # # #	# 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	+ + + + + + + + + + + + + + + + + + +	44444 4444 4444 4444 4444 4444 4444 4444
44.0         44.0 <td< td=""><td>44.0         <td< td=""><td>+ + + + + + + + + + + + + + + + + + +</td><td>+ + + + + + + + + + + + + + + + + + +</td><td></td><td># # # # # # # # # # # # # # # # # # #</td><td># # # # # # # # # # # # # # # # # # #</td><td>+ + + + + + + + + + + + + + + + + + +</td><td>4 4 4 4 6 0 0 7 6 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7</td></td<></td></td<>	44.0         44.0 <td< td=""><td>+ + + + + + + + + + + + + + + + + + +</td><td>+ + + + + + + + + + + + + + + + + + +</td><td></td><td># # # # # # # # # # # # # # # # # # #</td><td># # # # # # # # # # # # # # # # # # #</td><td>+ + + + + + + + + + + + + + + + + + +</td><td>4 4 4 4 6 0 0 7 6 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7</td></td<>	+ + + + + + + + + + + + + + + + + + +	+ + + + + + + + + + + + + + + + + + +		# # # # # # # # # # # # # # # # # # #	# # # # # # # # # # # # # # # # # # #	+ + + + + + + + + + + + + + + + + + +	4 4 4 4 6 0 0 7 6 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7
4         +	4. +         +	+ + + + + + + + + + + + + + + + + + +	+ + + + + + + + + + + + + + + + + + +		# # # # # # # # # # # # # # # # # # #	+ + + + + + + + + + + + + + + + + + +	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
+         +	+         +	+ + + + + + + + + + + + + + + + + + +	+ + + + + + + + + + + + + + + + + + +		# # # # # # # # # # # # # # # # # # #	4 + + + + + + + + + + + + + + + + + + +	+ + + · · · · · · · · · · · · · · · · ·	44400000000000000000000000000000000000
+         +	145.7         + <td>+ + + + + + + + + + + + + + + + + + +</td> <td>+ + + + + + + + + + + + + + + + + + +</td> <td></td> <td># # # # # # # # # # # # # # # # # # #</td> <td>+ + + + + + + + + + + + + + + + + + +</td> <td>00000000000000000000000000000000000000</td> <td>4400 4400 4400 4400 4400 4400 4400 440</td>	+ + + + + + + + + + + + + + + + + + +	+ + + + + + + + + + + + + + + + + + +		# # # # # # # # # # # # # # # # # # #	+ + + + + + + + + + + + + + + + + + +	00000000000000000000000000000000000000	4400 4400 4400 4400 4400 4400 4400 440
+         +	4         6         9	148.5   1	+         +         +         +         7.37         76.0         1.37         206.0         1.25         2.39         74.0         2.52         2.79         74.0         2.52         206.0         1.25         2.79         74.0         2.25         206.0         1.25         4.57         206.0         1.25         4.57         206.0         1.25         4.57         206.0         1.25         4.37         4.34         4.35         270.0         1.25         4.35         4.36         1.27		10	# 4 2 7 1 0 0 0 4 0 0 0 4 0 0 0 0 0 0 0 0 0 0 0	4 0 0 0 0 0 0 0 1 0 1 0 1 0 0 0 0 0 1	200 200 200 200 200 200 200 200 200 200
7.3         7.3         7.3         7.2         7.3         7.3         7.3         7.3         7.3         7.3         7.3         7.4         9.9         7.3         7.4         9.9         7.3         7.3         7.4         9.9         7.4         9.9         7.4         9.9         7.4         9.0         1.5         9.0         4.5         9.2 <td>7.8         7.37         +         9.91         7.37         206.0         1.5         162.0         +         16.09         9.23         +         12.06         9.23         7.6         9.3         7.6         9.3         7.6         9.3         7.6         9.3         7.6         9.3         7.6         9.3         7.6         9.3         7.6         9.2         3.5         6.18         8.5         6.18         8.5         6.11         4.5         7.6         9.2         3.7         2.5         2.0         1.5         1.6         9.5         9.6         9.2         3.7         2.0         9.2         3.6         4.6         4.8         4.8         4.8         4.8         4.8         4.8         4.8         4.8         4.8         4.8         4.8         4.8         4.8         4.8         7.0         9.2         2.0         9.2         3.0         9.2         3.0         9.2         3.0         9.2         3.0         9.2         3.0         9.2         3.0         9.2         3.0         9.2         3.0         9.2         3.0         9.2         4.8         4.8         4.8         4.8         4.8         4.8         4.8         4.8         &lt;</td> <td>10. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.</td> <td>7.37 + 9.91 7.37 206.0 1. 5.31 3.62 5.58 2.79 74.0 2. 2.52 4.95 3.87 2.52 206.0 1. 4.57 4.60 4.67 4.57 206.0 1. 4.63 3.74 6.01 3.74 270.0 1. 4.84 3.76 3.99 3.76 270.0 1. 3.06 3.12 4.04 3.35 770.0 1. 3.89 4.77 4.58 3.21 74.0 1. 3.97 4.18 5.98 3.97 206.0 1. 4.51 3.93 3.99 3.74 74.0 1. 5.47 7.46 9.09 3.74 74.0 1. 11.47 7.46 9.09 5.77 140.0 2. 11.47 7.46 9.09 5.77 140.0 2. 11.47 7.26 4.43 3.51 74.0 1. 2.68 3.69 3.19 2.68 206.0 1. 2.68 3.69 3.31 2.66 0 1. 3.30 3.30 2.37 206.0 1.</td> <td>4 4 4 4 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8</td> <td></td> <td>7 4 4 4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6</td> <td>0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0</td> <td>206. 206. 206. 270. 270.</td>	7.8         7.37         +         9.91         7.37         206.0         1.5         162.0         +         16.09         9.23         +         12.06         9.23         7.6         9.3         7.6         9.3         7.6         9.3         7.6         9.3         7.6         9.3         7.6         9.3         7.6         9.3         7.6         9.2         3.5         6.18         8.5         6.18         8.5         6.11         4.5         7.6         9.2         3.7         2.5         2.0         1.5         1.6         9.5         9.6         9.2         3.7         2.0         9.2         3.6         4.6         4.8         4.8         4.8         4.8         4.8         4.8         4.8         4.8         4.8         4.8         4.8         4.8         4.8         4.8         7.0         9.2         2.0         9.2         3.0         9.2         3.0         9.2         3.0         9.2         3.0         9.2         3.0         9.2         3.0         9.2         3.0         9.2         3.0         9.2         3.0         9.2         4.8         4.8         4.8         4.8         4.8         4.8         4.8         4.8         <	10. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.	7.37 + 9.91 7.37 206.0 1. 5.31 3.62 5.58 2.79 74.0 2. 2.52 4.95 3.87 2.52 206.0 1. 4.57 4.60 4.67 4.57 206.0 1. 4.63 3.74 6.01 3.74 270.0 1. 4.84 3.76 3.99 3.76 270.0 1. 3.06 3.12 4.04 3.35 770.0 1. 3.89 4.77 4.58 3.21 74.0 1. 3.97 4.18 5.98 3.97 206.0 1. 4.51 3.93 3.99 3.74 74.0 1. 5.47 7.46 9.09 3.74 74.0 1. 11.47 7.46 9.09 5.77 140.0 2. 11.47 7.46 9.09 5.77 140.0 2. 11.47 7.26 4.43 3.51 74.0 1. 2.68 3.69 3.19 2.68 206.0 1. 2.68 3.69 3.31 2.66 0 1. 3.30 3.30 2.37 206.0 1.	4 4 4 4 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8		7 4 4 4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	206. 206. 206. 270. 270.
5.5         5.3         3.6         5.5         6.79         7.64         5.29         8.05         4.53         7.4           8.3         2.5         4.65         3.67         2.60         1.5         187.5         6.18         5.86         3.25         6.01         4.81         3.52         206         0         1.5         187.5         6.18         5.86         3.56         6.01         4.81         2.70         0         4.25         206         0         1.5         187.5         6.18         5.86         3.14         4.81         4.81         4.13         2.70         2.50         1.5         187.0         5.89         5.38         4.96         3.86         4.13         2.70         3.70         3.70         4.15         4.12         4.12         4.13         2.70         3.86         4.12         4.13         4.13         2.70         3.70         3.70         3.70         4.15         4.12         4.12         4.14         3.74         4.16         4.15         4.12         3.91         4.16         4.13         2.70         3.70         3.70         3.70         3.70         3.70         3.70         3.70         3.70         3.70         3.70 <t< td=""><td>5.2         5.31         3.62         5.58         2.79         74.0         2.0         162.0         4.53         6.79         7.64         5.29         8.05         4.53         74.0           3.3         2.52         4.95         3.87         2.52         206.0         1.5         187.0         6.18         5.86         3.51         4.81         5.20         6.01         4.81         206.0         1.5         187.0         5.61         5.11         4.87         4.69         4.81         5.11         4.81         206.0         4.61         3.62         4.63         3.14         5.11         4.81         4.82         4.69         4.61         4.81         4.81         4.81         4.81         4.81         4.81         270         200         1.5         224.0         5.89         5.38         4.98         4.81         4.81         270         270         200         3.89         4.82         4.88         4.89         4.81         270</td><td>  1.5   1.5   2.6   2.75   2.79   74.0   2.0   162.0   4.53   6.79   7.64   5.29   8.05   4.53   74.0   2.06   3.5   3.5   2.06   3.5   3.5   3.5   2.06   3.5   3</td><td>5.31 3.62 5.58 2.79 74.0 2.52 4.95 3.87 2.52 206.0 1.4.63 3.74 6.01 3.74 270.0 11.47 2.59 4.92 3.59 2.70.0 11.47 2.59 4.92 3.59 2.70.0 11.47 2.59 4.92 3.59 2.70.0 11.47 2.59 4.92 3.59 3.76 2.70.0 11.47 4.58 3.70 3.76 2.06.0 11.47 4.58 3.21 74.0 11.47 7.46 9.09 3.34 74.0 11.47 7.46 9.09 5.77 140.0 2.11.47 7.46 9.09 5.77 140.0 2.11.47 7.46 9.09 5.77 140.0 2.11.47 7.46 9.09 5.77 140.0 2.11.47 7.46 9.09 5.77 140.0 2.11.47 7.46 9.09 5.77 140.0 1.2.68 3.69 3.38 2.70.0 11.47 7.46 9.09 5.77 140.0 2.11.47 7.46 9.09 5.77 140.0 2.11.47 7.46 9.09 5.77 140.0 1.2.68 3.69 3.38 2.70.0 11.47 7.46 9.09 5.77 140.0 2.11.47 7.46 9.09 5.77 140.0 1.2.68 3.69 3.38 2.70.0 1.2.68 3.69 3.70.0 1.2.68 3.69 3.70.0 1.2.68 3.60 0.1.70.0 3</td><td>4 6 6 4 4 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8</td><td></td><td>4 4 4 4 4 6 6 7 7 7 8 6 6 7 7 7 8 6 7 7 8 6 7 7 8 6 7 7 8 6 7 7 8 6 7 7 8 6 7 7 8 6 7 7 8 6 7 8 7 8</td><td>0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0</td><td>206. 206. 206. 270. 270.</td></t<>	5.2         5.31         3.62         5.58         2.79         74.0         2.0         162.0         4.53         6.79         7.64         5.29         8.05         4.53         74.0           3.3         2.52         4.95         3.87         2.52         206.0         1.5         187.0         6.18         5.86         3.51         4.81         5.20         6.01         4.81         206.0         1.5         187.0         5.61         5.11         4.87         4.69         4.81         5.11         4.81         206.0         4.61         3.62         4.63         3.14         5.11         4.81         4.82         4.69         4.61         4.81         4.81         4.81         4.81         4.81         4.81         270         200         1.5         224.0         5.89         5.38         4.98         4.81         4.81         270         270         200         3.89         4.82         4.88         4.89         4.81         270	1.5   1.5   2.6   2.75   2.79   74.0   2.0   162.0   4.53   6.79   7.64   5.29   8.05   4.53   74.0   2.06   3.5   3.5   2.06   3.5   3.5   3.5   2.06   3.5   3	5.31 3.62 5.58 2.79 74.0 2.52 4.95 3.87 2.52 206.0 1.4.63 3.74 6.01 3.74 270.0 11.47 2.59 4.92 3.59 2.70.0 11.47 2.59 4.92 3.59 2.70.0 11.47 2.59 4.92 3.59 2.70.0 11.47 2.59 4.92 3.59 3.76 2.70.0 11.47 4.58 3.70 3.76 2.06.0 11.47 4.58 3.21 74.0 11.47 7.46 9.09 3.34 74.0 11.47 7.46 9.09 5.77 140.0 2.11.47 7.46 9.09 5.77 140.0 2.11.47 7.46 9.09 5.77 140.0 2.11.47 7.46 9.09 5.77 140.0 2.11.47 7.46 9.09 5.77 140.0 2.11.47 7.46 9.09 5.77 140.0 1.2.68 3.69 3.38 2.70.0 11.47 7.46 9.09 5.77 140.0 2.11.47 7.46 9.09 5.77 140.0 2.11.47 7.46 9.09 5.77 140.0 1.2.68 3.69 3.38 2.70.0 11.47 7.46 9.09 5.77 140.0 2.11.47 7.46 9.09 5.77 140.0 1.2.68 3.69 3.38 2.70.0 1.2.68 3.69 3.70.0 1.2.68 3.69 3.70.0 1.2.68 3.60 0.1.70.0 3	4 6 6 4 4 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8		4 4 4 4 4 6 6 7 7 7 8 6 6 7 7 7 8 6 7 7 8 6 7 7 8 6 7 7 8 6 7 7 8 6 7 7 8 6 7 7 8 6 7 7 8 6 7 8 7 8	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	206. 206. 206. 270. 270.
83         2.52         4.95         3.87         2.52         206.0         1.5         175.5         6.18         5.86         3.52         6.01         4.81         206         1.0         4.67         4.60         4.67         4.67         4.60         4.67         4.60         4.67         4.67         206.0         1.5         199.0         5.64         5.11         4.81         4.87         206         10         4.11         4.13         6.60         4.13         6.60         1.5         215.0         5.89         5.38         4.96         3.66         270         3.62         4.96         3.66         3.14         4.13         6.70         3.86         4.87         4.96         3.66         270         3.86         4.87         4.96         3.66         270         3.86         4.87         4.96         3.96         270         3.88         4.87         4.98         4.96         3.96         4.96         3.96         4.96         3.96         4.96         3.96         4.96         3.96         4.96         3.96         4.96         3.96         4.96         3.96         4.96         3.96         4.96         3.96         4.96         3.96         4.96         3.96 <td>83         2.52         4.95         3.87         2.52         206.0         1.5         175.5         6.18         5.86         3.52         6.01         4.81         3.52         206.0         4.60         4.57         206.0         1.5         199.0         6.18         5.86         5.14         6.11         4.13         6.64         4.83         4.96         4.68         4.69         4.69         5.14         5.11         4.13         6.70         3.62         215.0         5.89         5.14         5.11         4.13         6.70         3.66         215.0         5.89         5.14         4.13         6.70         3.6         215.0         3.86         4.96         3.66         5.10         3.86         270         3.62         4.06         3.86         4.06         3.86         2.70         3.70         3.72         4.96         3.96         3.96         3.96         3.96         3.96         3.96         3.96         3.96         3.96         3.96         3.96         3.96         3.96         3.96         3.96         3.96         4.18         3.96         3.96         3.96         4.86         4.16         4.16         3.96         4.96         3.96         4.86         &lt;</td> <td>  175.5   4.95   3.57   2.52   206.0   1.5   175.5   6.18   5.86   3.52   6.01   4.81   3.52   206.0   4.57   4.67   4.57   206.0   1.5   1.5   1.5   1.5   4.87   4.89  </td> <td>4.57 4.60 4.67 4.57 206.0 1.4.57 4.60 4.67 4.57 206.0 1.4.63 3.74 6.01 3.74 270.0 1.4.64 3.35 270.0 1.4.84 3.75 270.0 1.4.84 3.76 270.0 1.4.84 3.76 270.0 1.4.84 3.76 270.0 1.4.84 3.76 270.0 1.4.85 3.78 4.82 3.78 2.70.0 1.4.85 3.89 4.77 4.58 3.54 74.0 1.4.8 5.98 3.97 206.0 1.4.85 3.84 3.86 0 1.4.85 3.88 2.74 74.0 1.88 5.94 3.94 3.94 3.86 0 1.4.87 7.46 9.09 5.77 140.0 2.4.85 3.38 2.70.0 1.4.87 7.46 9.09 5.77 140.0 2.4.87 3.18 6.80 3.38 2.70.0 1.4.87 7.46 9.09 5.77 140.0 2.4.87 3.23 2.37 206.0 1.4.87 7.46 9.09 5.77 140.0 2.4.87 3.51 74.0 1.4.97 7.46 9.09 5.77 140.0 2.4.87 3.51 74.0 1.4.97 7.46 9.09 5.77 140.0 2.4.87 3.51 74.0 1.4.97 7.46 9.09 5.77 7.40 7.40 7.40 7.40 7.40 7.40 7.40 7</td> <td></td> <td>0 4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0</td> <td>4 4 4 4 0 0 0 4 4 6 0 0 0 4 4 6 0 0 0 0</td> <td>**************************************</td> <td>2006. 2006. 2007. 2007.</td>	83         2.52         4.95         3.87         2.52         206.0         1.5         175.5         6.18         5.86         3.52         6.01         4.81         3.52         206.0         4.60         4.57         206.0         1.5         199.0         6.18         5.86         5.14         6.11         4.13         6.64         4.83         4.96         4.68         4.69         4.69         5.14         5.11         4.13         6.70         3.62         215.0         5.89         5.14         5.11         4.13         6.70         3.66         215.0         5.89         5.14         4.13         6.70         3.6         215.0         3.86         4.96         3.66         5.10         3.86         270         3.62         4.06         3.86         4.06         3.86         2.70         3.70         3.72         4.96         3.96         3.96         3.96         3.96         3.96         3.96         3.96         3.96         3.96         3.96         3.96         3.96         3.96         3.96         3.96         3.96         4.18         3.96         3.96         3.96         4.86         4.16         4.16         3.96         4.96         3.96         4.86         <	175.5   4.95   3.57   2.52   206.0   1.5   175.5   6.18   5.86   3.52   6.01   4.81   3.52   206.0   4.57   4.67   4.57   206.0   1.5   1.5   1.5   1.5   4.87   4.89	4.57 4.60 4.67 4.57 206.0 1.4.57 4.60 4.67 4.57 206.0 1.4.63 3.74 6.01 3.74 270.0 1.4.64 3.35 270.0 1.4.84 3.75 270.0 1.4.84 3.76 270.0 1.4.84 3.76 270.0 1.4.84 3.76 270.0 1.4.84 3.76 270.0 1.4.85 3.78 4.82 3.78 2.70.0 1.4.85 3.89 4.77 4.58 3.54 74.0 1.4.8 5.98 3.97 206.0 1.4.85 3.84 3.86 0 1.4.85 3.88 2.74 74.0 1.88 5.94 3.94 3.94 3.86 0 1.4.87 7.46 9.09 5.77 140.0 2.4.85 3.38 2.70.0 1.4.87 7.46 9.09 5.77 140.0 2.4.87 3.18 6.80 3.38 2.70.0 1.4.87 7.46 9.09 5.77 140.0 2.4.87 3.23 2.37 206.0 1.4.87 7.46 9.09 5.77 140.0 2.4.87 3.51 74.0 1.4.97 7.46 9.09 5.77 140.0 2.4.87 3.51 74.0 1.4.97 7.46 9.09 5.77 140.0 2.4.87 3.51 74.0 1.4.97 7.46 9.09 5.77 7.40 7.40 7.40 7.40 7.40 7.40 7.40 7		0 4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	4 4 4 4 0 0 0 4 4 6 0 0 0 4 4 6 0 0 0 0	**************************************	2006. 2006. 2007. 2007.
100         4.57         206.0         1.5         187.0         5.64         5.31         4.87         4.87         206.0         1.5         189.0         4.30         5.14         4.13         5.64         4.87         206         4.63         3.74         6.01         3.74         5.00         1.5         215.0         6.30         5.11         4.13         5.64         4.83         5.11         4.13         5.04         3.82         4.96         4.96         4.96         4.96         4.96         4.96         3.91         270         3.92         224.0         3.82         4.96         4.96         4.96         4.96         4.96         3.91         270         3.96         3.97         4.96         4.66         4.96	10         4.57         4.60         4.57         206.0         1.5         187.0         5.64         5.31         4.87         4.88         4.87         206.1           1.5         4.63         3.74         6.01         3.74         270.0         1.5         199.0         4.36         5.18         4.18         4.89         4.81         270.0         3.70         1.5         224.0         3.82         4.98         4.96         3.66         4.91         3.82         74         3.70         3.95         4.89         4.38         4.96         3.66         4.94         3.82         74         4.15         4.16         3.91         4.70         3.82         74         9.83         4.96         3.86         4.96         3.66         4.94         3.91         270         74         4.86         3.95         4.98         4.96         3.96         4.94         3.91         4.70         3.91         4.96         3.96         4.96         3.96         4.96         3.96         4.96         3.96         4.96         3.96         4.96         3.96         4.96         3.96         4.96         3.96         4.96         3.96         4.96         3.91         4.96         3.91	187.0 4.57 4.60 4.67 4.57 206.0 1.5 187.0 5.64 5.31 4.87 4.89 4.88 4.87 206.  187.0 4.63 2.74 6.01 3.74 270.0 1.5 189.0 4.30 5.14 4.87 4.89 4.88 4.87 270.  187.1 4.15 4.12 4.44 5.15 2.70.0 1.5 224.0 3.82 4.98 4.68 4.55 4.94 3.82 770.  187.1 4.15 4.12 4.44 3.35 74.0 1.5 224.0 3.82 4.98 4.68 4.55 4.94 3.82 770.  187.1 4.15 4.12 4.44 3.35 74.0 1.5 224.0 3.89 4.32 3.50 3.91 4.34 3.82 770.  187.1 4.14 4.15 4.14 4.14 3.15 74.0 1.5 224.0 3.89 4.32 3.50 3.91 4.34 3.48 770.  187.1 4.14 4.15 3.12 4.44 3.06 2.00 1.5 224.0 3.89 4.32 3.50 3.48 4.34 3.48 770.  187.1 4.14 4.15 3.19 3.10 7.40 1.5 224.0 3.89 4.32 3.50 3.48 4.34 3.48 7.70 3.48 4.21 4.10 4.15 5.15 3.88 74.20 3.49 4.29 4.10 4.10 4.10 1.5 282.0 5.68 4.59 4.10 4.10 4.10 1.5 282.0 5.20 5.68 4.59 4.10 4.10 4.10 1.5 282.0 5.48 4.10 4.10 4.10 1.5 3.80 4.10 4.10 4.10 1.5 3.10 1.0 5.42 6.49 10.49 5.93 4.79 4.10 1.5 3.80 4.10 4.10 1.5 3.80 4.10 4.10 1.5 3.80 4.10 4.10 1.5 3.80 4.10 4.10 1.5 3.80 4.10 4.10 1.5 3.80 4.10 4.10 1.5 3.80 4.10 4.10 1.5 3.80 4.10 4.10 1.5 3.80 4.10 4.10 1.5 3.80 4.10 4.10 1.5 3.80 4.10 4.10 1.5 3.80 4.10 1.10 1.10 1.10 1.10 1.10 1.10 1.1	4.57 4.60 4.67 4.57 206.0 1.463 3.74 6.01 3.74 270.0 1.471 2.59 4.92 3.59 270.0 1.484 3.35 74.0 1.484 3.35 74.0 1.484 3.76 270.0 1.484 3.76 270.0 1.484 3.76 270.0 1.484 3.76 270.0 1.489 4.77 4.58 3.21 74.0 1.489 4.21 3.94 3.94 3.94 3.94 3.94 3.94 3.94 3.94	7 4 4 0 0 3 3 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	F H O 80 O 4 A 4 4 W 4 W W 4 W 8 H 80 W 90 A H 0 9 W 80 W 10 W 4 H 0 9 W 80 W 10	8 4 0 4 0 4 1 6 4 1 6 4 1 6 1 6 1 6 1 6 1 6 1 6 1	206. 270. 270. 270.
.56         4.63         3.74         6.01         3.74         270.0         1.5         199.0         4.30         5.14         5.11         4.13         6.64         4.13         270           .11         4.77         2.59         4.92         3.59         270.0         1.5         215.0         5.89         5.36         5.10         3.86         270         3.86         270.0         1.5         220.0         3.95         4.96         3.96         4.96         3.91         4.16         3.91         4.16         3.91         270         3.91         270         3.95         4.96         3.91         4.16         3.91         4.16         3.91         4.16         3.91         4.16         3.91         4.20         3.91         4.20         3.91         4.21         3.91         3.79         4.21         3.91         4.21         3.91         4.21         3.91         4.21         3.92         3.92         4.21         4.14         4.15         5.15         3.91         4.21         3.91         4.21         4.21         4.14         4.15         5.15         3.91         4.21         4.21         4.21         4.21         4.21         4.21         4.21         4.21<	.56         4.63         3.74         6.01         3.74         270.0         1.5         215.0         5.89         5.38         5.31         4.36         5.11         4.13         6.64         4.13         270.0         1.5         215.0         5.89         5.89         4.96         3.86         5.10         3.86         5.10         3.86         5.10         3.86         5.10         3.86         4.96         3.86         5.10         3.86         4.96         3.86         4.96         3.86         4.96         3.86         4.96         3.91         270.0         3.92         4.82         3.91         4.16         3.91         270.0         3.95         4.82         4.96         4.86         4.96         4.96         4.96         4.96         4.96         4.86         4.86         4.86         4.86         4.86         4.86         4.86         4.86         4.86	56 4.63 3.74 6.01 3.74 270.0 1.5 199.0 4.30 5.14 5.11 4.13 6.64 4.13 270.  11 4.17 2.59 4.92 3.59 270.0 1.5 215.0 5.89 5.38 4.96 4.56 4.55 4.94 3.82 74.  12 4.14 4.15 4.44 3.25 270.0 1.5 220.0 3.89 4.08 4.08 4.56 4.36 3.91 270.  13 4.15 4.16 3.12 4.04 3.06 206.0 1.5 220.0 3.89 4.35 3.91 4.16 3.91 270.  14 5.16 3.12 4.04 3.06 206.0 1.5 220.0 3.89 4.35 3.91 4.16 3.91 270.  15 3.06 3.12 4.04 3.06 206.0 1.5 220.0 3.89 4.32 3.50 3.48 4.34 3.48 2.70 2.70 3.00 3.00 4.30 4.30 4.30 3.91 4.16 3.91 2.70 3.00 3.91 4.10 4.12 4.15 5.15 3.00 3.91 2.70 3.91 4.10 4.10 4.10 4.10 4.10 4.10 4.10 4.1	4.63 3.74 6.01 3.74 270.0 1.4.15 4.12 4.92 3.59 270.0 1.4.84 3.35 74.0 1.4.84 3.35 74.0 1.4.84 3.76 270.0 1.3.06 3.12 4.04 3.76 270.0 1.3.06 3.12 4.04 3.76 270.0 1.3.89 4.77 4.58 3.21 74.0 1.3.89 4.77 4.58 3.97 206.0 1.4.85 3.99 3.74 74.0 1.4.85 3.18 3.11 74.0 1.3.85 4.92 4.01 4.01 336.0 1.4.47 7.46 9.09 5.77 140.0 2.4.85 3.38 2.70.0 1.4.87 7.26 4.43 3.51 74.0 1.3.25 2.37 2.68 3.69 3.38 2.70.0 1.3.25 2.37 2.83 3.23 2.37 2.06.0 1.3.25 2.06.0 1.3.2	4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	22 9 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	H 0 80 0 0 4 0	40 40 40 40 40 40 40 40 40 40 40 40 40 4	270. 270. 270.
4.77         2.59         4.92         3.86         5.10         3.86         5.10         3.86         5.10         3.86         5.10         3.86         5.10         3.86         5.10         3.86         4.96         3.86         5.10         3.86         74         4.15         4.15         4.98         4.68         4.58         4.94         3.82         74         4.16         3.76         4.06         3.06         3.06         3.06         3.06         3.09         3.79         4.85         4.98         4.68         4.55         4.94         3.48         270         3.91         3.10         3.48         4.34         3.48         270         3.99         3.48         4.34         3.48         4.34         3.48         4.34         3.48         4.34         3.48         4.34         3.48         4.34         3.48         4.34         3.48         4.34         3.48         4.34         3.48         4.34         3.48         4.34         3.48         4.34         3.48         4.34         3.48         3.49         3.79         4.21         3.48         4.36         4.36         4.36         4.36         4.36         4.36         4.37         4.21         4.21         4.21<	11         4.77         2.59         4.96         3.86         5.10         3.86         5.10         3.86         5.10         3.86         5.10         3.86         5.10         3.86         5.10         3.86         5.10         3.86         5.10         3.86         5.10         3.86         5.10         3.86         4.97         4.44         3.35         74.0         1.5         224.0         3.89         4.32         3.50         3.91         4.96         3.91         4.96         3.91         74         1.7         4.84         3.91         4.16         5.10         3.82         70         3.70 </td <td>111 4.77 \$\cdot 5.9  4.92  3.59  270.0  1.5  215.0  5.89  5.38  4.96  5.80  5.10  3.86  5.10  3.82  774.15  4.12  4.44  3.35  74.0  1.5  224.0  3.85  4.95  4.96  3.95  4.95  4.96  3.91  4.15  3.92  74.2  3.06  3.06  206.0  1.5  236.0  3.89  4.32  3.50  3.48  4.15  5.39  4.85  4.96  3.91  4.15  5.91  2.70  3.66  3.66  0.15  236.0  3.89  4.32  3.50  3.48  4.15  5.35  3.48  2.70  3.78  4.82  3.54  74.0  1.5  226.0  3.89  4.87  4.15  5.98  3.99  4.15  5.96  3.91  4.15  5.96  3.91  4.15  5.96  3.95  4.15  5.96  3.95  4.15  5.96  4.21  3.94  3.94  3.96  1.5  5.20  5.20  5.68  4.22  4.15  4.15  5.96  4.21  3.94  3.96  1.5  5.20  5.68  4.22  4.15  4.15  5.96  4.15  4.15  5.96  4.25</td> <td>4.77 2.59 4.92 3.59 270.0 1.48 4.35 3.76 270.0 1.48 4.37 4.04 3.35 74.0 1.306 3.12 4.04 3.06 206.0 1.306 3.12 4.04 3.06 206.0 1.309 4.21 74.0 1.309 4.21 74.0 1.309 3.34 74.0 1.309 3.11 74.0 1.309 3.38 270.0 1.309 3.38 270.0 1.309 3.38 270.0 1.309 3.38 270.0 1.309 3.38 270.0 1.309 3.38 270.0 1.309 3.38 270.0 1.309 3.38 270.0 1.309 3.38 270.0 1.309 3.38 270.0 1.309 3.38 2.37 206.0 1.309 3.39 2.68 206.0 1.309 3.30 2.37 2.68 3.69 3.39 2.68 206.0 1.309 2.37 2.68 3.69 3.30 2.37 2.68 3.30 2.30 2.30 2.30 3.30 2.30 3.30 2.30 3.30 2.30 3.30 3</td> <td>21.5 24.0 26.0 26.0 26.0 26.0 26.0 26.0 26.0 26</td> <td>6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6</td> <td>6 8 0 0 4 6 8 4 8 8 4 8 8 8 8 9 4 1 0 8 1 1 8 1 8 8</td> <td>0 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4</td> <td>270.</td>	111 4.77 \$\cdot 5.9  4.92  3.59  270.0  1.5  215.0  5.89  5.38  4.96  5.80  5.10  3.86  5.10  3.82  774.15  4.12  4.44  3.35  74.0  1.5  224.0  3.85  4.95  4.96  3.95  4.95  4.96  3.91  4.15  3.92  74.2  3.06  3.06  206.0  1.5  236.0  3.89  4.32  3.50  3.48  4.15  5.39  4.85  4.96  3.91  4.15  5.91  2.70  3.66  3.66  0.15  236.0  3.89  4.32  3.50  3.48  4.15  5.35  3.48  2.70  3.78  4.82  3.54  74.0  1.5  226.0  3.89  4.87  4.15  5.98  3.99  4.15  5.96  3.91  4.15  5.96  3.91  4.15  5.96  3.95  4.15  5.96  3.95  4.15  5.96  4.21  3.94  3.94  3.96  1.5  5.20  5.20  5.68  4.22  4.15  4.15  5.96  4.21  3.94  3.96  1.5  5.20  5.68  4.22  4.15  4.15  5.96  4.15  4.15  5.96  4.25	4.77 2.59 4.92 3.59 270.0 1.48 4.35 3.76 270.0 1.48 4.37 4.04 3.35 74.0 1.306 3.12 4.04 3.06 206.0 1.306 3.12 4.04 3.06 206.0 1.309 4.21 74.0 1.309 4.21 74.0 1.309 3.34 74.0 1.309 3.11 74.0 1.309 3.38 270.0 1.309 3.38 270.0 1.309 3.38 270.0 1.309 3.38 270.0 1.309 3.38 270.0 1.309 3.38 270.0 1.309 3.38 270.0 1.309 3.38 270.0 1.309 3.38 270.0 1.309 3.38 270.0 1.309 3.38 2.37 206.0 1.309 3.39 2.68 206.0 1.309 3.30 2.37 2.68 3.69 3.39 2.68 206.0 1.309 2.37 2.68 3.69 3.30 2.37 2.68 3.30 2.30 2.30 2.30 3.30 2.30 3.30 2.30 3.30 2.30 3.30 3	21.5 24.0 26.0 26.0 26.0 26.0 26.0 26.0 26.0 26	6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	6 8 0 0 4 6 8 4 8 8 4 8 8 8 8 9 4 1 0 8 1 1 8 1 8 8	0 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	270.
47         4.15         4.44         3.35         74.0         1.5         224.0         3.82         4.98         4.68         4.55         4.94         3.82         74         3.91         270.0         1.5         230.0         3.95         4.85         4.90         3.91         4.16         3.91         270         4.84         3.76         270.0         1.5         230.0         3.95         4.85         4.36         3.91         270         3.91         270         3.92         3.76         3.91         270         3.93         3.91         270         3.91         270         3.93         3.91         4.34         4.34         3.79         74         3.82         4.20         4.16         5.08         4.36         3.79         74         3.83         74         74.0         1.5         253.0         4.52         4.29         4.16         5.08         4.21         3.93         3.79         74         3.83         4.21         4.29         4.16         5.08         4.21         3.79         74         3.79         4.29         4.29         4.16         5.08         4.21         4.21         4.21         4.21         4.21         4.21         4.21         4.21	47         4.15         4.16         4.68         4.68         4.68         4.68         4.68         4.68         4.68         4.68         4.89         3.82         74         4.16         3.99         3.76         3.99         3.76         3.99         3.76         3.99         3.76         3.99         3.76         3.99         3.76         3.99         3.76         3.99         3.76         3.99         3.76         3.99         3.77         4.88         3.79         4.14         4.15         5.15         3.91         270           4.56         3.79         4.21         3.50         3.79         4.29         4.16         5.08         4.98         3.79         74           .00         3.97         4.21         3.94         3.96         1.5         263.0         4.29         4.16         5.08         4.98         3.79         74           .01         4.21         3.94         3.36         0         1.5         263.0         4.08         4.29         4.16         6.20         4.21         3.08         4.21         3.43         74         1.40         6.25         4.21         4.21         4.21         4.21         4.21         4.21         4.	47 4.15 4.12 4.44 3.35 74.0 1.5 224.0 3.82 4.98 4.68 4.55 4.94 3.82 74.97 4.15 4.15 4.12 4.44 3.35 74.0 1.5 230.0 3.95 4.26 4.25 4.99 3.76 3.99 3.76 270.0 1.5 230.0 3.95 4.26 4.26 3.49 4.34 3.48 2.70 3.16 3.10 3.10 3.10 3.10 3.10 3.10 3.10 3.10	4.15 4.12 4.44 3.35 74.0 1.  4.84 3.76 3.99 3.76 270.0 1.  3.06 3.12 4.04 3.06 206.0 1.  3.70 3.78 4.82 3.54 74.0 1.  3.89 4.77 4.58 3.21 74.0 1.  4.34 4.21 3.94 3.97 206.0 1.  4.51 3.93 3.99 3.74 74.0 1.  8.59 4.92 4.01 4.01 336.0 1.  11.47 7.46 9.09 5.77 140.0 2.  4.05 7.26 4.43 3.51 74.0 1.  2.68 3.69 3.38 270.0 1.  2.68 3.69 3.39 2.68 206.0 1.  2.77 2.83 3.23 2.37 206.0 1.  3.04 3.00 2.00 3.36.0 1.	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	2 4 98 4 89 4 8 8 8 8 8 8 8 8 8 8 8 8 8 8	8 0 0 4 0 0 4 0 0 0 0 0 0 0 0 0 0 0 0 0	40. 44. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6	276. 270.
.77         4.84         3.76         3.70         1.5         230.0         3.95         4.85         4.90         3.91         4.16         3.91         270           .96         3.06         3.12         4.04         3.06         206.0         1.5         236.0         3.89         4.32         3.50         3.48         4.34         3.48         270           .96         3.06         3.78         4.02         3.50         1.5         254.0         3.59         4.16         5.08         4.34         3.79         74           .94         3.80         3.21         74.0         1.5         263.0         4.28         4.21         4.06         6.25         4.21         206           .90         3.97         206.0         1.5         282.0         5.20         5.68         4.59         4.21         3.79         74         27         336         4.21         3.36         4.21         3.36         4.21         3.36         4.21         3.36         4.21         3.36         4.21         4.21         3.36         4.21         4.21         4.21         4.21         4.21         4.21         4.21         4.21         4.21         4.21         4.	.77         4.84         3.76         3.99         3.76         270.0         1.5         230.0         3.95         4.85         4.90         3.91         4.16         3.91         270           .96         3.06         3.12         4.04         3.06         206.0         1.5         240.0         3.89         4.32         3.50         3.48         4.34         3.91         270           .96         3.06         3.06         3.06         1.5         256.0         3.79         4.16         5.08         4.39         3.79         74           .94         3.89         4.77         4.58         3.21         74.0         1.5         263.0         4.29         4.16         5.08         4.27         3.74           .00         3.97         4.06.0         1.5         263.0         4.52         4.29         4.60         3.79         7.40           .36         4.34         4.21         3.94         3.50         1.5         282.0         5.20         5.68         4.57         4.24         4.27         3.69         4.21         4.34         4.31         4.34         4.34         4.34         4.34         4.34         4.34         4.34 <t< td=""><td>7.77 4.84 3.76 3.99 3.76 270.0 1.5 230.0 3.95 4.85 4.90 3.91 4.16 3.91 270.  9.6 3.10 4.04 3.06 206.0 1.5 236.0 3.89 4.32 3.50 3.48 4.34 2.34 2.70 2.70 4.34 2.54 3.66 2.06.0 1.5 240.0 3.69 4.32 3.50 3.48 4.34 3.79 74.34 2.70 3.10 4.18 5.98 3.21 74.0 1.5 240.0 3.79 4.29 4.16 5.08 4.98 3.79 74.39 2.70 3.79 4.21 3.94 3.97 206.0 1.5 254.0 3.79 4.29 4.16 5.08 4.98 3.79 74.21 3.94 3.94 3.36 0 1.5 282.0 5.20 5.68 4.50 4.31 4.40 6.25 4.21 206. 3.79 4.21 3.94 3.94 3.36 0 1.5 282.0 5.20 5.68 4.50 4.31 4.31 4.31 4.27 3.36 2.35 4.51 3.93 3.99 3.74 74.0 1.5 293.0 4.04 4.13 5.24 4.31 4.31 4.31 4.31 74.0 1.5 305.0 3.42 6.01 3.58 3.57 74.3 74.3 74.3 74.3 1.2 3.93 3.99 3.74 7.0 1.5 3.90 0 3.52 6.49 10.49 5.93 4.79 4.79 3.36 2.25 8.59 4.92 4.01 4.01 3.36.0 1.5 3.30 0 3.52 6.49 10.49 5.93 4.79 4.79 4.79 3.36 2.06 2.37 2.38 6.80 3.38 2.70 1.5 3.90 3.50 0 3.52 6.81 4.27 3.69 6.95 3.50 74.3 1.0 1.5 3.00 0 3.52 6.81 4.27 3.69 6.95 3.50 74.3 1.0 1.5 3.00 0 3.64 3.08 3.79 3.44 3.08 3.44 2.81 2.06 2.00 2.37 2.83 2.30 2.20 3.36.0 1.5 3.36 0 2.36 4.40 3.17 3.19 2.87 2.81 2.00 2.37 2.20 3.36.0 1.5 3.36 2.36 4.40 3.17 3.19 2.87 2.36 7.48 2.41 2.41 2.41 2.41 2.41 2.41 2.41 2.41</td><td>4.84 3.76 3.99 3.76 270.0 1.3.06 3.12 4.04 3.06 206.0 1.3.18 4.82 3.54 74.0 1.3.89 4.77 4.58 3.21 74.0 1.3.4 4.21 3.94 3.97 206.0 1.4.34 4.21 3.99 3.74 74.0 1.3.13 3.11 74.0 1.3.13 3.13 3.14 74.0 1.3.13 3.13 3.14 74.0 1.3.13 3.11 74.0 1.3.13 3.13 3.13 74.0 1.3.13 3.13 3.14 7.4.0 1.3.13 3.13 3.13 2.70.0 1.3.13 3.3.13 2.70.0 1.3.13 3.3.13 2.70.0 1.3.13 3.3.13 2.68 3.69 3.38 2.70.0 1.3.13 3.3.13 2.68 3.69 3.38 2.70.0 1.3.13 3.3.13 2.68 3.69 3.37 2.66.0 1.3.13 3.74 7.40 1.3.13 3.37 2.66.0 1.3.13 3.37 2.66.0 1.3.13 3.37 2.66.0 1.3.13 3.37 2.66.0 1.3.13 3.37 2.66.0 1.3.13 3.37 2.66.0 1.3.13 3.37 2.66.0 1.3.13 3.37 2.66.0 1.3.13 3.37 2.66 2.68 3.38 2.33 2.33 2.33 2.33 2.33 2.33 2.3</td><td>86.00 W W W W W W W W W W W W W W W W W W</td><td>5 4.85 4. 9 4.32 3.</td><td>6 4 4 91 6 5 1 5 5 6 8 9 1 5 5 6 8 9 1 5 5 6 8 9 1 5 5 6 8 9 1 5 5 6 8 9 9 1 5 6 8 9 9 1 5 6 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9</td><td>.34 3.9</td><td>270.</td></t<>	7.77 4.84 3.76 3.99 3.76 270.0 1.5 230.0 3.95 4.85 4.90 3.91 4.16 3.91 270.  9.6 3.10 4.04 3.06 206.0 1.5 236.0 3.89 4.32 3.50 3.48 4.34 2.34 2.70 2.70 4.34 2.54 3.66 2.06.0 1.5 240.0 3.69 4.32 3.50 3.48 4.34 3.79 74.34 2.70 3.10 4.18 5.98 3.21 74.0 1.5 240.0 3.79 4.29 4.16 5.08 4.98 3.79 74.39 2.70 3.79 4.21 3.94 3.97 206.0 1.5 254.0 3.79 4.29 4.16 5.08 4.98 3.79 74.21 3.94 3.94 3.36 0 1.5 282.0 5.20 5.68 4.50 4.31 4.40 6.25 4.21 206. 3.79 4.21 3.94 3.94 3.36 0 1.5 282.0 5.20 5.68 4.50 4.31 4.31 4.31 4.27 3.36 2.35 4.51 3.93 3.99 3.74 74.0 1.5 293.0 4.04 4.13 5.24 4.31 4.31 4.31 4.31 74.0 1.5 305.0 3.42 6.01 3.58 3.57 74.3 74.3 74.3 74.3 1.2 3.93 3.99 3.74 7.0 1.5 3.90 0 3.52 6.49 10.49 5.93 4.79 4.79 3.36 2.25 8.59 4.92 4.01 4.01 3.36.0 1.5 3.30 0 3.52 6.49 10.49 5.93 4.79 4.79 4.79 3.36 2.06 2.37 2.38 6.80 3.38 2.70 1.5 3.90 3.50 0 3.52 6.81 4.27 3.69 6.95 3.50 74.3 1.0 1.5 3.00 0 3.52 6.81 4.27 3.69 6.95 3.50 74.3 1.0 1.5 3.00 0 3.64 3.08 3.79 3.44 3.08 3.44 2.81 2.06 2.00 2.37 2.83 2.30 2.20 3.36.0 1.5 3.36 0 2.36 4.40 3.17 3.19 2.87 2.81 2.00 2.37 2.20 3.36.0 1.5 3.36 2.36 4.40 3.17 3.19 2.87 2.36 7.48 2.41 2.41 2.41 2.41 2.41 2.41 2.41 2.41	4.84 3.76 3.99 3.76 270.0 1.3.06 3.12 4.04 3.06 206.0 1.3.18 4.82 3.54 74.0 1.3.89 4.77 4.58 3.21 74.0 1.3.4 4.21 3.94 3.97 206.0 1.4.34 4.21 3.99 3.74 74.0 1.3.13 3.11 74.0 1.3.13 3.13 3.14 74.0 1.3.13 3.13 3.14 74.0 1.3.13 3.11 74.0 1.3.13 3.13 3.13 74.0 1.3.13 3.13 3.14 7.4.0 1.3.13 3.13 3.13 2.70.0 1.3.13 3.3.13 2.70.0 1.3.13 3.3.13 2.70.0 1.3.13 3.3.13 2.68 3.69 3.38 2.70.0 1.3.13 3.3.13 2.68 3.69 3.38 2.70.0 1.3.13 3.3.13 2.68 3.69 3.37 2.66.0 1.3.13 3.74 7.40 1.3.13 3.37 2.66.0 1.3.13 3.37 2.66.0 1.3.13 3.37 2.66.0 1.3.13 3.37 2.66.0 1.3.13 3.37 2.66.0 1.3.13 3.37 2.66.0 1.3.13 3.37 2.66.0 1.3.13 3.37 2.66.0 1.3.13 3.37 2.66 2.68 3.38 2.33 2.33 2.33 2.33 2.33 2.33 2.3	86.00 W W W W W W W W W W W W W W W W W W	5 4.85 4. 9 4.32 3.	6 4 4 91 6 5 1 5 5 6 8 9 1 5 5 6 8 9 1 5 5 6 8 9 1 5 5 6 8 9 1 5 5 6 8 9 9 1 5 6 8 9 9 1 5 6 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	.34 3.9	270.
.96         3.06         3.06         206.0         1.5         236.0         3.89         4.32         3.50         3.48         4.34         3.48         270           .45         3.70         3.78         4.82         3.54         74.0         1.5         240.0         3.88         4.87.4         4.15         5.15         3.88         74           .94         3.70         3.78         74.0         1.5         254.0         3.09         4.28         4.21         4.08         7.79         74           .00         3.97         4.28         4.21         4.04         6.25         4.21         4.01         4.21         2.0         74	.96         3.12         4.04         3.06         206.0         1.5         236.0         3.89         4.32         3.50         3.48         4.34         3.48         270         3.88         4.32         3.54         74.0         1.5         240.0         3.88         4.87         4.18         5.15         3.48         270         3.48         2.15         3.48         270         3.48         3.79         3.	96 3.06 3.12 4.04 3.06 206.0 1.5 236.0 3.89 4.32 3.50 3.48 4.134 3.48 270.  45 3.70 3.78 4.82 3.54 74.0 1.5 240.0 3.88 4.87 4.14 4.15 5.15 3.48 770 74.0 1.5 240.0 3.88 4.87 4.14 4.15 5.15 3.79 74.0 1.5 240.0 3.08 4.21 4.16 5.08 4.98 3.79 74.0 1.5 263.0 4.52 4.28 4.21 4.40 6.25 4.21 206. 3.79 4.18 5.98 3.97 206.0 1.5 282.0 5.28 4.28 4.21 4.40 6.25 4.21 206. 3.56 4.21 3.94 3.94 3.94 3.94 3.94 3.94 3.94 3.94	3.06 3.12 4.04 3.06 206.0 1.3.70 3.78 4.82 3.54 74.0 1.3.89 4.77 4.58 3.21 74.0 1.3.34 4.21 3.94 3.97 206.0 1.4.34 4.21 3.94 3.94 3.94 3.94 3.6.0 1.3.95 4.92 4.01 4.01 336.0 1.1.47 7.46 9.09 5.77 140.0 2.11.47 7.46 9.09 5.77 140.0 2.11.47 7.26 4.43 3.51 74.0 1.2.68 3.69 3.38 270.0 1.2.68 3.69 3.37 206.0 1.3.93 3.23 2.37 206.0 1.3.93 3.23 2.37 206.0 1.3.93 3.04 3.06 2.06 3.36 0.00 3.36 0.00 3.36 0.00 3.36 0.00 3.36 0.00 3.36 0.00 3.37 206.0 3.37 20	86.0 86.0 86.0 86.0 86.0 86.0 86.0 86.0	9 4.32 3.	6 4 3.48 5 5.08	.34 3.4	270
.45         3.70         3.88         4.87         4.14         4.15         5.15         3.88         74           .94         3.79         4.29         4.16         5.08         4.98         3.79         74           .94         3.89         4.77         4.58         3.21         74.0         1.5         254.0         3.79         4.16         5.08         4.98         3.79         74           .00         3.97         4.18         5.98         3.97         206.0         1.5         263.0         4.51         4.21         4.40         6.25         4.21         3.06           .36         4.34         4.21         3.94         3.14         74.0         1.5         293.0         4.04         4.27         4.27         4.27         3.04         4.27         3.04         4.27         4.27         3.04         4.27         3.04         4.27         3.04         4.27         4.27         3.04         4.27         3.04         4.27         4.27         3.04         4.27         3.04         4.27         3.04         4.27         3.04         4.27         3.04         4.27         3.04         4.27         3.04         4.27         3.04 <td< td=""><td>45         3.76         4.82         3.54         74.0         1.5         240.0         3.88         4.87         4.15         5.15         3.88         74           94         3.89         4.77         4.58         3.21         74.0         1.5         254.0         3.79         4.29         4.16         5.08         4.98         3.79         74           94         3.89         4.77         4.60         1.5         262.0         5.20         4.29         4.21         4.21         3.79         74           36         4.34         4.51         3.94         3.94         3.96         1.5         293.0         4.04         4.73         4.82         4.31         4.21         4.21         4.21         3.20         4.21</td><td>145 3.70 3.78 4.82 3.54 74.0 1.5 240.0 3.88 4.87.4.14 4.15 5.15 5.15 3.88 74.14 3.88 74.14 4.58 3.21 74.58 3.21 74.0 1.5 263.0 3.79 4.29 4.16 5.08 4.98 3.79 74.29 4.10 2.63 0.0 3.89 4.27 4.58 3.21 74.0 1.5 263.0 4.52 4.28 4.21 4.21 2.06 74.2 4.24 3.94 3.94 3.94 3.94 3.94 3.96 1.5 263.0 4.52 4.28 4.21 4.31 4.31 2.06 7.2 4.34 4.21 3.93 3.94 3.09 3.74 74.0 1.5 293.0 4.04 4.73 4.82 4.31 4.31 4.04 74.2 74.2 6.5 5.47 3.16 3.13 3.11 74.0 1.5 305.0 3.43 5.24 6.01 3.58 3.57 3.43 74.2 77 11.47 7.46 9.09 5.77 140.0 1.5 335.0 3.43 5.24 6.01 3.58 3.57 3.43 74.2 77 11.47 7.46 9.09 5.77 140.0 2.0 3.20 6.26 12.82 8.21 9.56 6.25 140.2 74.1 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2</td><td>3.70 3.78 4.82 3.54 74.0 1.3.89 4.77 4.58 3.21 74.0 1.3.93 4.34 4.21 3.94 3.97 206.0 1.4.34 4.51 3.94 3.99 3.74 74.0 1.5.47 4.58 3.99 3.74 74.0 1.5.47 7.46 9.09 5.77 140.0 2.11.47 7.46 9.09 5.77 140.0 2.11.47 7.26 4.43 3.51 74.0 1.2.68 3.69 3.38 2.70.0 1.2.68 3.69 3.37 206.0 1.3.93 3.23 2.37 206.0 1.3.93 3.04 3.06 2.07 3.06 3.06 3.07 3.06 3.07 3.06 3.07 3.06 3.07 3.07 3.07 3.07 3.07 3.07 3.07 3.07</td><td>664.0 63.0 63.0 63.0</td><td>8 4.87 4.</td><td>4 4.15 6 5.08</td><td>م س</td><td></td></td<>	45         3.76         4.82         3.54         74.0         1.5         240.0         3.88         4.87         4.15         5.15         3.88         74           94         3.89         4.77         4.58         3.21         74.0         1.5         254.0         3.79         4.29         4.16         5.08         4.98         3.79         74           94         3.89         4.77         4.60         1.5         262.0         5.20         4.29         4.21         4.21         3.79         74           36         4.34         4.51         3.94         3.94         3.96         1.5         293.0         4.04         4.73         4.82         4.31         4.21         4.21         4.21         3.20         4.21	145 3.70 3.78 4.82 3.54 74.0 1.5 240.0 3.88 4.87.4.14 4.15 5.15 5.15 3.88 74.14 3.88 74.14 4.58 3.21 74.58 3.21 74.0 1.5 263.0 3.79 4.29 4.16 5.08 4.98 3.79 74.29 4.10 2.63 0.0 3.89 4.27 4.58 3.21 74.0 1.5 263.0 4.52 4.28 4.21 4.21 2.06 74.2 4.24 3.94 3.94 3.94 3.94 3.94 3.96 1.5 263.0 4.52 4.28 4.21 4.31 4.31 2.06 7.2 4.34 4.21 3.93 3.94 3.09 3.74 74.0 1.5 293.0 4.04 4.73 4.82 4.31 4.31 4.04 74.2 74.2 6.5 5.47 3.16 3.13 3.11 74.0 1.5 305.0 3.43 5.24 6.01 3.58 3.57 3.43 74.2 77 11.47 7.46 9.09 5.77 140.0 1.5 335.0 3.43 5.24 6.01 3.58 3.57 3.43 74.2 77 11.47 7.46 9.09 5.77 140.0 2.0 3.20 6.26 12.82 8.21 9.56 6.25 140.2 74.1 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2	3.70 3.78 4.82 3.54 74.0 1.3.89 4.77 4.58 3.21 74.0 1.3.93 4.34 4.21 3.94 3.97 206.0 1.4.34 4.51 3.94 3.99 3.74 74.0 1.5.47 4.58 3.99 3.74 74.0 1.5.47 7.46 9.09 5.77 140.0 2.11.47 7.46 9.09 5.77 140.0 2.11.47 7.26 4.43 3.51 74.0 1.2.68 3.69 3.38 2.70.0 1.2.68 3.69 3.37 206.0 1.3.93 3.23 2.37 206.0 1.3.93 3.04 3.06 2.07 3.06 3.06 3.07 3.06 3.07 3.06 3.07 3.06 3.07 3.07 3.07 3.07 3.07 3.07 3.07 3.07	664.0 63.0 63.0 63.0	8 4.87 4.	4 4.15 6 5.08	م س	
94         3.89         4.77         4.58         3.21         74.0         1.5         254.0         3.79         4.29         4.16         5.08         4.98         3.79         74           .00         3.97         4.18         5.98         3.97         206.0         1.5         263.0         4.52         4.21         4.40         6.25         4.21         206           .36         4.34         4.21         3.94         4.21         4.21         4.21         4.21         4.21         4.21         4.21         4.21         4.21         4.21         4.21         3.14         3.14         3.14         3.14         4.14         4.14         4.17         3.14         4.19         4.19         4.19         4.19         4.19         4.19         4.19         4.19         4.19         4.19         4.19         4.19         4.19         4.19         4.19	94         3.89         4.77         4.58         3.21         74.0         1.5         254.0         3.79         4.29         4.16         5.08         4.98         3.79         74.0           .00         3.97         4.18         5.98         3.97         206.0         1.5         263.0         4.52         4.21         4.40         6.25         4.21         3.79         74.0           .36         4.21         3.94 <td>94 3.89 4.77 4.58 3.21 74.0 1.5 254.0 3.79 4.29 4.16 5.08 4.98 3.79 74.00 3.97 4.18 5.98 3.97 206.0 1.5 263.0 4.52 4.28 4.51 4.40 6.25 4.21 206.2 3.6 4.98 3.79 74.00 3.97 206.0 1.5 283.0 4.52 4.58 4.51 4.40 6.25 4.21 206.2 3.6 4.31 4.31 4.31 4.31 4.27 336.0 2.2 6.6 6.6 6.2 6.2 6.2 6.2 6.2 6.2 6.2</td> <td>3.89 4.77 4.58 3.21 74.0 1. 3.97 4.18 5.98 3.97 206.0 1. 4.51 3.93 3.99 3.74 74.0 1. 5.47 3.16 3.13 3.11 74.0 1. 8.59 4.02 4.01 4.01 336.0 1. 11.47 7.46 9.09 5.77 140.0 2. 4.05 7.26 4.43 3.51 74.0 1. 2.68 3.69 3.19 2.68 206.0 1. 2.37 2.83 3.23 2.37 206.0 1.</td> <td>63.0 63.0 63.0 63.0 63.0</td> <td></td> <td>6 5.08</td> <td>0.0</td> <td>74.</td>	94 3.89 4.77 4.58 3.21 74.0 1.5 254.0 3.79 4.29 4.16 5.08 4.98 3.79 74.00 3.97 4.18 5.98 3.97 206.0 1.5 263.0 4.52 4.28 4.51 4.40 6.25 4.21 206.2 3.6 4.98 3.79 74.00 3.97 206.0 1.5 283.0 4.52 4.58 4.51 4.40 6.25 4.21 206.2 3.6 4.31 4.31 4.31 4.31 4.27 336.0 2.2 6.6 6.6 6.2 6.2 6.2 6.2 6.2 6.2 6.2	3.89 4.77 4.58 3.21 74.0 1. 3.97 4.18 5.98 3.97 206.0 1. 4.51 3.93 3.99 3.74 74.0 1. 5.47 3.16 3.13 3.11 74.0 1. 8.59 4.02 4.01 4.01 336.0 1. 11.47 7.46 9.09 5.77 140.0 2. 4.05 7.26 4.43 3.51 74.0 1. 2.68 3.69 3.19 2.68 206.0 1. 2.37 2.83 3.23 2.37 206.0 1.	63.0 63.0 63.0 63.0 63.0		6 5.08	0.0	74.
.00         3.97         4.18         5.98         3.97         206.0         1.5         282.0         5.20         5.68         4.21         4.40         6.25         4.21         336           .23         4.34         4.21         3.94         3.95         4.27         3.36         4.27         3.36         4.27         3.36         4.27         3.36         4.27         3.36         4.27         3.36         4.27         3.36         4.27         3.36         4.27         3.36         4.27         3.36         4.27         3.36         4.27         3.36         4.27         3.36         4.27         3.36         4.27         3.36         4.27         3.36         4.27         3.36         4.27         3.36         4.27         3.26         6.26         4.28         4.21         3.27         4.27	3.97     4.18     5.98     3.97     206.0     1.5     263.0     4.52     4.28     4.21     4.40     6.25     4.21     206.0       36     4.34     4.21     3.94     336.0     1.5     282.0     5.68     4.59     4.50     4.27     4.27     336.0       .23     4.51     3.93     3.74     74.0     1.5     293.0     4.04     4.73     4.62     4.27     4.27     336.0       .65     5.47     3.16     3.11     74.0     1.5     305.0     3.43     5.24     6.01     3.43     4.79     4.79     4.79       .25     8.59     4.92     4.01     336.0     1.5     312.0     5.42     6.49     10.49     5.93     4.79     4.79     4.79       .25     8.59     4.92     4.01     336.0     1.5     3321.0     8.64     6.26     12.93     4.79     4.79     336.0       .48     4.02     3.51     74.0     1.5     339.0     3.52     6.81     4.04     3.06     6.26     12.82     8.21     9.56     6.26     12.74       .40     2.03     3.52     3.52     6.81     3.06     0.09     3.52     1.36     1.36	.00     3.97     4.18     5.98     3.97     206.0     1.5     263.0     4.52     4.28     4.21     4.40     6.25     4.21     3.04       36     4.34     4.21     3.94     336.0     1.5     282.0     5.68     4.59     4.50     4.27     4.27     336.0       1.23     4.51     3.94     336.0     1.5     293.0     4.04     4.73     4.82     4.21     4.04     7.74     4.04     7.74       1.5     3.11     7.0     1.5     305.0     3.42     6.01     3.51     4.79     4.79     4.79     376       1.5     3.11     7.46     9.09     5.77     140.0     2.0     321.0     8.49     6.26     12.82     8.21     9.56     6.26     140.9       1.6     4.02     3.38     6.80     3.38     270.0     1.5     339.0     3.52     6.81     4.27     3.69     6.95     3.52     74       1.6     4.05     7.26     4.43     3.51     74.0     1.5     350.0     3.62     7.36     4.14     7.32     4.53     3.62     7.4       1.0     2.06     1.5     3.60     3.14     3.06     3.79     3.44     3.08	3.97 4.18 5.98 3.97 206.0 1. 4.34 4.21 3.94 3.94 336.0 1. 4.51 3.93 3.99 3.74 74.0 1. 5.47 3.16 3.13 3.11 74.0 1. 8.59 4.92 4.01 4.01 336.0 1. 11.47 7.46 9.09 5.77 140.0 2. 4.02 3.38 6.80 3.38 270.0 1. 4.05 7.26 4.43 3.51 74.0 1. 2.68 3.69 3.19 2.68 206.0 1. 2.37 2.83 3.23 2.37 206.0 1.	63.0 4	9 4.29 4.		.98 3.7	74.
.36     4.21     3.94     3.94     3.94     3.94     3.94     3.94     3.94     3.94     3.94     3.94     3.94     3.94     3.94     3.94     3.94     3.94     3.94     3.94     3.94     3.74     74.0     1.5     293.0     4.04     4.73     4.82     4.31     4.04     74       .65     5.47     3.11     74.0     1.5     305.0     3.43     5.24     6.01     3.57     3.43     74       .25     8.59     4.92     4.01     4.01     1.5     312.0     5.42     6.49     10.49     5.93     4.79 <td>.36     4.21     3.94     336.0     1.5     282.0     5.20     5.68     4.59     4.57     4.27     4.27     336.0       .23     4.51     3.93     3.74     74.0     1.5     293.0     4.04     4.73     4.82     4.31     4.04     74.0       .65     5.47     3.13     3.11     74.0     1.5     305.0     3.43     5.24     6.01     3.58     3.57     3.43     74.3       .25     8.59     4.92     4.01     4.01     336.0     1.5     312.0     5.42     6.49     10.49     5.93     4.79     4.79     34.3       .25     8.59     4.92     4.01     4.02     3.38     6.80     3.38     6.26     12.82     8.20     14.9       .48     4.02     3.38     6.80     3.52     6.81     4.27     3.62     140       .10     4.05     7.26     4.34     3.08     3.44     2.81     2.06       .10     2.37     2.06.0     1.5     352.0     3.64     3.62     2.81     3.08     3.44     2.81     2.06       .10     2.27     2.26     3.26     2.26     3.26     3.26     3.26     3.28     3.62     3.44</td> <td>36 4.34 4.21 3.94 3.94 336.0 1.5 282.0 5.20 5.68 4.59 4.50 4.27 4.27 336.23 4.51 3.93 3.99 3.74 74.0 1.5 293.0 4.04 4.73 4.82 4.31 4.31 4.04 74.0 74.0 1.5 293.0 4.04 4.73 4.82 4.31 4.31 4.04 74.0 74.0 1.5 305.0 3.43 5.24 6.01 3.58 3.57 3.43 74.27 74.0 1.5 305.0 3.43 5.24 6.01 3.58 3.57 3.43 74.79 74.6 9.09 5.77 140.0 2.0 3.12.0 5.42 6.49 10.49 5.93 4.79 4.79 336.1 1.47 7.46 9.09 5.77 140.0 2.0 3.20 3.20 3.52 7.36 4.14 7.36 6.26 140.1 1.5 339.0 3.52 6.81 4.27 3.69 6.26 140.1 1.5 3.60 0.3 1.2 2.6 1.2 1.8 3.62 7.36 4.14 3.08 3.44 2.63 3.52 7.36 4.14 3.08 3.44 2.81 2.06 7.4 2.63 2.30 2.20 336.0 1.5 383.0 2.36 4.40 3.17 3.19 2.87 2.36 7.4 2.63 2.30 2.20 336.0 1.5 394.0 2.97 2.96 2.02 2.00 2.78 2.60 2.00 3.64 2.63 2.81 3.08 2.87 2.80 2.60 2.70 3.65 2.88 3.88 2.80 2.80 2.80 2.80 2.80 2.80 2.80 2</td> <td>4.34 4.21 3.94 3.94 336.0 1. 4.51 3.93 3.99 3.74 74.0 1. 5.47 3.16 3.13 3.11 74.0 1. 8.59 4.92 4.01 4.01 336.0 1. 11.47 7.46 9.09 5.77 140.0 2. 4.02 3.38 6.80 3.38 270.0 1. 4.05 7.26 4.43 3.51 74.0 1. 2.68 3.69 3.19 2.68 206.0 1. 2.37 2.83 3.23 2.37 206.0 1. 3.04 3.06 2.68 1.93 74.0 1.</td> <td>82.0 5</td> <td>2 4.28 4.</td> <td>1 4.40</td> <td>.25 4.2</td> <td>206.</td>	.36     4.21     3.94     336.0     1.5     282.0     5.20     5.68     4.59     4.57     4.27     4.27     336.0       .23     4.51     3.93     3.74     74.0     1.5     293.0     4.04     4.73     4.82     4.31     4.04     74.0       .65     5.47     3.13     3.11     74.0     1.5     305.0     3.43     5.24     6.01     3.58     3.57     3.43     74.3       .25     8.59     4.92     4.01     4.01     336.0     1.5     312.0     5.42     6.49     10.49     5.93     4.79     4.79     34.3       .25     8.59     4.92     4.01     4.02     3.38     6.80     3.38     6.26     12.82     8.20     14.9       .48     4.02     3.38     6.80     3.52     6.81     4.27     3.62     140       .10     4.05     7.26     4.34     3.08     3.44     2.81     2.06       .10     2.37     2.06.0     1.5     352.0     3.64     3.62     2.81     3.08     3.44     2.81     2.06       .10     2.27     2.26     3.26     2.26     3.26     3.26     3.26     3.28     3.62     3.44	36 4.34 4.21 3.94 3.94 336.0 1.5 282.0 5.20 5.68 4.59 4.50 4.27 4.27 336.23 4.51 3.93 3.99 3.74 74.0 1.5 293.0 4.04 4.73 4.82 4.31 4.31 4.04 74.0 74.0 1.5 293.0 4.04 4.73 4.82 4.31 4.31 4.04 74.0 74.0 1.5 305.0 3.43 5.24 6.01 3.58 3.57 3.43 74.27 74.0 1.5 305.0 3.43 5.24 6.01 3.58 3.57 3.43 74.79 74.6 9.09 5.77 140.0 2.0 3.12.0 5.42 6.49 10.49 5.93 4.79 4.79 336.1 1.47 7.46 9.09 5.77 140.0 2.0 3.20 3.20 3.52 7.36 4.14 7.36 6.26 140.1 1.5 339.0 3.52 6.81 4.27 3.69 6.26 140.1 1.5 3.60 0.3 1.2 2.6 1.2 1.8 3.62 7.36 4.14 3.08 3.44 2.63 3.52 7.36 4.14 3.08 3.44 2.81 2.06 7.4 2.63 2.30 2.20 336.0 1.5 383.0 2.36 4.40 3.17 3.19 2.87 2.36 7.4 2.63 2.30 2.20 336.0 1.5 394.0 2.97 2.96 2.02 2.00 2.78 2.60 2.00 3.64 2.63 2.81 3.08 2.87 2.80 2.60 2.70 3.65 2.88 3.88 2.80 2.80 2.80 2.80 2.80 2.80 2.80 2	4.34 4.21 3.94 3.94 336.0 1. 4.51 3.93 3.99 3.74 74.0 1. 5.47 3.16 3.13 3.11 74.0 1. 8.59 4.92 4.01 4.01 336.0 1. 11.47 7.46 9.09 5.77 140.0 2. 4.02 3.38 6.80 3.38 270.0 1. 4.05 7.26 4.43 3.51 74.0 1. 2.68 3.69 3.19 2.68 206.0 1. 2.37 2.83 3.23 2.37 206.0 1. 3.04 3.06 2.68 1.93 74.0 1.	82.0 5	2 4.28 4.	1 4.40	.25 4.2	206.
.23     4.51     3.93     3.74     74.0     1.5     293.0     4.04     4.73     4.82     4.31     4.04     74       .65     5.47     3.16     3.13     3.11     74.0     1.5     305.0     3.43     5.24     6.01     3.57     3.43     74       .25     8.59     4.92     4.01     336.0     1.5     312.0     5.42     6.49     10.49     5.93     4.79     4.79     4.79     336       .77     11.47     7.46     9.09     5.77     140.0     2.0     321.0     8.49     6.26     12.82     8.21     9.66     6.26     140       .48     4.05     7.36     6.43     3.56     7.4     7.32     4.53     3.52     74       .10     2.68     3.59     3.14     3.74     3.74     3.08     3.09     3.44     3.08     3.08       .10     2.37     2.06.0     1.5     383.0     2.36     4.40     3.17     3.44     2.36     2.36       .12     3.04     3.23     2.20     3.36.0     1.5     394.0     2.97     2.96     2.82     2.60     2.78     2.60     2.78       .2     2.30     2.30     2.36	.23     4.51     3.93     3.74     74.0     1.5     293.0     4.04     4.73     4.82     4.31     4.04     74.0       .65     5.47     3.13     3.11     74.0     1.5     305.0     3.43     5.24     6.01     3.58     3.57     3.43     74.3       .25     8.59     4.92     4.01     4.01     336.0     1.5     312.0     5.42     6.49     10.49     5.93     4.79     4.79     34.3       .77     11.47     7.46     9.09     5.77     140.0     2.0     321.0     8.49     6.26     12.82     8.21     9.56     6.26     140       .48     4.02     3.38     6.80     3.38     270.0     1.5     339.0     3.52     6.81     4.27     3.62     74       .10     4.05     7.26     1.5     350.0     3.62     7.36     4.14     7.32     4.53     3.06     2.06       .10     2.37     2.88     3.23     2.37     3.44     3.08     3.44     2.81     2.06       .12     3.04     3.06     2.60     1.5     3.62     3.64     3.55     2.81     3.06     2.81     2.06     2.36     4.40     3.17     3.14	.23 4.51 3.93 3.99 3.74 74.0 1.5 293.0 4.04 4.73 4.82 4.31 4.31 4.04 74.05 5.47 3.16 3.13 3.11 74.0 1.5 305.0 3.43 5.24 6.01 3.58 3.57 3.43 74.25 8.59 4.92 4.01 4.01 336.0 1.5 312.0 5.42 6.49 10.49 5.93 4.79 4.79 336.25 7.7 140.0 2.0 3.21.0 8.49 6.26 12.82 8.21 9.56 6.26 140.2 7.7 11.47 7.46 9.09 5.77 140.0 2.0 3.21.0 8.49 6.26 12.82 8.21 9.56 6.26 140.2 4.8 4.02 3.38 6.80 3.38 2.70.0 1.5 339.0 3.52 7.36 4.14 7.27 3.69 6.95 3.52 7.4 4.05 3.69 3.19 2.60 2.00 1.5 350.0 3.62 7.36 4.14 7.79 3.62 7.4  3.62 7.4  3.62 7.4  3.62 7.4  3.62 7.4  3.62 7.4  3.62 7.4  3.62 7.4  3.62 7.4  3.62 7.4  3.62 7.4  3.62 7.4  3.62 7.4  3.64	4.51 3.93 3.99 3.74 74.0 1. 5.47 3.16 3.13 3.11 74.0 1. 8.59 4.92 4.01 4.01 336.0 1. 11.47 7.46 9.09 5.77 140.0 2. 4.02 3.38 6.80 3.38 270.0 1. 4.05 7.26 4.43 3.51 74.0 1. 2.68 3.69 3.19 2.68 206.0 1. 2.37 2.83 3.23 2.37 206.0 1. 3.04 3.06 2.68 1.93 74.0 1.	•	0 5.68 4.	9 4.50	.27 4.2	336.
.65     5.47     3.16     3.11     74.0     1.5     305.0     3.43     5.24     6.01     3.58     3.57     3.43     74       .25     8.59     4.01     336.0     1.5     312.0     5.42     6.49     10.49     5.93     4.79     4.79     336       .77     11.47     7.46     9.09     5.77     140.0     2.0     321.0     8.49     6.26     12.82     8.21     9.56     6.26     140       .48     4.02     3.38     270.0     1.5     339.0     3.52     6.81     4.27     3.69     6.95     3.52     74       .16     4.05     7.26     4.43     3.51     74.0     1.5     350.0     3.62     7.36     4.14     7.32     4.53     3.62     74       .10     2.68     3.69     3.14     3.08     3.79     3.44     3.08     2.06       .10     2.37     2.37     2.06.0     1.5     371.0     3.64     3.55     2.81     3.08     3.44     2.81     206       .12     3.04     3.06     2.36     4.40     3.17     3.19     2.78     2.60     2.78     2.60     2.78     2.60     2.78     2.60     2.78 <td>.65     5.47     3.16     3.11     74.0     1.5     305.0     3.43     5.24     6.01     3.58     3.57     3.43     74.       .25     8.59     4.92     4.01     336.0     1.5     312.0     5.42     6.49     10.49     5.93     4.79     4.79     336.0       .77     11.47     7.46     9.09     5.77     140.0     2.0     321.0     8.49     6.26     12.82     8.21     9.56     6.26     140       .48     4.02     3.38     6.80     3.38     270.0     1.5     339.0     3.52     6.81     4.27     3.69     6.95     3.52     74       .16     4.05     7.26     4.43     3.51     74.0     1.5     362.0     3.14     3.79     3.44     2.81     2.06       .10     2.37     2.88     3.23     2.37     2.81     3.06     1.5     362.0     3.14     3.19     3.44     2.81     2.06       .10     2.37     2.36     4.40     3.17     3.19     2.87     2.36     1.40       .10     2.20     2.20     2.20     3.36     1.40     1.5     394.0     2.97     2.96     2.85     2.45     4.80     140</td> <td>.65 5.47 3.16 3.13 3.11 74.0 1.5 305.0 3.43 5.24 6.01 3.58 3.57 3.43 74.  25 8.59 4.92 4.01 4.01 336.0 1.5 312.0 5.42 6.49 10.49 5.93 4.79 4.79 336.  77 11.47 7.46 9.09 5.77 140.0 2.0 321.0 8.49 6.26 12.82 8.21 9.56 6.26 140.  48 4.02 3.38 6.80 3.38 270.0 1.5 339.0 3.52 7.36 4.14 7.32 4.53 3.62 74.  10 2.68 2.06.0 1.5 350.0 3.62 7.36 4.14 7.32 4.53 3.62 74.  10 2.68 2.06.0 1.5 362.0 3.14 3.44 3.08 3.79 3.44 2.81 2.06.  11 3.04 2.63 2.30 2.20 2.20 336.0 1.5 394.0 2.97 2.96 2.82 2.60 2.78 2.60 2.70 2.70 3.66 5.28 4.82 4.36 140.0 1.5 394.0 2.97 2.96 2.82 2.60 2.78 2.60 2.70 3.66 2.70 3.70 3.64 3.70 3.70 3.70 3.70 3.70 3.70 3.70 3.70</td> <td>5.47 3.16 3.13 3.11 74.0 1. 8.59 4.92 4.01 4.01 336.0 1. 11.47 7.46 9.09 5.77 140.0 2. 4.02 3.38 6.80 3.38 270.0 1. 4.05 7.26 4.43 3.51 74.0 1. 2.37 2.83 3.23 2.37 206.0 1. 3.04 3.06 2.68 1.93 74.0 1.</td> <td>₩ O. 7</td> <td>4 4.73 4.</td> <td>2 4.31</td> <td>.31 4.0</td> <td>74.</td>	.65     5.47     3.16     3.11     74.0     1.5     305.0     3.43     5.24     6.01     3.58     3.57     3.43     74.       .25     8.59     4.92     4.01     336.0     1.5     312.0     5.42     6.49     10.49     5.93     4.79     4.79     336.0       .77     11.47     7.46     9.09     5.77     140.0     2.0     321.0     8.49     6.26     12.82     8.21     9.56     6.26     140       .48     4.02     3.38     6.80     3.38     270.0     1.5     339.0     3.52     6.81     4.27     3.69     6.95     3.52     74       .16     4.05     7.26     4.43     3.51     74.0     1.5     362.0     3.14     3.79     3.44     2.81     2.06       .10     2.37     2.88     3.23     2.37     2.81     3.06     1.5     362.0     3.14     3.19     3.44     2.81     2.06       .10     2.37     2.36     4.40     3.17     3.19     2.87     2.36     1.40       .10     2.20     2.20     2.20     3.36     1.40     1.5     394.0     2.97     2.96     2.85     2.45     4.80     140	.65 5.47 3.16 3.13 3.11 74.0 1.5 305.0 3.43 5.24 6.01 3.58 3.57 3.43 74.  25 8.59 4.92 4.01 4.01 336.0 1.5 312.0 5.42 6.49 10.49 5.93 4.79 4.79 336.  77 11.47 7.46 9.09 5.77 140.0 2.0 321.0 8.49 6.26 12.82 8.21 9.56 6.26 140.  48 4.02 3.38 6.80 3.38 270.0 1.5 339.0 3.52 7.36 4.14 7.32 4.53 3.62 74.  10 2.68 2.06.0 1.5 350.0 3.62 7.36 4.14 7.32 4.53 3.62 74.  10 2.68 2.06.0 1.5 362.0 3.14 3.44 3.08 3.79 3.44 2.81 2.06.  11 3.04 2.63 2.30 2.20 2.20 336.0 1.5 394.0 2.97 2.96 2.82 2.60 2.78 2.60 2.70 2.70 3.66 5.28 4.82 4.36 140.0 1.5 394.0 2.97 2.96 2.82 2.60 2.78 2.60 2.70 3.66 2.70 3.70 3.64 3.70 3.70 3.70 3.70 3.70 3.70 3.70 3.70	5.47 3.16 3.13 3.11 74.0 1. 8.59 4.92 4.01 4.01 336.0 1. 11.47 7.46 9.09 5.77 140.0 2. 4.02 3.38 6.80 3.38 270.0 1. 4.05 7.26 4.43 3.51 74.0 1. 2.37 2.83 3.23 2.37 206.0 1. 3.04 3.06 2.68 1.93 74.0 1.	₩ O. 7	4 4.73 4.	2 4.31	.31 4.0	74.
.25         8.59         4.01         336.0         1.5         312.0         5.42         6.49         10.49         5.93         4.79         4.79         336           .77         11.47         7.46         9.09         5.77         140.0         2.0         321.0         8.49         6.26         12.82         8.21         9.56         6.26         140           .48         4.02         3.38         6.80         3.38         270.0         1.5         339.0         3.52         6.81         4.27         3.69         6.95         3.52         74           .16         4.05         7.26         4.43         3.51         74.0         1.5         350.0         3.62         7.36         4.14         7.32         4.53         3.62         74           .10         2.68         3.69         3.14         3.44         3.08         2.06         2.08         2.06.0         1.5         371.0         3.64         3.55         2.81         3.08         3.08         2.06         2.31         2.36         4.40         3.17         3.19         2.87         2.56         2.78         2.60         2.78         2.60         2.78         2.60         2.78	.25         8.59         4.92         4.01         336.0         1.5         312.0         5.42         6.49         10.49         5.93         4.79         4.79         336.0           .77         11.47         7.46         9.09         5.77         140.0         2.0         321.0         8.49         6.26         12.82         8.21         9.56         6.26         140.0           .48         4.02         3.38         6.80         3.38         270.0         1.5         339.0         3.52         6.81         4.27         3.69         6.95         3.52         74           .16         4.02         3.38         6.80         3.51         74.0         1.5         350.0         3.64         3.78         4.53         3.62         74           .10         2.37         2.81         3.08         3.44         3.08         3.44         2.81         2.06         1.5         371.0         3.64         3.55         2.81         2.81         2.81         2.81         2.81         2.81         2.81         2.81         2.81         2.81         2.81         2.81         2.81         2.81         2.81         2.81         2.81         2.81         2.81	25 8.59 4.92 4.01 4.01 336.0 1.5 312.0 5.42 6.49 10.49 5.93 4.79 4.79 336.77 11.47 7.46 9.09 5.77 140.0 2.0 321.0 8.49 6.26 12.82 8.21 9.56 6.26 140.48 4.02 3.38 6.80 3.38 270.0 1.5 339.0 3.52 7.36 4.14 7.32 4.53 3.52 74.51 1.00 2.68 2.06.0 1.5 350.0 3.14 3.08 3.79 4.73 4.53 3.62 74.51 1.00 2.68 3.69 3.19 2.68 2.06.0 1.5 362.0 3.14 3.08 3.74 3.08 3.74 2.06.0 1.5 371.0 3.64 3.55 2.81 3.08 3.44 3.08 2.06.0 1.5 371.0 3.64 3.55 2.81 3.08 3.44 2.81 2.06.1 1.5 383.0 2.36 4.00 3.17 3.19 2.87 2.36 74.14 2.63 2.30 2.20 336.0 1.5 394.0 2.97 2.96 2.62 2.60 2.78 2.60 2.70 3.08 3.44 2.63 2.60 2.78 2.60 2.70 3.08 3.44 2.63 2.60 2.78 2.60 2.70 3.08 3.44 2.63 2.60 2.78 2.60 2.70 3.08 3.44 2.63 2.60 2.78 2.60 2.70 3.08 3.44 2.63 2.60 2.78 2.60 2.70 3.08 3.44 2.63 2.60 2.78 2.60 2.78 2.60 2.70 3.08 3.44 2.63 2.60 2.78 2.60 2.78 2.60 2.70 3.08 3.44 2.63 2.60 2.78 2.60 2.78 2.60 2.70 3.08 3.44 2.63 2.60 2.78 2.60 2.70 3.08 3.44 2.63 2.60 2.78 2.60 2.70 3.08 3.44 2.63 2.60 2.78 2.60 2.70 3.08 3.44 2.63 2.60 2.78 2.60 2.70 3.08 3.44 2.63 2.60 2.78 2.60 2.70 3.08 3.44 2.63 2.60 2.78 2.60 2.70 3.08 3.44 2.63 2.60 2.70 3.08 3.44 3.08 3.40 3.08 3.44 3.08 3.44 3.08 3.40 3.08 3.44 3.08 3.40 3.08 3.40 3.00 3.00 3.00 3.00 3.00 3.00 3.00	8.59 4.92 4.01 4.01 336.0 1. 11.47 7.46 9.09 5.77 140.0 2. 4.02 3.38 6.80 3.38 270.0 1. 4.05 7.26 4.43 3.51 74.0 1. 2.68 3.69 3.19 2.68 206.0 1. 2.37 2.83 3.23 2.37 206.0 1. 3.04 3.0 2.0 3.7 206.0 1.	05.0 3	3 5.24 6.	1 3.58	.57 3.4	74.
.77     11.47     7.46     9.09     5.77     140.0     2.0     321.0     8.49     6.26     12.82     8.21     9.56     6.26     140       .48     4.02     3.38     6.80     3.38     270.0     1.5     350.0     3.52     74     7.36     4.14     7.32     4.53     3.62     74       .10     2.68     3.69     3.19     2.68     206.0     1.5     362.0     3.14     3.44     3.08     3.79     3.44     3.08     206       .06     2.37     2.83     3.23     2.37     206.0     1.5     371.0     3.64     3.55     2.81     3.08     3.44     2.81     206       .12     3.04     3.06     2.36     4.40     3.17     3.19     2.87     2.36     74       .44     2.63     2.20     2.20     2.20     2.78     2.60     2.78     2.60     2.78	.77     11.47     7.46     9.09     5.77     140.0     2.0     321.0     8.49     6.26     12.82     8.21     9.56     6.26     140.       .48     4.02     3.38     6.80     3.38     270.0     1.5     339.0     3.52     6.81     4.27     3.69     6.95     3.52     74       .16     4.02     7.26     4.43     3.51     74.0     1.5     350.0     3.62     7.36     4.14     7.32     4.53     3.62     74       .10     2.68     3.06     0     1.5     371.0     3.64     3.64     3.08     3.44     2.81     206       .12     3.04     3.04     3.64     3.17     3.19     2.81     2.06     2.78     2.60     2.76       .12     3.04     2.97     2.96     2.82     2.60     2.78     2.60     2.70       .44     2.63     2.20     336.0     1.5     403.0     4.95     4.89     5.92     5.45     4.89     140.0	.77 11.47 7.46 9.09 5.77 140.0 2.0 321.0 8.49 6.26 12.82 8.21 9.56 6.26 140.48 4.02 3.38 6.80 3.38 270.0 1.5 339.0 3.52 6.81 4.27 3.69 6.95 3.52 74.51 16 4.05 7.26 4.43 3.51 74.0 1.5 350.0 3.62 7.36 4.14 7.32 4.53 3.62 74.51 10 2.68 3.69 3.19 2.68 206.0 1.5 350.0 3.14 3.44 3.08 3.44 2.08 206.0 1.5 371.0 3.64 3.08 3.74 2.08 2.06 2.0 1.5 371.0 3.64 3.05 2.81 3.08 3.44 2.81 2.06 2.0 1.5 371.0 3.64 3.55 2.81 3.08 3.44 2.81 2.06 2.0 2.20 336.0 1.5 394.0 2.97 2.96 2.82 2.60 2.78 2.60 2.70 2.36 5.28 5.28 4.82 4.36 140.0 1.5 394.0 2.97 2.96 2.82 2.60 2.78 2.60 2.70 2.00 2.00 2.00 2.00 2.00 2.00 2.0	11.47 7.46 9.09 5.77 140.0 2. 4.02 3.38 6.80 3.38 270.0 1. 4.05 7.26 4.43 3.51 74.0 1. 2.68 3.69 3.19 2.68 206.0 1. 2.37 2.83 3.23 2.37 206.0 1. 3.04 3.06 2.68 1.93 74.0 1.	12.0 5	2 6.49 10.	9 5.93	. 79 4.7	336.
.48     4.02     3.38     6.80     3.38     270.0     1.5     339.0     3.52     6.81     4.27     3.69     6.95     3.52       .16     4.05     7.26     4.43     3.51     74.0     1.5     350.0     3.62     7.36     4.14     7.32     4.53     3.62       .10     2.68     3.19     2.68     206.0     1.5     362.0     3.14     3.08     3.79     3.44     2.81     3.08     2.44     2.81     3.08     3.44     2.81     2.81       .12     3.04     3.06     2.68     1.93     74.0     1.5     383.0     2.36     4.40     3.17     3.19     2.87     2.60     2.78       .44     2.63     2.30     2.20     2.20     336.0     1.5     394.0     2.97     2.96     2.82     2.60     2.78     2.60     2.78	.48     4.02     3.38     6.80     3.38     270.0     1.5     339.0     3.52     6.81     4.27     3.69     6.95     3.52     74.       .16     4.05     7.26     4.43     3.51     74.0     1.5     350.0     3.62     7.36     4.14     7.32     4.53     3.62     74.       .10     2.68     3.69     3.19     2.68     206.0     1.5     371.0     3.14     3.44     3.08     3.44     2.06       .12     3.04     3.06     2.37     2.06.0     1.5     383.0     2.36     4.40     3.17     3.19     2.81     2.06       .12     3.04     3.06     2.20     336.0     1.5     394.0     2.97     2.96     2.82     2.60     2.78     2.60     2.70       .44     2.28     5.28     5.28     4.89     5.92     5.45     4.89     140.0	.48 4.02 3.38 6.80 3.38 270.0 1.5 339.0 3.52 6.81 4.27 3.69 6.95 3.52 74.  16 4.05 7.26 4.43 3.51 74.0 1.5 350.0 3.62 7.36 4.14 7.32 4.53 3.62 74.  10 2.68 3.69 3.19 2.68 206.0 1.5 352.0 3.14 3.44 3.08 3.79 3.44 2.06.  10 2.68 3.69 3.19 2.68 206.0 1.5 371.0 3.64 3.55 2.81 3.08 3.44 2.06.  12 3.04 3.06 2.68 1.93 7.40 1.5 383.0 2.36 4.40 3.17 3.19 2.87 2.36 74.  14 2.63 2.30 2.20 336.0 1.5 394.0 2.97 2.96 2.62 2.60 2.78 2.60 2.70 2.00 3.00 3.00 3.00 3.00 3.00 3.00 3.0	4.02 3.38 6.80 3.38 270.0 1. 4.05 7.26 4.43 3.51 74.0 1. 2.68 3.69 3.19 2.68 206.0 1. 2.37 2.83 3.23 2.37 206.0 1. 3.04 3.06 2.68 1.93 74.0 1.	21.0 8	9 6.26 12.	2 8.21	.56 6.2	140
.16     4.05     7.26     4.43     3.51     74.0     1.5     350.0     3.62     7.36     4.14     7.32     4.53     3.62       .10     2.68     3.69     3.19     2.68     206.0     1.5     362.0     3.14     3.08     3.79     3.44     3.08     20       .06     2.37     2.37     2.06.0     1.5     371.0     3.64     3.55     2.81     3.08     3.44     2.81     2.81       .12     3.04     3.06     2.68     1.93     74.0     1.5     383.0     2.36     4.40     3.17     3.19     2.87     2.36       .44     2.63     2.30     2.20     2.20     336.0     1.5     394.0     2.97     2.96     2.82     2.60     2.78     2.60     2.78	16     4.05     7.26     4.43     3.51     74.0     1.5     350.0     3.62     7.36     4.14     7.32     4.53     3.62     74.       10     2.68     3.19     2.68     206.0     1.5     362.0     3.14     3.08     3.79     3.44     3.08     206       10     2.37     2.81     2.37     206.0     1.5     371.0     3.64     3.55     2.81     3.08     3.44     2.81     206       12     3.04     3.06     2.68     1.93     74.0     1.5     383.0     2.36     4.40     3.17     3.19     2.87     2.36     74.       14     2.63     2.20     2.20     336.0     1.5     394.0     2.97     2.96     2.82     2.60     2.78     2.60     2.70       36     5.28     5.28     4.82     4.36     140.0     1.5     403.0     4.95     4.89     5.97     5.92     5.45     4.89     140.0	16 4.05 7.26 4.43 3.51 74.0 1.5 350.0 3.62 7.36 4.14 7.32 4.53 3.62 74.  10 2.68 3.69 3.19 2.68 206.0 1.5 362.0 3.14 3.44 3.08 3.79 3.44 3.08 206.0 2.66 2.37 2.37 2.68 2.37 2.60 1.5 371.0 3.64 3.55 2.81 3.08 3.44 2.81 2.06 2.60 2.37 2.83 3.23 2.37 2.83 74.0 1.5 383.0 2.36 4.40 3.17 3.19 2.87 2.36 74.0 44 2.63 2.30 2.20 2.20 336.0 1.5 394.0 2.97 2.96 2.82 2.60 2.78 2.60 2.70 2.36 5.28 5.28 4.82 4.36 140.0 1.5 \$	4.05 7.26 4.43 3.51 74.0 1. 2.68 3.69 3.19 2.68 206.0 1. 2.37 2.83 3.23 2.37 206.0 1. 3.04 3.06 2.68 1.93 74.0 1.	39.0 3	2 6.81 4.	7 3.69	.95 3.5	74.
.10 2.68 3.69 3.19 2.68 206.0 1.5 362.0 3.14 3.44 3.08 3.79 3.44 3.08 20. 06 2.37 2.83 3.23 2.37 206.0 1.5 371.0 3.64 3.55 2.81 3.08 3.44 2.81 20. 12 3.04 3.06 2.68 1.93 74.0 1.5 383.0 2.36 4.40 3.17 3.19 2.87 2.36 7. 3.44 2.63 2.30 2.20 2.20 336.0 1.5 394.0 2.97 2.96 2.82 2.60 2.78 2.60 2.78	.10     2.68     3.69     3.19     2.68     206.0     1.5     362.0     3.14     3.08     3.74     3.08     206     206.0       .06     2.37     2.83     2.37     206.0     1.5     371.0     3.64     3.55     2.81     3.08     3.44     2.81     206       .12     3.04     3.06     2.68     1.93     74.0     1.5     383.0     2.36     4.40     3.17     3.19     2.87     2.36     74.0       .44     2.63     2.20     2.20     336.0     1.5     394.0     2.97     2.96     2.60     2.78     2.60     2.70       .36     5.28     4.82     4.36     140.0     1.5     403.0     4.95     4.89     5.97     5.92     5.45     4.89     140.0	.10 2.68 3.69 3.19 2.68 206.0 1.5 362.0 3.14 3.44 3.08 3.79 3.44 3.08 206.0 2.06 2.37 2.83 2.37 2.06.0 1.5 371.0 3.64 3.55 2.81 3.08 3.44 2.81 2.06 2.06 2.37 2.83 74.0 1.5 383.0 2.36 4.40 3.17 3.19 2.87 2.36 74.12 3.04 2.60 2.20 2.20 336.0 1.5 394.0 2.97 2.96 2.82 2.60 2.78 2.60 2.70 2.06 2.28 5.28 4.82 4.36 140.0 1.5 403.0 4.95 4.89 5.97 5.92 5.45 4.89 140.0 1.5 SEGMENT MINIMUM = 2.36 AT THE 383.0 INCH STATION	2.68 3.69 3.19 2.68 206.0 1. 2.37 2.83 3.23 2.37 206.0 1. 3.04 3.06 2.68 1.93 74.0 1.	50.03	2 7.36 4.	4 7.32	.53 3.6	74.
.06 2.37 2.83 3.23 2.37 206.0 1.5 371.0 3.64 3.55 2.81 3.08 3.44 2.81 20 .12 3.04 3.06 2.68 1.93 74.0 1.5 383.0 2.36 4.40 3.17 3.19 2.87 2.36 7. .44 2.63 2.30 2.20 2.20 336.0 1.5 394.0 2.97 2.96 2.82 2.60 2.78 2.60 27	.06 2.37 2.83 3.23 2.37 206.0 1.5 371.0 3.64 3.55 2.81 3.08 3.44 2.81 206.12 3.04 3.05 2.81 3.08 3.44 2.81 206.12 3.04 3.04 3.05 2.68 1.93 74.0 1.5 383.0 2.36 4.40 3.17 3.19 2.87 2.36 74.24 2.63 2.30 2.20 2.20 336.0 1.5 394.0 2.97 2.96 2.82 2.60 2.78 2.60 2.70.36 5.28 4.82 4.82 4.36 140.0 1.5 403.0 4.95 4.89 5.97 5.92 5.45 4.89 140.	.06 2.37 2.83 3.23 2.37 206.0 1.5 371.0 3.64 3.55 2.81 3.08 3.44 2.81 206.12 2.06 2.12 3.04 3.06 2.68 1.93 74.0 1.5 383.0 2.36 4.40 3.17 3.19 2.87 2.36 74.14 2.63 2.30 2.20 2.20 336.0 1.5 394.0 2.97 2.96 2.82 2.60 2.78 2.60 2.70 2.96 2.28 5.28 4.82 4.36 140.0 1.5 403.0 4.95 4.89 5.97 5.92 5.45 4.89 140.1 1.5 SEGMENT MINIMUM = 2.36 AT THE 383.0 INCH STATION	3.04 3.06 2.68 1.93 74.0 1	62.0 3	4 3.44 3.	8 3.79	.44 3.0	206.
.12 3.04 3.06 2.68 1.93 74.0 1.5 383.0 2.36 4.40 3.17 3.19 2.87 2.36 7 3.44 2.63 2.30 2.20 2.20 336.0 1.5 394.0 2.97 2.96 2.82 2.60 2.78 2.60 27	.12 3.04 3.06 2.68 1.93 74.0 1.5 383.0 2.36 4.40 3.17 3.19 2.87 2.36 74. .44 2.63 2.30 2.20 2.20 336.0 1.5 394.0 2.97 2.96 2.82 2.60 2.78 2.60 270. .36 5.28 5.28 4.82 4.36 140.0 1.5 403.0 4.95 4.89 5.97 5.92 5.45 4.89 140.	.12 3.04 3.06 2.68 1.93 74.0 1.5 383.0 2.36 4.40 3.17 3.19 2.87 2.36 74.34 2.63 2.30 2.20 2.20 336.0 1.5 394.0 2.97 2.96 2.82 2.60 2.78 2.60 270.36 5.28 5.28 4.82 4.36 140.0 1.5 403.0 4.95 4.89 5.97 5.92 5.45 4.89 140. = 1.93 AT THE 383.0 INCH STATION SEGMENT MINIMUM = 2.36 AT THE 383.0 INCH STATION	3.04 3.06 2.68 1.93 74.0 1.	71.0 3	4 3.55 2.	1 3.08	.44 2.8	206
.44 2.63 2.30 2.20 2.20 336.0 1.5 394.0 2.97 2.96 2.82 2.60 2.78 2.60 27	.44 2.63 2.30 2.20 2.20 336.0 1.5 394.0 2.97 2.96 2.82 2.60 2.78 2.60 270. .36 5.28 5.28 4.82 4.36 140.0 1.5 403.0 4.95 4.89 5.97 5.92 5.45 4.89 140.	.44 2.63 2.30 2.20 2.20 336.0 1.5 394.0 2.97 2.96 2.82 2.60 2.78 2.60 270. 36 5.28 5.28 4.82 4.36 140.0 1.5 403.0 4.95 4.89 5.97 5.92 5.45 4.89 140. = 1.93 AT THE 383.0 INCH STATION SEGMENT MINIMUM = 2.36 AT THE 383.0 INCH STATION	2 63 2 30 2 20 2,20 336,0 1,	83.0 2	6 4.40 3.	7 3.19	.87 2.3	74
	.36 5.28 5.28 4.82 4.36 140.0 1.5 403.0 4.95 4.89 5.97 5.92 5.45 4.89 140.	.36 5.28 5.28 4.82 4.36 140.0 1.5 403.0 4.95 4.89 5.97 5.92 5.45 4.89 140. = 1.93 AT THE 383.0 INCH STATION SEGMENT MINIMUM = 2.36 AT THE 383.0 INCH STATION		94.0 2	7 2.96 2.	2 2.60	.78 2.6	270
36 5.28 5.28 4.82 4.36 140.0 1.5 403.0 4.95 4.89 5.97 5.92 5.45 4.89 14		= 1.93 AT THE 383.0 INCH STATION SEGMENT MINIMUM = 2.36 AT THE 383.0 INCH S	5.28 5.28 4.82 4.36 140.0 1.	3.0 4	5 4.89 5	5.92	.45 4.8	140

66.4 66.4 66.4 66.4

SECONDS 122.9 TIME MOTOR ACTION

76.6

70.8

66.4 66.4 66.4 66.4 66.4 66.4 89.4

+ 3 SIGMA DESIGN CRITERIA Z INDICATES THE PRECEDING MDD HAS EXCEEDED THE

Vol. III TWR-17546

A

PREFIRE MEASUREMENTS	PART NO SERIAL	). 1U7666 NO. 0000	6-01 005			POSTF	IRE MEA INCHES	MEASUREMENT	v	ART NO. ERIAL NO	1U76650-04 - 0000003
LOCAT				STATIO	2	4 5 3 C	1.0				
.0 206.0 270.0	O MIN.	MEDIAN	MOT	(IN)	74.0	20.	0.90		36.0	MIN.	MEDIAN
3.5 2.548 2.512 2.487 2.454 2.49	0 2.45	. 49	. 12	•	.47	.47	.420	.342	39	.34	. 4 2
3.0 0.986 0.916 0.879 0.886 0.99	8 0.87	. 91	. 65	ω.	0.779	0.761	0.762 0	.800 0	. 748	0.748	. 76
7.0 0.590 0.594 0.585 0.610 0.63	0 0.58	. 59	. 45	7.	J	H		H		u	. 59
0.7 0.433 0.443 0.429 0.483 0.43	2 0.42	. 43	. 40	٥.	ŭ	u	u		u	<u>ب</u>	43
4.2 0.469 0.475 0.467 0.487 0.47	7 0.46	. 47	.38	•	J	13	ដ	J	J	u	47
7.7 0.378 0.393 0.366 0.372 0.37	5 0.36	. 37	. 33	7.	ដ	ב	בו	ы	i.	ם	.37
1.2 0.290 0.298 0.289 0.293 0.29	2 0.28	. 29	. 28	Ξ.	IJ	1	J	ב	u	ם	. 29
4.0 0.289 0.301 0.284 0.295 0.28	9 0.28	. 28	. 25	4	J	u	.1	'n	ы	ı	. 28
94.7 0.111 0.107 0.107 0.110 0.11	0 0.10	. 11	0.	4.	ı	u	J	ų	u	ħ	. 11
42.0 0.156 0.163 0.160 0.157 0.15	6 0.15	. 15	. 11	42.	ដ	u	J	נו	u	ני	. 15
45.7 0.264 0.260 0.260 0.262 0.26	1 0.26	. 26	. 23	45.	'n	u	7	Ļ	ı	د	. 26
48.5 0.298 0.324 0.319 0.308 0.32	7 0.29	. 31	. 27	48.	ដ	ם	IJ	J	ı	ı	.31
52.0 0.383 0.370 0.397 0.384 0.38	6 0.37	. 38	. 31	52.	. 400	.347	.354	. 418	•	4	. 35
02.0 0.888 0.821 0.787 0.799 0.78	9 0.78	. 79	. 54	62.	. 692	.700	99.	. 648	69.	64	. 69
73.3 0.742 0.732 0.845 0.733 0.75	0 0.73	. 74	9.	75.	. 622	.607	. 605	.611	. 59	. 59	.60
00.0 089.0 789.0 0.080.0 1/9.0 0.000	9 0 6	9.	. 64	87.	. 552	. 552	. 542	. 541	. 53	. 53	. 54
1/:0 TT/:0 01/:0 CT/:0 CT/:0 0:16	0 0.71	. 71	. 64	99	. 547	. 584	.571	. 539	9.	. 53	. 57
13.0 0.063.0.2/3.0.683.0.051.0.064.0.004.0.004.0.004.0.004.0.004.0.004.0.004.0.004.0.004.0.004.0.004.0.004.0.004.0.004.0.004.0.004.0.004.0.004.0	9 0 0	9 :	. 63	15.	. 567	. 547	. 531	503	. 53	. 50	. 53
7/'0 90/'0 TZ/'0 ZT/'0 67/'0 0'EZ	0/.0	7 .	9	24.	. 538	. 569	. 567	. 551	. 56	. 53	. 56
36.0 0.630 0.630 0.647 0.663 0.66	40.0	90.	20.	30.	. 499	. 516	. 515	495	. 50	. 49	. 50
20.0 C.63.0 C.63.0 C.64.5 C.64	79.0	. 63		36.	468	484	. 473	. 458	. 47	. 45	.47
19:0 169:0 159:0 070:0 670:0 0.01 24 0 0 670 0 618 0 608 0 605 0 61	10.0	70.		9.0	.467	499	6 8 6	.479	49	.46	. 48
63.0 0 610 0 608 0 602 0 508 0 50		10.	ָ הַ הַ	T (		4/4	.462	80 0	. 49	. 46	. 48
0 0.582 0.602 0.601 0.608 0.61	5 0.582	0.602	890.0	282.0	0.470	406.0	20.4.0	473 0	9.5	0.459	0.466
93.0 0.590 0.610 0.583 0.599 0.59	0 0.58	59	.54		444	481	.462	460	4.5	4 4	7 7
05.0 0.580 0.592 0.577 0.595 0.59	9 0.57	. 59	. 52	05.	. 411	.479	. 481	.429	4.3	41	4.
12.0 0.667 0.668 0.661 0.65. 0.64	7 0.64	99.	. 54	12.	. 544	. 565	. 598	. 542	. 51	. 51	5.4
21.0 0.993 0.996 1.626 1.010 0.96	96.0	.99	. 91	21.	.876	.837	.946	.887	.86	. 83	.87
39.0 0.570 0.579 0.585 0.602 0.56	3 0.56	. 57	. 55	39.	. 408	. 494	. 448	.439	. 4.8	. 40	. 44
50.0 0.540 0.537 0.534 0.527 0.53	4 0.52	. 53	. 52	50.	.391	.464	. 405	.455.	. 41	. 39	.41
62.0 0.571 0.578 0.598 0.534 0.56	0.53	. 57	. 52	62.	. 389	.410	. 404	.393	.39	. 38	. 39
71.0 0.583 0.604 0.615 0.566 0.55	0.55		. 52	71.	. 423	. 434	.396	.382	. 39	. 38	.39
83.0 0.626 0.546 0.532 0.532 0.54	8 0.53	. 54	. 51	83.	.361	.422	.364	.365	.35	.35	.36
94.0 0.559 0.510 0.539 0.570 0.63	0.53	. 57	. 50	94.	.368	. 404	. 348	.351	.40	.34	36
03.0 1.0/0 1.06/ 1.0/4 1.065 1.07	1.06	.07	9.	03.	. 854	. 849	894	. 885	.87	. 84	.87

AN " L " INDICATES THAT LINER MATERIAL WAS REMAINING AT THAT LOCATION. THE MEDIAN AND MINIMUM VALUES WERE CALCULATED USING THE PREFIRE THICKNESSES AT THE LOCATIONS WHERE LINER MATERIAL WAS REMAINING

TWR-17546 Vol. III Page 126

A P P E N D I X A

Table A-1 RSRM-7A Aft Dome Factory Joint Weatherseal Evaluation

Motor No	.: RSRM-7A	Date:	26 November	r 1989				
Assessment Engineer(s): S. Hicken, T. Morgan								
Factory	Joint Weatherseal Observat	ions:						Comment Numbers
A.	Charred/Heat Affected Mate	erial (HTA	FF)?	X	yes		no	1
В.	Insulation Damage/Missing Due to Reentry/Debris/Wate				yes	<u> </u>	no	
C.	Insulation Damage/Missing Reentry/Debris/Water Impa			<del></del>	yes	<u> </u>	no	
D.	Insulation to Case Unbond	s (DEBND)?			yes	<u> </u>	no	
Е.	Evidence of Water Leakage Joint (WATER)?	From Fact	ory		yes	<u> </u>	no	

## Notes/Comments:

1. Normal heat effects in 270° region.

Table A-2 RSRM-7A Aft Segment Stiffener to Stiffener Factory Joint Weatherseal Evaluation

Motor No.: RSRM-7A	Date: 26 Novembe	r 1989				
Assessment Engineer(s): S. Hicken	, T. Morgan	<u> </u>				
Factory Joint Weatherseal Observat	ions:					Comment Numbers
A. Charred/Heat Affected Mat	erial (HTAFF)?	<u> </u>	yes		no	1
B. Insulation Damage/Missing Due to Reentry/Debris/Wat			yes	<u> </u>	no	
C. Insulation Damage/Missing Reentry/Debris/Water Impa			yes	<u> </u>	no	
D. Insulation to Case Unbond	s (DEEND)?	<u> </u>	yes		no	2
E. Evidence of Water Leakage Joint (WATER)?	From Factory		yes	X	no	

- 1. Minor heat effects on the orbiter side (270°) like normal.
- 2. Unbond intermittent full circumference on aft edge. Depth 0.8 in. to 0.9 in. typical approx. 70% of circumference. Adhesive failure at 205 to case.

Table A-3 RSRM-7A Aft Segment ET Attach to Stiffener Factory Joint Weatherseal Evaluation

Motor No.:	RSRM-7A	Date: 26 Novem	nber 1989				
Assessment E	ngineer(s): S. Hicken	T. Morgan					
Factory Join	it Weatherseal Observat	ions:					Comment Numbers
A. Cha	rred/Heat Affected Mate	erial (HTAFF)?	<u> </u>	yes		no	1
	ulation Damage/Missing to Reentry/Debris/Wate			yes	<u> </u>	no	
	ulation Damage/Missing ntry/Debris/Water Impa	the state of the s		yes	<u> </u>	no	
D. Ins	rulation to Case Unbond	s (DEEND)?		yes	X	no	
	dence of Water Leakage nt (WATER)?	From Factory		yes	<u> </u>	no	

1. Normal heat effects in 270° region.

Table A-4
RSRM-7A Aft Center Segment Factory Joint Weatherseal Evaluation

Motor No	otor No.: RSRM-7A Date: 26 November 1989							
Assessme	nt Engineer(s): S. Hick	en, T. Morgan						
Factory	Joint Weatherseal Observ	ations:					Comment Numbers	
Α.	Charred/Heat Affected N	aterial (HTAFF)?		yes	<u> </u>	no		
В.	Insulation Damage/Missi Due to Reentry/Debris/V			yes	<u> </u>	no		
c.	Insulation Damage/Missi Reentry/Debris/Water In			yes	<u> </u>	no		
D.	Insulation to Case Unbo	onds (DEBND)?	<del></del>	yes	<u> </u>	no		
E.	Evidence of Water Leaka Joint (WATER)?	age From Factory		yes	<u> </u>	no		

Table A-5 RSRM-7A Forward Center Segment Factory Joint Weatherseal Evaluation

Motor No.: RSRM-7A	Date: 26 November 1989	
Assessment Engineer(s): S. Hicken	, T. Morgan	
Factory Joint Weatherseal Observat	ions:	Comment Numbers
A. Charred/Heat Affected Mat	erial (HTAFF)? yes <u>X</u> no	
B. Insulation Damage/Missing Due to Reentry/Debris/Wat		
C. Insulation Damage/Missing Reentry/Debris/Water Impa		
D. Insulation to Case Unbond	ds (DEBND)? yesX no	
E. Evidence of Water Leakage Joint (WATER)?	From Factory yesXno	

Table A-6 RSRM-7A Forward Segment Cylinder to Cylinder Factory Joint Weatherseal Evaluation

Motor No.: RSRM-7A	Date: 26 November 1989				
Assessment Engineer(s): S. Hicken	, T. Morgan				
Factory Joint Weatherseal Observat	ions:				Comment Numbers
A. Charred/Heat Affected Mate	erial (HTAFF)?	yes	<u> </u>	no	
B. Insulation Damage/Missing Due to Reentry/Debris/Wate		yes	<u> </u>	no	
C. Insulation Damage/Missing Reentry/Debris/Water Impa		yes	<u> </u>	no	
D. Insulation to Case Unbond	s (DEEND)?	yes	<u> </u>	no	
E. Evidence of Water Leakage Joint (WATER)?	From Factory	yes	<u> </u>	no	

Table A-7
RSRM-7A Forward Dome Factory Joint Weatherseal Evaluation

Motor No.: RSRM-7A	Date: 26 November	er 1989				•
Assessment Engineer(s): S. Hicke	n, T. Morgan					
Factory Joint Weatherseal Observa	tions:					Comment Numbers
A. Charred/Heat Affected Ma	terial (HTAFF)?		yes	<u> </u>	no	
B. Insulation Damage/Missir Due to Reentry/Debris/Wa		<del></del>	yes	<u> </u>	no	
C. Insulation Damage/Missir Reentry/Debris/Water Imp			yes	<u> </u>	no	
D. Insulation to Case Unbor	ds (DEBND)?	<del></del>	yes	<u> </u>	no	****
E. Evidence of Water Leakag Joint (WATER)?	ge From Factory		yes	<u> </u>	no	

Table A-8
RSRM-7A Aft Stiffener Ring TPS Evaluation

Motor No.:	RSRM-7A Date: 26 November 1989							
Assessment	Engineer(s): S. Hicken,	T. Morgan						
St <b>iffene</b> r F	Ring/Stiffener Stub Insul	ation Observations:					Comment Numbers	
A. Cr	narred/Heat Affected Mate	rial (HTAFF)?	<u> </u>	yes		no	1	
	nsulation Damage/Missing De to Reentry/Debris/Wate			yes	<u> </u>	no		
	nsulation Damage/Missing eentry/Debris/Water Impac			yes	<u> </u>	no		
	nsulation to Stiffener Ri tub Unbonds (DEEND)?	ng/Stiffener		yes	<u> </u>	no		

Notes/Comments:

1. Normal heat effects in 270° region.

## Table A-9 RSRM-7A Center Stiffener Ring TPS Evaluation

Motor No.: RSRM-7A	Date: 26 Novembe	r 1989				
Assessment Engineer(s): S. Hicker	, T. Morgan					
Stiffener Ring/Stiffener Stub Inst	lation Observations:					Comment Numbers
A. Charred/Heat Affected Mar	erial (HTAFF)?	<u> </u>	yes		no	1
B. Insulation Damage/Missing Due to Reentry/Debris/Wa			yes	<u> </u>	no	
C. Insulation Damage/Missing Reentry/Debris/Water Impa			yes	<u> </u>	no	
D. Insulation to Stiffener I Stub Unbonds (DEBND)?	ling/Stiffener		yes	<u> </u>	no	

#### Notes/Comments:

1. Normal heat effects in 270° region. Heat effect blisters on outboard face at 270°.

Table A-10 RSRM-7A Forward Stiffener Ring TPS Evaluation

Motor No	Date: 26 November 1989						
Assessme	ent Engineer(s): S. Hic	ken, T. Morgan					
Stiffene	er Ring/Stiffener Stub I	nsulation Observations:					Comment Numbers
Α.	Charred/Heat Affected	faterial (HTAFF)?	<u> </u>	yes		no	1
В.	Insulation Damage/Miss Due to Reentry/Debris/			yes	X_	no	
C.	Insulation Damage/Miss Reentry/Debris/Water I		<u>.                                    </u>	yes	<u> </u>	no	
D.	Insulation to Stiffene Stub Unbonds (DEEND)?	r Ring/Stiffener		yes	<u> </u>	no	

#### Notes/Comments:

1. Normal heat effects in 270° region.

## Table A-11 RSRM-7A Forward Stiffener Stub TPS Evaluation

Motor No.: RSRM-7A	Date: 26 Novembe	r 1989				
Assessment Engineer(s): S. Hi	cken, T. Morgan					
Stiffener Ring/Stiffener Stub	Insulation Observations:					Comment Numbers
A. Charred/Heat Affected	Material (HTAFF)?	<u> </u>	yes		no	1
B. Insulation Damage/Miss Due to Reentry/Debris	sing Material Not /Water Impact (TPSVD)?		yes	<u> </u>	no	
C. Insulation Damage/Mis Reentry/Debris/Water		·	. yes .	<u> </u>	no	
D. Insulation to Stiffen Stub Unbonds (DEEND)?		<del></del>	yes	<u> </u>	no	

- 1. Normal heat effects in 270° region.
- 2. K5NA repair of outboard edge of insulation is flaking off intermittently around the circumference.

### Table A-12 RSRM-7A Nozzle to Case Joint Insulation Evaluation

Notor No.: RSRM-7A	Date: 1 December 19	89			
Assessment Engineer(s): J. Passma	n, S. Hicken				
Nozzle to Case Joint Observations:					Comment Jumbers
A. Gas Penetration in Polysulfic		yes	<u>X</u> no		
B. Foreign Material in Polysulf	ide (FMIJ)?	yes	X no		
C. Voids in Polysulfide (VOID)?	, –	X yes	no		$\frac{1}{2}$
<ul><li>D. Polysulfide Porosity (PSPOR)</li><li>E. Polysulfide Extrusion Past W</li></ul>		X yes	X no		
E. Polysulfide Extrusion Past W F. Polysulfide Failure Mode?	15 % Adhesive			nesive (CRAI	OH)
ozzle to Case Joint Insulation Pa	rt Observations:				
G. Aft Dome Edge Unbonds (DBOND	)?	yes	X no		
H. Baffle Torn (DBAFL)?	·	yes	X no		
ecord Aft Dome End Nozzle to Case	Joint Insulation Measur	ements:			
		Degree	Depth	Depth	Depth
1,		ocation	(1)*	(2)**	<u>(3)***</u>
3					5 70 .
		00	6.95 in.	$\frac{6.00 \text{ in.}}{6.00 \text{ in.}}$	$\frac{5.78 \text{ in.}}{5.00 \text{ in}}$
		90°	7.30 in.	6.40 in. 6.25 in.	5.90 in. 5.95 in.
		180° 270°	7.30 in. 7.35 in.	$\frac{6.25 \text{ in.}}{6.35 \text{ in.}}$	5.85 in.
		210	7.00 111.	<u> </u>	<u> </u>
V THE	Max				
Territor.	Min				
	_				
Depth (1) is to be measured f					
Depth (2) is to be measured f	rom the aft face of the	aft dome to 1	the inboard ed	ge or the ho	eat :

#### Notes/Comments:

1. Void in polysulfide at  $109^{\circ}$  (1.60 in. axial length 0.25 in. wide) extending across step. No sooting present within void.

\*\*\* Depth (3) is to be measured from the aft face of the aft dome to the outboard edge of the heat

2. Porosity noted on step full circumference.

affected polysulfide

affected polysulfide

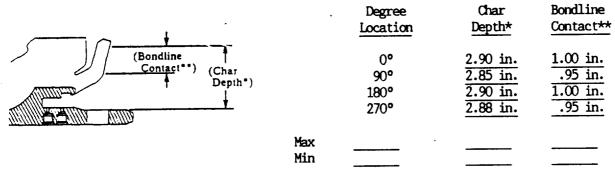
Table A-13 RSRM-7A Nozzle to Case Joint Vent Slot Fill

ssessment Engineer(s): J. Passman, S. Hicken								
Degree Location	% Slot Fill	Degree Location	% Slot Fill	Degree Location	% Slot Fill			
0.00	100	122.4°	5	244.8°	10			
7.2°	100	129.6°	Ò	252.0°	20			
14.40	80	136.8°	10	259.2°	40			
21.6°	60	144.0°	5	266.4°	0			
28.8°	70	151.2°	0	273.6°	30			
36.0°	80	158.4°	20	280.8°	20			
43.2°	0	165.6°	10	288.0°	20			
50.4°	50	172.8°	20	295.2°	20			
57.6°	50 .	180.0°	10	302.4°	20			
64.8°	20	187.2°	5	309.6°	80			
72.0°	30	194.4°	10	316.8°	100			
79.2°	20	202.6°	30	324.0°	100			
86.4°	10	208.8°	30	331.2°	80			
93.6°	40	216.0°	40	338.4°	90			
100.8°		223.2°	3	345.6°	100			
108.0°	5	230.4°	10	352.8°	90			
115.2°	5 5 5	237.6°	10	•				

### Table A-14 RSRM-7A Aft Field Joint Insulation Evaluation

Motor No.: RSRM-7A	Date: 1 December 1989	
Assessment Engineer(s): S. Hicken,	J. Passman, D. Bartelt	
Field Joint Insulation Joint Observ	vations:	Comment Numbers
A. Gas Penetration (TBH, PGPTH)? B. Foreign Material (FMIJ)? C. Areas of J-leg Non-contact (ED. Wet Soot (SOOT)?	yes X no	2
Field Joint Insulation Part Observa	ations:	
E. Clevis Edge Unbonds > 0.10 ir F. Clevis Insulation Crack/Carzi		3

#### Record Tang End Field Joint Insulation Measurements:



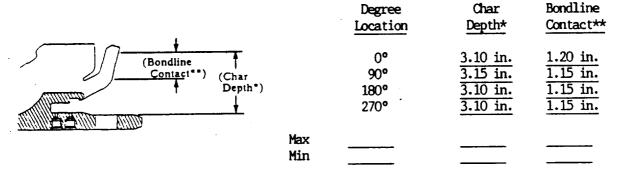
- \* Char depth is to be measured from the inner diameter of the tang leg to the outbard edge of the char layer.
- \*\* Bondline contact is to be measured from the outboard edge of the char layer to the outboard extent of contact.

- 1. Clevis edge separation repair adhesive residue on clevis insulation at 245°.
- 2. Wet sooting present intermittent full circumference approximately 0.30 in. .40 in. (Unable to verify due to large amounts of grease on tang insulation)
- 3. Cracks/crazing present on clevis insulation radius region at 310°, 140°, 82°, and 38°.

Table A-15
RSRM-7A Center Field Joint Insulation Evaluation

Motor No.: RSRM-7A	Date: 1 Decemb	er 1989				
Assessment Engineer(s): S. Hid	eken, J. Passman, D. Ba	rtelt				
Field Joint Insulation Joint O	oservations:					Comment Numbers
A. Gas Penetration (TBH, PGB. Foreign Material (FMIJ)? C. Areas of J-leg Non-contact D. Wet Soot (SOOT)?		<u> </u>	yes yes yes	X X X	no no no	1 2
Field Joint Insulation Part Ob	servations:					
E. Clevis Edge Unbonds > 0.3 F. Clevis Insulation Crack/			yes yes	<u> </u>	no no	3

#### Record Tang End Field Joint Insulation Measurements:



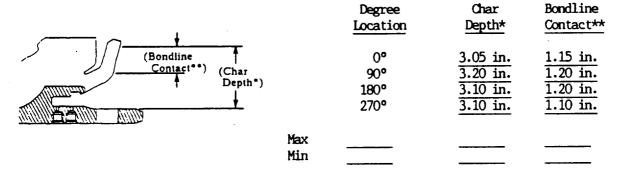
- \* Char depth is to be measured from the inner diameter of the tang leg to the outbard edge of the char layer.
- \*\* Bondline contact is to be measured from the outboard edge of the char layer to the outboard extent of contact.

- 1. Masking tape residue on clevis leg insulation.
- 2. Wet sooting into joint 0.30 in. 0.70 in. full circumference.
- 3. Crazing was to be at 158° (not detectable).

### Table A-16 RSRM-7A Forward Field Joint Insulation Evaluation

Motor No.: RSRM-7A	Date: 1 December 1989		
Assessment Engineer(s): S. Hicken,	J. Passman, D. Bartelt		
A. Gas Penetration (TBH, PGPTH)? B. Foreign Material (FMIJ)? C. Areas of J-leg Non-contact (BD). Wet Soot (SOOT)?	yes yes	s X no s X no	Comment Numbers
Field Joint Insulation Part Observa	tions:		
E. Clevis Edge Unbonds > 0.10 in F. Clevis Insulation Crack/Carzin		<del></del>	

#### Record Tang End Field Joint Insulation Measurements:



- \* Char depth is to be measured from the inner diameter of the tang leg to the outbard edge of the char layer.
- \*\* Bondline contact is to be measured from the outboard edge of the char layer to the outboard extent of contact.

- 1. 0.30 in. 0.60 in. deep full circumference.
- 2. Intermittent tang edge unbonds visible.

## Table A-17 RSRM-7A Igniter Boss Insulation Evaluation

Motor No.: RSRM-7A	Date: 30 November 1989				
Assessment Engineer(s): S. Hicken	, J. Passman				
A. Abnormal Insulation Erosion B. Tears, Gouges, or Cuts (TEAR) C. Ply Separations or Delaminati D. Blistering (BLSPT)? E. Insulation Flashing (FLASH)? F. Edge Unbonds (DBOND)?	(INSER)? S)? ions (PLYSP)?	yes _ yes _ yes _ yes _ yes _	х х х х	no no no no no no	Comment Numbers

#### Notes/Comments:

1. Small amount of loose flashing near 60° (1 in. circumference).

## Table A-18 RSRM-7A Igniter Chamber Insulation Evaluation

otor No.: RSRM-7A	Date: 30 Novemb	per 1989			
ssessment Engineer(s): S.	Hicken, J. Passman				
gniter Chamber/Igniter Boss	s Insulation Observations:				Comment
gniter Chamber/Igniter Boss	s Insulation Observations:				Comment Numbers
gniter Chamber/Igniter Boss  A. Abnormal Insulation E		ye	es X	no	•••••
	rosion (INSER)?		es X	no no	•••••
A. Abnormal Insulation E	rosion (INSER)? s (TEARS)?	ye			••••••

## Table A-19 RSRM-7A Igniter Adapter to Forward Dome Putty Evaluation

Motor No.: RSRM-7A	Date: 30 November 1989	
Assessment Engineer(s): S. Hicker	n, J. Passman	·
Igniter Putty Condition  1. Color? 2. Tack?	Variable X Constant Good X Nominal	Poor
Igniter Putty Observations:  A. Gas Penetration in Putty ('B. Foreign Material in Putty C. Voids in Putty (VOID)?  D. Putty Failure Mode	(FMLJ)? yes yes	Comment Numbers  no 1  X no X no 100 % Cohesive (CRADH)
Record the following if any of the  Degree Condition Start (Observation Location Code) (deg.) PCPIH 332	above conditions exist:  Degree Stop Location (deg.) 332 0.20 at fwd edge 1.15 at aft edge	

#### Notes/Comments:

1. Blowhole through the putty with gas to the seal at  $332^{\circ}$ .

# $\begin{array}{c} \text{Table A--20} \\ \text{RSRM--7A Igniter Adapter to Igniter Chamber Putty Evaluation} \end{array}$

Motor No.: RSRM-7A	Date: 30 November 1989	
Assessment Engineer(s): S. Hicken	, J. Passman	
Igniter Putty Condition  1. Color? 2. Tack? X	VariableX	
Igniter Putty Observations:  A. Gas Penetration in Putty ( B. Foreign Material in Putty C. Voids in Putty (VOID)? D. Putty Failure Mode	(FMIJ)? yes X no yes X no O X Adhesve (AFJFM) 100 % Cohesive (CRADH)	
Record the following if any of the  Degree Condition Start (Observation Code) (deg.)	above conditions exist:  Degree Stop Location Circumferential Axial Radial (deg.) Width (in.) Length (in.) Depth (in.	)

## Table A-21 RSRM-7A Aft Segment Internal Insulation Evaluation

Motor No.: RSRM-7A	Date: 1 December 1989				
Assessment Engineer(s): J. Passme	n, S. Hicken				
Segment Internal Insulation Observ	ations:				Comment Numbers
A. Abnormal Insulation Erosi	on (INSER)?	yes	X	no	
B. Tears, Gouges, or Cuts (1	EARS)?	yes	X	no	
C. Ply Separations or Delami	nations (PLYSP)?	yes	<u> </u>	no	
<pre>D. Blistering (BLSPT)?</pre>	<u> </u>	yes		no	1
E. Abnormal Liner Pattern (A	BLNR)?	yes	X	no	2
F. NBR Under CF/EPDM Exposed	(INSER)?	yes		no	3

- A small amount of (open and unopen) blistering in the CF/EPDM was present intermittent.
   Approximate number is 4-6. Worst case near 300° (1.75 in. long x 0.25 in. wide) and it was open. All blisters were located in a region approx. 6-9 in. (surface measurement) forward of remaining aft dome NBR insulation. No abnormal erosion occurred to the blisters or surrounding area.
- 2. Liner was not present, which is normal.
- NER was exposed under the CF/EPDM intermittent just aft of the remaining CF/EPDM to NER interface approx. 18-23 in. forward of boss. This is normal condition in this region.

### Table A-22 RSRM-7A Aft Segment NBR Inhibitor Height Evaluation

otor No.: RSRM-7A	Date: 1 Dece	ember 1989			
ssessment Engineer(s)	: S. Hicken, J. Passman, D.	Bartelt			
BR Inhibitor Observat	ions (Other Than Tears):				omment umbers
	or Separations (PLYSP)? normal Erosion (INSER)?	yes yes	<del></del>	no	
ecord NBR Inhibitor M	leasurements:				
ecord NER Inhibitor M	easurements:  Radial Distance	Degree Locat	ion	Radial Dis	stance
Degree Location	Radial Distance	Degree Locat	<u>ion</u>	Radial Dis	
Degree Location	Radial Distance 4.5 in.		ion		in.
Degree Location  0° 30°	Radial Distance	180°	<u>ion</u>	7.75 : 7.5	in.
Degree Location  0° 30° 60°	Radial Distance  4.5 in.  4.5 in.  5.0 in.	180° 210°	<u>ion</u>	7.75 : 7.5 : 8.5 :	in.
Degree Location  0° 30°	Radial Distance  4.5 in.  4.5 in.  5.0 in.	180° 210° 240°	ion	7.75 : 7.5 : 8.5 : 4.5 :	in. in. in.

Notes/Comments:

Max. inhibitor height =
Min. inhibitor height =

Table A-23 RSRM-7A Aft Segment NBR Inhibitor Tear Evaluation

•	
Motor No.: RSRM-7A	Date: 1 December 1989
Assessment Engineer(s): S. Hicken, J.	. Passman, D. Bartelt
NBR Inhibitor Description	Comment Numbers
A. Radial Tears > 3 in. Long (TEARS) B. Circumferential tears? C. Tears exhibiting charring or eros	? yesX no
Record NER Inhibitor Tear Measurements	s (if applicable, for radial tears > 3 in. long or circ. tears):
begree Location Meas. "A"*	Meas. "B"* Comments (Charring, etc.)
	180°

## Table A-24 RSRM-7A Aft Center Segment Internal Insulation Evaluation

tor No	: RSRM-7A	Date: 1 December	1989				
Sessin	nt Engineer(s): J. Passman	·					
<b></b>							<b>Q</b>
gment	Internal Insulation Observati	ons:					Comment Numbers
		···		yes	X	no	
Α.	Abnormal Insulation Erosion	(INSER)?		yes yes	<u> </u>	no no	
A. B.	Abnormal Insulation Erosion Tears, Gouges, or Cuts (TEAR	(INSER)? (S)?		•	X X	<del>-</del>	
A. B. C.	Abnormal Insulation Erosion	(INSER)? (S)?		yes	X X X	no	• • • • • • • • • • • • • • • • • • • •

#### Notes/Comments:

1. Liner present in normal condition 1-2 ft. forward of factory joint to NER inhibitor.

Table A-25
RSRM-7A Aft Center Segment NBR Inhibitor Height Evaluation

Motor No.: RSRM-7A	Date: 1 December	er 1989	
Assessment Engineer(s):	S. Hicken, J. Passman, D. Bar	rtelt	
A. Delaminations	or Separations (PLYSP)?	yesX yesX	Comment Numbers no 1
Record NBR Inhibitor Me	easurements: Radial Distance	Degree Location	Radial Distance
0° 30° 60° 90° 120° 150°	12.0 in. 13.0 in. 13.0 in. 11.5 in. 13.5 in. 12.0 in.	180° 210° 240° 270° 300° 330°	13.5 in. 13.0 in. 12.5 in. 14.5 in. 14.5 in. 12.5 in.
Max. inhibitor h Min. inhibitor h	<del>-</del>		

#### Notes/Comments:

1. Missing chunks of inhibitor on inboard edge due to splashdown impact (See Figure on Table A-26).

### Table A-26 RSRM-7A Aft Center Segment NBR Inhibitor Tear Evaluation

Motor No.: RSRM-7A	Date: 1 December 1989					
Assessment Engineer(s): S. Hicken, J. Passman, D. Bartelt						
NER Inhibitor Description  A. Radial Tears > 3 in. Long (TEARS)?  B. Circumferential tears?  C. Tears exhibiting charring or erosi	yes X no					
Record NBR Inhibitor Tear Measurements	s (if applicable, for radial tears > 3 in. long or circ. tears):					
begree Location Meas. "A"*	Meas. "B"*  Comments (Charring, etc.)  asured  90°					
Bernand	0°					

Notes/Comments:

270\*

## Table A-27 RSRM-7A Aft Center Segment Stress Relief Flap Evaluation

Motor No.: RSRM-7A	Date: 1 December 1989
Assessment Engineer(s): S. Hicken	, J. Passman, D. Bartelt
A. Abnormal CF/EPDM or NER Eros: B. Tears Gouges, or Cuts (TEARS) C. Ply Separations, Delamination D. Abnormal/Unusual Missing Mate E. Castable Inhibitor Present?	Numbers
Max. Missing (If Appl.) Min. Missing (If Appl.)	Axial Distance  15.5 in.  90°  15.5 in.  15.5 in.  15.5 in.  15.5 in.  15.5 in.
* Axial distance is to be meant "A" is to be to	ment "A"** Measurement "B"*** Comments (Charring, etc.)  assured from the tip of the tang to the aft edge of the flap.  asken from the aft edge of the flap.  aken from the aft edge of the flap.

#### Notes/Comments

1. Flap is eroded uniformly to flap bulb full circumference.

# Table A-28 RSRM-7A Forward Center Segment Internal Insulation Evaluation

tor No	.: RSRM-7A	Date: 1 December	r 1989				
Sessine	nt Engineer(s): J. Passman	1					
							G
gment	Internal Insulation Observa	ations:					Comment Numbers
<del></del>	,			yes	<u> </u>	no	•••••
A. B.	Abnormal Insulation Erosic Tears, Gouges, or Cuts (T	on (INSER)? EARS)?		yes	<u> </u>	no	•••••
A. B.	Abnormal Insulation Erosic Tears, Gouges, or Cuts (T	on (INSER)? EARS)?		yes yes	X X X	no no	•••••
A. B. C. D.	Abnormal Insulation Erosic	on (INSER)? EARS)? nations (PLYSP)?		yes	X X X	no	•••••

#### Notes/Comments:

1. Liner present in normal condition forward of factory joint to NBR inhibitor.

Table A-29
RSRM-7A Forward Center Segment NBR Inhibitor Height Evaluation

Motor No.: RSRM-7A	Date: 1 Decembe	er 1989	
Assessment Engineer(s):	S. Hicken, J. Passman, D. Bar	telt	
NBR Inhibitor Observation  A. Delaminations of B. Severe or Abnormalian	ons (Other Than Tears): or Separations (PLYSP)? rmal Erosion (INSER)?	yesX yesX	Comment Numbers no no
Record NER Inhibitor Me	asurements:		
Degree Location	Radial Distance	Degree Location	Radial Distance
0° 30° 60° 90° 120° 150°	24.5 in. 25.0 in. 26.5 in. 27.5 in. 26.25 in. 26.75 in.	180° 210° 240° 270° 300° 330°	25.25 in. 25.5 in. 24.5 in. 23.75 in. 24.0 in. 25.0 in.
Max. inhibitor he Min. inhibitor he			

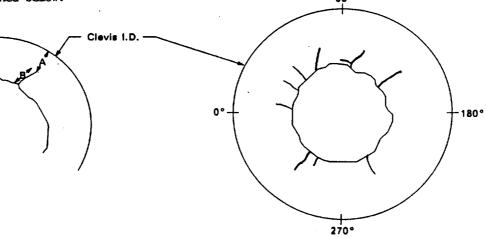
Table A-30
RSRM-7A Forward Center Segment NBR Inhibitor Tear Evaluation

Motor No.: RSRM-7A	Date: 1 December 1989	
Assessment Engineer(s): S. Hicken, J.	Passman, D. Bartelt	
NBR Inhibitor Description		Comment Numbers
<ul><li>A. Radial Tears &gt; 3 in. Long (TEARS)?</li><li>B. Circumferential tears?</li><li>C. Tears exhibiting charring or erosi</li></ul>	yes X no	See Below

### Record NBR Inhibitor Tear Measurements (if applicable, for radial tears > 3 in. long or circ. tears):

Degree Location	Meas. "A"*	Meas. "B"*	Comments (Charring, etc.)
10	14.5 in.	7.5 in.	
40	19.0 in.	5.5 in.	
70	18.5 in.	6.5 in.	
87	17.5 in.	8.5 in.	
104	20.0 in.	6.0 in.	
128	14.75 in.	10.5 in.	
244	12.5 in.	11.75 in.	
301	18.0 in.	5.0 in.	
327	15.5 in.	9.0 in.	

\* Measurements "A" and "B" are to measured as shown and sketched below.



#### Table A-31 RSRM-7A Forward Center Segment Stress Relief Flap Evaluation

Motor No.: RSRM-7A	Date: 1 December 1989		
Assessment Engineer(s): S. Hicken	, J. Passman, D. Bartelt		
A. Abnormal CF/EPDM or NER Eros: B. Tears Gouges, or Cuts (TEARS) C. Ply Separations, Delamination D. Abnormal/Unusual Missing Mate E. Castable Inhibitor Present?	ion (INSER)? )? ns, or Voids (PLYSP)?	yes X n	0
Record Stress Relief Flap Measure	ments:		
11 2 Max. Missing (If Appl.)	e Location Axial Dist  0° 10.5 i  90° 10.5 i  80° 11.5 i  70° 11.5 i  6.5 i	n. n. n.	
Record Stress Relief Flap Tear Mea	-		(7)
* Axial distance is to be me  ** Measurement "A" is to be t	asured from the tip of the ta aken from the aft edge of the	ng to the aft edge of	the flap.

#### Notes/Comments:

1. Blistcus noted in carbon fiber EPDM (54°-80°) ( 4 in. - 9 in. axially forward of tang).

Table A-32 RSRM-7A Forward Segment Internal Insulation Evaluation

Motor No.: RSRM-7A	Date: 1 December 1989	
Assessment Engineer(s): J. Passmar		
Segment Internal Insulation Observa	ations:	Comment Numbers
A. Abnormal Insulation Erosic B. Tears, Gouges, or Cuts (TI C. Ply Separations or Delamin D. Blistering (BLSPT)? E. Abnormal Liner Pattern (Al	ARS)? yes X no yes X no yes X no	1

1. Eleven star liner pattern evident just aft of cylinder to cylinder factory joint.

### Table A-33 RSRM-7A Forward Segment Stress Relief Flap Evaluation

Motor No.: RSRM-7A	Date: 1 December 1989	
Assessment Engineer(s): S. Hicken	J. Passman, D. Bartelt	
A. Abnormal CF/EPDM or NBR Eros: B. Tears Gouges, or Cuts (TEARS) C. Ply Separations, Delamination D. Abnormal/Unusual Missing Mate E. Castable Inhibitor Present?	ion (INSER)?  ?  ns, or Voids (PLYSP)?	yes X no
Record Stress Relief Flap Measure		
1	## Location	<del></del>
Record Stress Relief Flap Tear Mea	surements (If Applicable):	
	ment "A"** Measurement "B	
** Measurement "A" is to be t	asured from the tip of the tang aken from the tip of the tang t aken from the aft edge of the f	to the aft edge of the flap. to the aft edge of the flap. That to the forward edge of the tear.

### PHOTOGRAPHS SORTED BY: SEGMENT, PHOTO CODE, JOINT, SEGMENT END, NEGATIVE # FOR RSRM-7A

eg Ber	PHOTO CODE	Segment	JOINT	SEGMENT END	DEG LOC	COMMENT
o Housi	NG					
99-01	00	FXD HOUSING	N/A	N/A	0	NOZZLE OVERALL
99-02	00	FXD HOUSING	N/A	N/A	45	NOZZLE OVERALL
99-03	00	FXD HOUSING	N/A	N/A	90	NOZZIE OVERALL
99-04	00	FXD HOUSING	N/A	N/A	135	NOZZLE OVERALL
99-05	00	FXD HOUSING	N/A	N/A	180	NOZZLE OVERALL ·
99-06	00	FXD HOUSING	N/A	N/A	225	NOZZLE OVERALL
99-07	00	FXD HOUSING	N/A	N/A	270	NOZZLE OVERALL
99-08	00	FXD HOUSING	N/A	N/A	315	NOZZLE OVERALL
99-09	00	FXD HOUSING	N/A	N/A	187	FIXED HOUSING INSULATION FORWARD TIP W/O AND SLAG
99–10	00	FXD HOUSING	N/A	N/A	284	FIXED HOUSING INSULATION FORWARD TIP W/O AND SLAG
01-01	00	FXD HOUSING	N/A	N/A	0	NOZZLE OVERALL
01-02	00	FXD HOUSING	N/A	N/A	90	NOZZLE OVERALL
01-03	00	FXD HOUSING	N/A	N/A	180	NOZZLE OVERALL
01-04	00	FXD HOUSING	N/A	N/A	270	NOZZLE OVERALL
T SEG						
97-03	33	AFT SEG	NOZZLE/CASE JNT	AFT DOME	240-0	NOZZLE BOSS, AFT DOME, AND CYLINDER REGION
197-02	32	AFT SEG	NOZZLE/CASE JNT	AFT DOME	120-240	NOZZLE BOSS, AFT DOME, AND CYLINDER REGION
197-01	31	AFT SEG	NOZZLE/CASE JNT	AFT DOME	0-120	NOZZLE BOSS, AFT DOME, AND CYLINDER REGION
193-04	25	AFT SEG	AFT FIELD JNT	CLEVIS	240-0	CLEVIS, NBR INHIBITOR, AND CYLINDER REGION
193-03	24	AFT SEG	AFT FIELD JNT	CLEVIS	120-240	CLEVIS, NBR INHIBITOR, AND CYLINDER REGION
193-02	23	AFT SEG	AFT FIELD JNT	CLEVIS	0-120	CLEVIS, NBR INHIBITOR, AND CYLINDER REGION
493-01	22	AFT SEG	AFT FIELD JNT	CLEVIS	360	INTERNAL INSULATION, NBR INHIBITOR, AND CYLINDER REGION
493-08	21	AFT SEG	AFT FIELD JNT	TANG	240-0	FLAP, CYLINDER REGION, AND TANG
493-07	20	AFT SEG	AFT FIELD JNT	TANG	120-240	FLAP, CYLINDER REGION, AND TANG
493-06	19	AFT SEG	AFT FIELD JNT	TANG	0-120	FLAP, CYLINDER REGION, AND TANG
493-05	18	AFT SEG	AFT FIELD JNT	TANG	360	FLAP, CYLINDER REGION, AND TANG
470-01	00	AFT SEG	STIFF/STIFF FACT JNT	N/A	270	WEATHERSEAL UNBOND
470-02	00	AFT SEG	STIFF/STIFF FACT JNT	N/A	270	WEATHERSEAL UNBOND
511-02	00	AFT SEG	STIFF/STIFF FACT JNT	N/A	270	AFT SEGMENT WEATHERSEAL UNBOND
496-05	00	AFT SEG	N/A	AFT DOME	0-120	AFT DOME
496-06	00	AFT SEG	N/A	AFT DOME	120-240	AFT DOME
			RSRM-7A INSULATION 1	POSTFIRE PHO	TOGRAPH L	IST

# PHOTOGRAPHS SORTED BY: SEGMENT, PHOTO CODE, JOINT, SEGMENT END, NEGATIVE # FOR RSRM-7A

EG	PHOTO		JOINT	SEGMENT END	DEG LOC	COMMENT
MBER 96-07	CODE	SEGMENT AFT SEG	N/A	AFT DOME	120-240	AFT DOME
96-08	00	AFT SEG	N/A	AFT DOME	240-0	AFT DOME
30-00		12.1 0110	.,			
T CTR S	EG					
94-04	17	AFT CTR SEG	CIR FIELD JNI	CLEVIS	240-0	CLEVIS, NBR INHIBITOR, AND CYLINDER REGION
82-12	17	AFT CTR SEG	CTR FIELD JNT	CLEVIS	240-0	CLEVIS, NBR INHIBITOR, AND CYLINDER REGION
94-03	<b>16</b>	AFT CTR SEG	CTR FIELD JNT	CLEVIS	120-240	CLEVIS, NBR INHIBITOR, AND CYLINDER REGION
82-11	16	AFT CTR SEG	CTR FIELD JNT	CLEVIS	120-240	CLEVIS, NBR INHIBITOR, AND CYLINDER REGION
194-02	15	AFT CTR SEG	CTR FIELD JNT	CLEVIS	0-120	CLEVIS, NBR INHIBITOR, AND CYLINDER REGION
182-10	15	AFT CTR SEG	CTR FIELD JNT	CLEVIS	0-120	CLEVIS, NBR INHIBITOR, AND CYLINDER REGION
194-01	14	AFT CTR SEG	CTR FIELD JNT	CLEVIS	360	INTERNAL INSULATION, NBR INHIBITOR, AND CYLINDER REGION
182-09	14	AFT CTR SEG	CTR FIELD JNT	CLEVIS	360	INTERNAL INSULATION, NBR INHIBITOR, AND CYLINDER REGION
OD CTR S	SEG					
194-08	13	FWD CTR SEG	CTR FIELD JNT	TANG	240-0	FLAP, CYLINDER REGION, AND TANG
)82-08	13	FWD CTR SEG	CTR FIELD JNT	TANG	240-0	FLAP, CYLINDER REGION, AND TANG FLAP, CYLINDER REGION, AND TANG
194-07	12	FWD CTR SEG	CTR FIELD JNT	TANG	120-240	•
)82-07	12	FWD CTR SEG	CTR FIELD JNT	TANG	120-240	FLAP, CYLINDER REGION, AND TANG
194-06	11	FWD CTR SEG	CTR FIELD JNT	TANG	0-120	FLAP, CYLINDER REGION, AND TANG
182-06	11	FWD CTR SEG	CTR FIELD JNT	TANG	0-120	FLAP, CYLINDER REGION, AND TANG
194-05	10	FWD CTR SEG	CTR FIELD JNT	TANG	360	FLAP, CYLINDER REGION, AND TANG
489 <b>–</b> 10	09	FWD CTR SEG	FWD FIELD JNT	CLEVIS	240-0	CLEVIS, NBR INHIBITOR, AND CYLINDER REGION
489-09	08	FWD CTR SEG	FWD FIELD JNT	CLEVIS	120-240	CLEVIS, NBR INHIBITOR, AND CYLINDER REGION
489-08	07	FWD CTR SEG	FWD FIELD JNT	CLEVIS	0-120	CLEVIS, NBR INHIBITOR, AND CYLINDER REGION
489-07	06	FWD CTR SEG	FWD FIELD JNT	CLEVIS	360	INTERNAL INSULATION, NBR INHIBITOR, AND CYLINDER REGION
WD SEG						
489-06	05	FWD SEG	FWD FIELD JNT	TANG	240-0	FLAP, CYLINDER REGION, AND TANG
489-05	04	FWD SEG	FWD FIELD JNT	TANG	120-240	FLAP, CYLINDER REGION, AND TANG
489-03	03	FWD SEG	FWD FIELD JNT	TANG	0-120	FLAP, CYLINDER REGION, AND TANG
489-02	02	FWD SEG	FWD FIELD JNT	TANG	360	INTERNAL INSULATION AND TANG
489-01	01	FWD SEG	FWD FIELD JNT	FWD DOME	360	FORWARD DOME AND CYLINDER REGION

Table A-34 (Cont)

OF FORM CHARTY

Page 155

# PHOTOGRAPHS SORTED BY: SEGMENT, PHOTO CODE, JOINT, SEGMENT END, NEGATIVE # FOR RSRM-7A

EG MBER	PHOTO CODE	SEGMENT	JOINT	SEGMENT END	DEG LOC	COMMENT
82-01	00	FWD SEG	igniter/case jnt	FWD DOME	360	FORWARD DOME PRIOR TO IGNITER REMOVAL
82-02	00	FWD SEG	igniter/case jnt	FWD DOME	360	FORWARD DOME PRIOR TO IGNITER REMOVAL
83-07	00	FWD SEG	IGNITER/CASE JNT	FWD DOME	360	FORWARD DOME AFTER IGNITER REMOVAL
08-01	00	FWD SEG	N/A	FWD DOME	0-90	IGNITER BOOT REMOVED FROM FORWARD DOME
08-02	00	FWD SEG	N/A	FWD DOME	90-180	IGNITER BOOT REMOVED FROM FORWARD DOME
08-03	00 .	FWD SEG	N/A	FWD DOME	180-270	IGNITER BOOT REMOVED FROM FORWARD DOME
08-04	00	FWD SEG	N/A	FWD DOME	270-0	IGNITER BOOT REMOVED FROM FORWARD DOME
08-05	00	FWD SEG	N/A	FWD DOME	360	IGNITER BOOT REMOVED FROM FORWARD DOME
96-04	00	FWD SEG	N/A	N/A	360	IGNITER BOOT INSULATION
NITER						
83-03	00	IGNITER	N/A	N/A	0	IGNITER
83-04	00	IGNITER	N/A	N/A	180	IGNITER
183-05	00	IGNITER	N/A	N/A	332	PUTTY BLOWHOLE
183-06	00	igniter	N/A	N/A	332	PUTTY BLOWHOLE
184-03	00	IGNITER	N/A	N/A		IGNITER NOZZLE INSERT
186-07	00	IGNITER	N/A	N/A	360	PUTTY ON ADAPTER SURFACE INTERMITTENT
187-03	00	IGNITER	N/A	N/A	360	IGNITER ADAPTER PLATE
187-04	00	IGNITER	N/A	N/A	360	IGNITER CHAMBER

<sup>\*\*</sup>END OF REPORT\*\*\*

CORPORATE THE SECOND

APPENDIX B

TWR-17546 Vol. III

Table B-1 RSRM-7B Aft Dome Factory Joint Weatherseal Evaluation

Motor No	.: RSRM-7B	Date: 26 Novemb	er 1989				
Assessme	nt Engineer(s): S. Hicken	, T. Morgan					
Factory	Joint Weatherseal Observat	ions:					Comment Numbers
Α.	Charred/Heat Affected Mate	erial (HTAFF)?	<u> </u>	yes		no	
В.	Insulation Damage/Missing Due to Reentry/Debris/Wat	Material Not er Impact (TPSVD)?		yes	<u> </u>	no	
c.	Insulation Damage/Missing Reentry/Debris/Water Impa	Material Due to ct (TPSDM)?		yes	<u> </u>	no	
D.	Insulation to Case Unbond	s (DEEND)?		yes	<u> </u>	no	
E.	Evidence of Water Leakage Joint (WATER)?	From Factory		yes	<u> </u>	no	

1. Normal heat effects in 270° region.

Table B-2
RSRM-7B Aft Segment Stiffener to Stiffener Factory Joint Weatherseal Evaluation

Motor No	.: RSRM-7B	Date:	26 Novembe	r 1989				
Assessme	nt Engineer(s): S. Hicken	, T. Morga	n					
Factory	Joint Weatherseal Observat	lons:						Comment Numbers
A.	Charred/Heat Affected Mate	erial (HTA	FF)?	<u> </u>	yes		no	1
в.	Insulation Damage/Missing Due to Reentry/Debris/Wate				yes	<u> </u>	no	
C.	Insulation Damage/Missing Reentry/Debris/Water Impac				yes	<u> </u>	no	
D.	Insulation to Case Unbonds	s (DEBND)?	ı		yes	<u> </u>	no	
E.	Evidence of Water Leakage Joint (WATER)?	From Fact	ory		yes	<u> </u>	no	

1. Normal heat effects in 270° region.

Table B-3
RSRM-7B Aft Segment ET Attach to Stiffener Factory Joint Weatherseal Evaluation

Motor No.	: RSRM-7B	Date: 26	November	1989				
Assessmen	nt Engineer(s): S. Hicken,	T. Morgan						
Factory J	Joint Weatherseal Observati	.ons:						Comment Numbers
Α.	Charred/Heat Affected Mate	erial (HTAFF)	?	<u> </u>	yes		no	1
	Insulation Damage/Missing Due to Reentry/Debris/Wate				yes	<u> </u>	no	
	Insulation Damage/Missing Reentry/Debris/Water Impac		e to		yes	<u> </u>	no	
D.	Insulation to Case Unbonde	E (DEBND)?			yes	<u> </u>	no	
E.	Evidence of Water Leakage Joint (WATER)?	From Factory	•		yes	<u> </u>	no	

1. Normal light heat effects in 270° region.

Table B-4
RSRM-7B Aft Center Segment Factory Joint Weatherseal Evaluation

otor No.: RSRM-7B Date: 26 November 1989							
SSESSITE	nt Engineer(s): S. Hick	en, T. Morgan					
ectory	Joint Weatherseal Observ	ations:					Comment Numbers
A.	Charred/Heat Affected M	aterial (HTAFF)?		yes	<u> </u>	no	
В.	Insulation Damage/Missin Due to Reentry/Debris/W			yes	<u> </u>	no	
. C.	Insulation Damage/Missi Reentry/Debris/Water Im		·	yes	<u> </u>	no	_,
D.	Insulation to Case Unbo	nds (DEBND)?		yes	<u> </u>	no	
E.	Evidence of Water Leaka Joint (WATER)?	ge From Factory		yes	<u> </u>	no	

Table B-5
RSRM-7B Forward Center Segment Factory Joint Weatherseal Evaluation

Motor No.: RSRM-7B	Date: 26 November	er 1989				
Assessment Engineer(s): S. Hicken	, T. Morgan					
Factory Joint Weatherseal Observat	ions:					Comment Numbers
A. Charred/Heat Affected Mat	erial (HTAFF)?		yes	<u> </u>	no	
B. Insulation Damage/Missing Due to Reentry/Debris/Wat	Material Not er Impact (TPSVD)?		yes	<u> </u>	no	
C. Insulation Damage/Missing Reentry/Debris/Water Impa		<u> </u>	yes		no	1
D. Insulation to Case Unbond	s (DEBND)?		yes	<u> </u>	no	
E. Evidence of Water Leakage Joint (WATER)?	From Factory		yes	<u> </u>	no	

1. Missing material at 270° on aft edge. Measures approx. 2 in. circ. by 1 in. long.

Table B-6
RSRM-7B Forward Segment Cylinder to Cylinder Factory Joint Weatherseal Evaluation

Motor No	.: RSRM-7B	Date: 26 November	er 1989				
Assessme	nt Engineer(s): S. Hicken	T. Morgan					
Factory	Joint Weatherseal Observat:	ons:		·			Comment Numbers
<b>A.</b>	Charred/Heat Affected Mate	erial (HIAFF)?		yes	<u> </u>	no	
В.	Insulation Damage/Missing Due to Reentry/Debris/Wate	Material Not er Impact (TPSVD)?		yes	<u> </u>	no	<u></u>
C.	Insulation Damage/Missing Reentry/Debris/Water Impa			yes	<u> </u>	no	
D.	Insulation to Case Unbonde	s (DEEND)?	<u> </u>	yes		no	1
E.	Evidence of Water Leakage Joint (WATER)?	From Factory		yes	<u> </u>	no	

#### 1. Three edge separations:

One at 160° on forward edge 1 in. to 1.5 in. deep, 14 in. circ., open 0.1 in., paint missing forward of weatherseal. Missing paint measures 2.4 in. long by 5 in. circ. and 3.25 in. long by 7 in. circ.

One at 210° on aft edge 0.6 in. long by 1 in. circ. Adhesive failure at Chemlok 205 to case.

One unbond at 135° 11 in. circ. on forward edge 0.1 in. deep.

Table B-7
RSRM-7B Forward Dome Factory Joint Weatherseal Evaluation

Motor No.: RSRM-7B	Date: 26 November	er 1989				
Assessment Engineer(s): S. Hid	ten, T. Morgan					
Factory Joint Weatherseal Observ	vations:					Comment Numbers
A. Charred/Heat Affected	faterial (HTAFF)?		yes	<u> </u>	no	
B. Insulation Damage/Miss Due to Reentry/Debris/	ing Material Not Water Impact (TPSVD)?		yes	<u> </u>	no	
C. Insulation Damage/Miss Reentry/Debris/Water I	ing Material Due to mpact (TPSDM)?		yes	<u> </u>	no	
D. Insulation to Case Unb	onds (DEBND)?	<del></del>	yes	<u> </u>	no	
E. Evidence of Water Leak Joint (WATER)?	age From Factory		yes	<u> </u>	no	

Table B-8 RSRM-7B Aft Stiffener Ring TPS Evaluation

Motor No	.: RSRM-7B	Date: 26 Novemb	oer 1989				
Assessme	nt Engineer(s): S. Hicken	, T. Morgan					
Stiffene	er Ring/Stiffener Stub Insu	lation Observations	<u>:</u>				Comment Numbers
Α.	Charred/Heat Affected Mat	erial (HTAFF)?	<u> </u>	yes		no	1
В.	Insulation Damage/Missing Due to Reentry/Debris/Wat	Material Not er Impact (TPSVD)?		yes	<u> </u>	no	
c.	Insulation Damage/Missing Reentry/Debris/Water Impo	Material Due to nct (TPSDM)?		yes	<u> </u>	no	•
D.	Insulation to Stiffener I Stub Unbonds (DEEND)?	Ring/Stiffener		yes	<u> </u>	no	

Notes/Comments:

1. Normal heat effects in 270° region. Blisters (heat effect) on outboard face at 270°.

### Table B-9 RSRM-7B Center Stiffener Ring TPS Evaluation

Motor No.: RSRM-7B	Date: 26 November	1989				
Assessment Engineer(s): S. Hicken	, T. Morgan					
Stiffener Ring/Stiffener Stub Insu	lation Observations:					Comment Numbers
A. Charred/Heat Affected Mat	erial (HTAFF)?	<u> </u>	yes		no	1
B. Insulation Damage/Missing Due to Reentry/Debris/Wat	Material Not er Impact (TPSVD)?		yes	<u> </u>	no	
C. Insulation Damage/Missing Reentry/Debris/Water Impe	Material Due to ct (TPSDM)?		yes	<u> </u>	no	
D. Insulation to Stiffener F Stub Unbonds (DEEND)?	ting/Stiffener		yes	<u> </u>	no	

#### Notes/Comments:

1. Normal heat effects in 270° region.

Table B-10
RSRM-7B Forward Stiffener Ring TPS Evaluation

otor No	otor No.: RSRM-7B Date: 26 November 1989							
\ssessme	nt Engineer(s): S. Hicken	, T. Morgan						
Stiffene	er Ring/Stiffener Stub Insu	lation Observations:					Comment Numbers	
Α.	Charred/Heat Affected Mat	erial (HTAFF)?	<u> </u>	yes		no	1	
В.	Insulation Damage/Missing Due to Reentry/Debris/Wat	Material Not er Impact (TPSVD)?	<del></del>	yes	<u> </u>	no		
c.	Insulation Damage/Missing Reentry/Debris/Water Impa	Material Due to ct (TPSDM)?		yes	<u> </u>	no	<u> </u>	
D.	Insulation to Stiffener F Stub Unbonds (DEBND)?	ing/Stiffener		yes	<u> </u>	no		

#### Notes/Comments:

1. Normal heat effects in 270° region.

# Table B-11 RSRM-7B Forward Stiffener Stub TPS Evaluation

Motor No.	: RSRM-7B	Date: 26 November	r 1989				
Assessmen	t Engineer(s): S. Hicken,	T. Morgan					
Stiffener	Ring/Stiffener Stub Insul	ation Observations:					Comment Numbers
Α. (	Charred/Heat Affected Mate	rial (HTAFF)?	<u> </u>	yes		no	1
<b>B.</b> [	Insulation Damage/Missing Due to Reentry/Debris/Wate	Material Not er Impact (TPSVD)?	<del></del>	yes	<u> </u>	no	
<b>C.</b> 1	Insulation Damage/Missing Reentry/Debris/Water Impac	Material Due to :t (TPSDM)?		yes	<u> </u>	no	
	Insulation to Stiffener Ri Stub Unbonds (DEEND)?	ing/Stiffener		yes	<u> </u>	no	

#### Notes/Comments:

1. Normal heat effects in 270° region. K5NA repair of outboard edge was broken off intermittently around the circumference.

## Table B-12 RSRM-7B Nozzle to Case Joint Insulation Evaluation

Motor No.: RSRM-7B	Date: 2 December 1989
Assessment Engineer(s): J. Passmar	n, S. Hicken
Nozzle to Case Joint Observations:  A. Gas Penetration in Polysulfic B. Foreign Material in Polysulfic C. Voids in Polysulfide (VOID)? D. Polysulfide Porosity (PSPOR) E. Polysulfide Extrusion Past W. F. Polysulfide Failure Mode?	ide (FMIJ)?
Mozzle to Case Joint Insulation Par G. Aft Dome Edge Unbonds (DBOND H. Baffle Torn (DBAFL)?	Y
Record Aft Dome End Nozzle to Case	Degree Depth Depth Depth Location (1)* (2)** (3)***
	0°       6.75 in.       5.95 in.       5.60 in.         90°       7.00 in.       6.10 in.       5.60 in.         180°       7.00 in.       6.10 in.       5.70 in.         270°       7.00 in.       6.05 in.       5.70 in.
Enterthin	Max
** Depth (2) is to be measured i	from the aft face of the aft dome to the edge of the remaining material from the aft face of the aft dome to the inboard edge of the heat from the aft face of the aft dome to the outboard edge of the heat

- 1. Slight porosity showing in the polysulfide in the step region.
- 2. Polysulfide showing past wiper, only at vent slot locations; normal condition due to large amount of polysulfide in joint.
- 3. Baffle was not torm (prefire DR condition as a result of nozzle removal repaired). Baffle was pulled up at the CF/EPDM to NBR bondlines full circ. It was pulled aft all the way back to the polysulfide as indicated by black marks on the adhesive. This is a result of disassembly where excess charred polysulfide on the fixed housing caught on the baffle at disassembly.

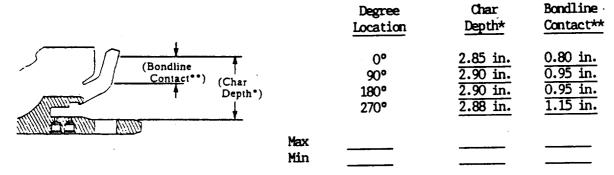
Table B-13 RSRM-7B Nozzle to Case Joint Vent Slot Fill

otor No.: RSRM-7B		Date: 2 December	1989		
ssessment Engineer(	s): J. rassim,	5. mcker			
Degree	% Slot	Degree	% Slot	Degree	% Slot
Location	Fill	Location	<u>Fill</u>	Location	<u>Fill</u>
0.00	100	122.4°	80	244.8°	90
7.2°	100	129.6°	100	252.0°	60
14.40	100	136.8°	80	259.2°	100
21.6°	100	144.0°	95	266.4°	30
28.8°	100	151.2°	50	273.6°	<b>70</b>
36.0°	100	158.4°	100	280.8°	60
43.2°	100	165.6°	100	288.0°	100
50.4°	100	172.8°	100	295.2°	60
57.6°	100	180.0°	100	302.4°	50
64.8°	100	187.2°	100	309.6°	100
72.0°	100	194.40	100	316.8°	60
72.0 79.2°	100	202.6°	100	324.0°	50
86.4°	100	208.8°	50	331.2°	100
93.6°	80	216.0°	60	338.4°	60
100.8°	60	223.2°	100	345.6°	40
108.0°	60	230.4°	30	352.8°	100
115.2°	100	237.6°	100		
	Average = <u>84%</u>		slots had 0% fi had 100% fill	11	

## Table B-14 RSRM-7B Aft Field Joint Insulation Evaluation

Motor No.: RSRM-7B	Date: 1 December 1989	
Assessment Engineer(s): S. Hicken	, J. Passman, D. Bartelt	
A. Gas Penetration (TBH, PGPIH): B. Foreign Material (FMLJ)? C. Areas of J-leg Non-contact (D. Wet Soot (SOOT)?  Field Joint Insulation Part Observe	yes         X         no           yes         X         no           yes         X         no           X         yes         no	Comment Numbers  1 2,3
E. Clevis Edge Unbonds > 0.10 in F. Clevis Insulation Crack/Carz	n. Deep (DBOND)? yesX no	4

### Record Tang End Field Joint Insulation Measurements:



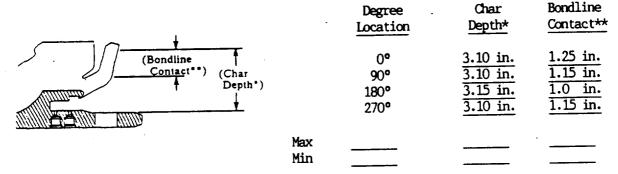
- \* Char depth is to be measured from the inner diameter of the tang leg to the outbard edge of the char layer.
- \*\* Bondline contact is to be measured from the outboard edge of the char layer to the outboard extent of contact.

- 1. Tape adhesive residue intermittent full circumference on clevis insulation.
- 2. Water line smudge marks 286°-296° and 246°-254° due to disassembly.
- 3. 0.20 0.70 in. intermittent full circumference. Maximum condition 182° 176° 0.90.
- 4. 0°, 10°-14°, 35°-42°, 52°, 82°-100°, 165°, 224°, 342°-338° cracks in radius region of clevis insulation.

## Table B-15 RSRM-7B Center Field Joint Insulation Evaluation

Motor No.: RSRM-7B	Date: 1 December 1989	
Assessment Engineer(s): S. Hicken,	J. Passman, D. Bartelt	
A. Gas Penetration (TBH, PGPIH)? B. Foreign Material (FMIJ)? C. Areas of J-leg Non-contact (BLD). Wet Soot (SOOT)?	yes X no yes X no yes X no X yes X no xyes x no	Comment Numbers  1 2
E. Clevis Edge Unbonds > 0.10 in. F. Clevis Insulation Crack/Carzin	Deep (DBOND)? yesXno	3

## Record Tang End Field Joint Insulation Measurements:



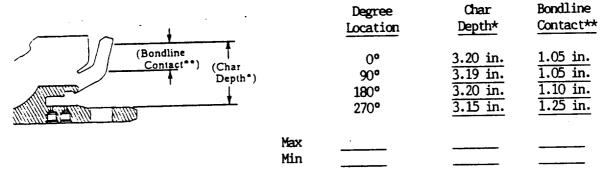
- \* Char depth is to be measured from the inner diameter of the tang leg to the outbard edge of the char layer.
- \*\* Bondline contact is to be measured from the outboard edge of the char layer to the outboard extent of contact.

- 1. Clevis edge separation repair adhesive noted on insulation surface 2.1 in. from tip of clevis at 260°, 265°, 292°, 295°, 296°, and 298°.
- 2. Maximum condition 1.35 in. at 166°-182°, 0.30 in. 0.70 in. full circumference.
- 3. Intermittent from 30°-180°-250°.

## Table B-16 RSRM-7B Forward Field Joint Insulation Evaluation

Motor No.: RSRM-7B	Date: 1 December	r 1989				
Assessment Engineer(s): S. Hicken	, J. Passman, D. Bar	telt			- :	
Field Joint Insulation Joint Obser	vations:					Comment Numbers
A. Gas Penetration (TBH, PGPTH) B. Foreign Material (FMLJ)? C. Areas of J-leg Non-contact ( D. Wet Soot (SOUT)?		<u>x</u>	yes yes yes yes	<u> </u>	no no no no	2
Field Joint Insulation Part Observ	ations:					
E. Clevis Edge Unbonds > 0.10 i F. Clevis Insulation Crack/Carz	n. Deep (DBOND)? ring (CRAZE)?	<u> </u>	yes yes	<u> </u>	no no	3

### Record Tang End Field Joint Insulation Measurements:



- \* Char depth is to be measured from the inner diameter of the tang leg to the outbard edge of the char layer.
- \*\* Bondline contact is to be measured from the outboard edge of the char layer to the outboard extent of contact.

- 1. Masking tape residue on clevis leg insulation.
- 2. 0.30 in. 0.50 in. deep full circumference. (Max. 0.80 at  $134^{\circ}$ )
- 3. Crack exists intermittently around circumference form 300°-0°-220°. Not open and did not affect function of the joint (prefire P.R. condition).

## Table B-17 RSRM-7B Igniter Boss Insulation Evaluation

Motor No.: RSRM-7B	Date: 30 November 198	39	
Assessment Engineer(s): S. Hicken,	J. Passman		
A. Abnormal Insulation Erosion (B. Tears, Gouges, or Cuts (TEARS). C. Ply Separations or Delamination. Blistering (BLSPT)? E. Insulation Flashing (FLASH)? F. Edge Unbonds (DBOND)?	INSER)?	yes         X           yes         X           yes         X           yes         X           X         yes           yes         X	Comment Numbers  no

#### lotes/Comments:

1. Intermittent loose flashing between 200°-270°-20°. Maximum length of 0.075 in.

# Table B-18 RSRM-7B Igniter Chamber Insulation Evaluation

Motor No.: RSRM-7B	Date: 30 November 1989	
Assessment Engineer(s): S. Hicken	J. Passman	
Igniter Chamber/Igniter Boss Insula	ation Observations:	Comment Numbers
<ul><li>A. Abnormal Insulation Erosion</li><li>B. Tears, Gouges, or Cuts (TEARS)</li><li>C. Ply Separations or Delamination</li><li>D. Blistering (BLSPT)?</li></ul>	S)? yes _X no	

# Table B-19 RSRM-7B Igniter Adapter to Forward Dome Putty Evaluation

Motor No.: RSRM-7B	Date: 30 November 1989	4
Assessment Engineer(s): S. Hicker	n, J. Passman	$\dashv$
Igniter Putty Condition		
1. Color? 2. Tack?	Variable X Constant Good X Nominal Poor	
Igniter Putty Observations:	Comment Numbers	
A. Gas Penetration in Putty (B. Foreign Material in Putty C. Voids in Putty (VOID)? D. Putty Failure Mode	TBH, PGPIH)?	
Record the following if any of the	e above conditions exist:	
Condition Start (Observation Location Code) (deg.)	Degree Stop Location Circumferential Axial Radial (deg.) Width (in.) Length (in.) Depth (in.)	— — — — — — — — — — — — — — — — — — —

### Notes/Comments:

1. Putty was present up to and intermittently on the adapter.

## Table B-20 RSRM-7B Igniter Adapter to Igniter Chamber Putty Evaluation

Motor No.: RSRM-7B	Date: 30 Nov	vember 1989		
Assessment Engineer(s): S	. Hicken, J. Passman			
Igniter Putty Condition  1. Color? 2. Tack?	Variable Good	X Constant X Nominal		Poor
A. Gas Penetration in B. Foreign Material in C. Voids in Putty (VC D. Putty Failure Model Record the following if an	Putty (TBH, PCPIH)? In Putty (FMLJ)? OID)?0	yes % Adhesve (AFJFM) 1	no X no X no 00 % Cohesive	(CRADH)
Condition (Observation Code) PGPTH	Degree Degree Start Stop Location Location (deg.) (deg.)	Circumferential Width (in.) 0.525 at aft edge 0.50 at fwd edge	Axial Length (in.)	Radial Depth (in.)

### Notes/Comments:

1. Blowhole at 340°. Soot in putty from 315° to 350°.

### Table B-21 RSRM-7B Aft Segment Internal Insulation Evaluation

Motor No	.: RSRM-7B	Date: 1 Decemb	er 1989				
Assessme	ent Engineer(s): J. Passman	n, S. Hicken					
Segment	Internal Insulation Observa	ations:					Comment Numbers
Α.	Abnormal Insulation Erosi	on (INSER)?		yes	X	no	
В.	Tears, Gouges, or Cuts (T	EARS)?	<u> X</u>	yes	<del>- ;;</del>	no	
C.	Ply Separations or Delami	nations (PLYSP)?		yes	X	no	
D.	Blistering (BLSPT)?			yes	X_	no	
E.	Abnormal Liner Pattern (A	BLNR)?		yes	<u> </u>	no	
F.	NBR Under CF/EPDM Exposed	(INSER)?	<u> </u>	yes		no	4

- Scratches and scuff marks from splashdown debris impact 0°-45° from dome factory joint to NER inhibitor. Small cut with peeled up insulation in the CF/EPDM in the aft dome at 215°, located 15 in. forward of nozzle boss measuring 3.1 in. circ. x 2.7 in. long. Triangular in shape with peeled up insulation ~ 0.05 in. thick. Scrapes were present indicating debris impact caused this.
- 2. No blisters were present in aft dome CF/EPDM.
- 3. No liner present which is normal.
- 4. NER under CF/EPDM was exposed in 4-5 places throughout circumference just aft of the remaining CF/EPDM to NER interface; approx. 15-20 in. from boss. This is normal condition.

## Table B-22 RSRM-7B Aft Segment NBR Inhibitor Height Evaluation

Motor No.: RSRM-7B	Date: 1 December 1989	
Assessment Engineer(s): S. Hick	ken, J. Passman, D. Bartelt	
NBR Inhibitor Observations (Other	er Than Tears):	Comment Numbers
A. Delaminations or Separa B. Severe or Abnormal Ero	ations (PLYSP)? yes X sion (INSER)? yes X	no
Record NBR Inhibitor Measuremen	ts:	

Degree Location	Radial Distance	Degree Location	Radial Distance
0° 30° 60°	8.5 in.  7.0 in.  7.5 in.	180° 210° 240° 270°	6.0 in. 5.0 in. 5.5 in. 4.5 in.
90° 120° 150°	3.5 in. 4.0 in.	300° 330°	7.5 in. 9.0 in.

Max. inhibitor height = Min. inhibitor height =

Table B-23 RSRM-7B Aft Segment NBR Inhibitor Tear Evaluation

Notor No.: RSRM-7B Date: 1 December 1989				
Assessment Engineer(s): S. Hicken, J	. Passman, D. Bartelt			
NBR Inhibitor Description		Comment Numbers		
A. Radial Tears > 3 in. Long (TEARS) B. Circumferential tears? C. Tears exhibiting charring or eros	yes X no			
Record NER Inhibitor Tear Measurement	s (if applicable, for radial tears > 3 in. long or circ.	tears):		
Degree Location Meas. "A"*	Meas. "B"* Comments (Charring, etc.)			
	· · · · · · · · · · · · · · · · · · ·			
		-		
* Measurements "A" and "B" are to me as shown and sketched below.	easured 90°			
Clevis	1.D. ———————————————————————————————————			

Notes/Comments:

270°

# Table B-24 RSRM-7B Aft Center Segment Internal Insulation Evaluation

Motor No.	: RSRM-7B	Date: 1 December	1989				
Assessmen	nt Engineer(s): J. Passman	1					
Segment 1	Internal Insulation Observ	ations:					Comment Numbers
В.	Abnormal Insulation Erosic Tears, Gouges, or Cuts (T Ply Separations or Delami	EARS)?	<u> </u>	yes yes yes	<u> </u>	no no no	<u> </u>
D.	Blistering (BLSPT)? Abnormal Liner Pattern (A			yes yes	<u>X</u>	no no	2

- 1. Scratches and scuff marks from splashdown debris impact 0°-30° full length of segment.
- 2. Liner present normally 2-3 ft. forward of factory joint to NBR inhibitor.

Table B-25 RSRM-7B Aft Center Segment NBR Inhibitor Height Evaluation

	S. Hicken, J. Passman, D. Ba		Comment
Inhibitor Observat:	ions (Other Than Tears):		Numbers
A. Delaminations	or Separations (PLYSP)?	yes <u>X</u>	no
	ormal Erosion (INSER)?	yes X	no
AMD Tubibison W	oog moments:		
cord NBR Inhibitor M	asureneros.		
Degree Location	Radial Distance	Degree Location	Radial Distance
	14 O in	180°	12.5 in.
0°	14.0 in. 14.7 in.	210°	14.0 in.
30°	15.0 in.	240°	13.5 in.
60° 90°	12.5 in.	270°	13.0 in.
	11.0 in.	300°	15.0 in.
	11.0 111.	330°	13.0 in.
120° 150°	12.5 in.		

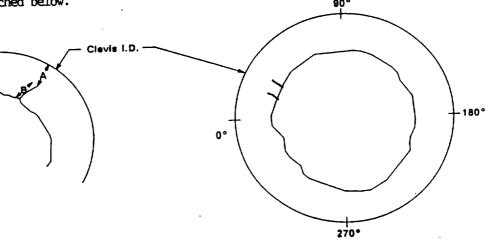
# Table B-26 RSRM-7B Aft Center Segment NBR Inhibitor Tear Evaluation

Motor No.: RSRM-7B	Date: 1 December 1989						
Assessment Engineer(s): S. Hicken, J. Passman, D. Bartelt							
NBR Inhibitor Description		Comment Numbers					
<ul><li>A. Radial Tears &gt; 3 in. Long (TEARS)?</li><li>B. Circumferential tears?</li><li>C. Tears exhibiting charring or erosis</li></ul>	yes X no	See Below					

## Record NER Inhibitor Tear Measurements (if applicable, for radial tears > 3 in. long or circ. tears):

Degree Location	Meas. "A"*	Meas. "B"*	Comments (Charring, etc.)
<del>9</del> 18 .	10.0 in.	4.5 in. 4.0 in.	
		<del></del>	
		<del></del>	
		<del></del>	
		<del></del>	
<del></del>			

\* Measurements "A" and "B" are to measured as shown and sketched below.



### Table B-27 RSRM-7B Aft Center Segment Stress Relief Flap Evaluation

fotor No.: RSRM-7B	Date: 1 December 1989
ssessment Engineer(s): S. Hicken	, J. Passman, D. Bartelt
tress Relief Flap Region Observat	tions: Comment Numbers
A. Abnormal CF/EPDM or NBR Eros B. Tears Gouges, or Cuts (TEARS C. Ply Separations, Delaminatio D. Abnormal/Unusual Missing Mat E. Castable Inhibitor Present?	yes   X   no     yes   X   no       yes   x   no
ecord Stress Relief Flap Measure	ements:
3	
Degre	ee Location Axial Distance 16.0 in. See Comment 1 below
	90° 16.0 in.
	180° 16.0 in.
·	270° <u>16.0 in.</u>
Max. Missing (If Appl.)	
Min. Missing (If Appl.)	
Record Stress Relief Flap Tear Mea	asurements (If Applicable):
	rement "A"** Measurement "B"*** Comments (Charring, etc.)
* Axial distance is to be m	measured from the tip of the tang to the aft edge of the flap.
which Washington HAII is to be	taken from the tip of the tang to the all edge of the Liap.
the Management "R" is to be	taken from the aft edge of the flap to the forward edge of the tear.

#### Notes/Comments

1. Flap is eroded back to flap bulb full circumference.

# Table B-28 RSRM-7B Forward Center Segment Internal Insulation Evaluation

fotor No.	.: RSRM-7B	Date: 1 December	r 1989					
Assessment Engineer(s): J. Passman								
Segment :	Internal Insulation Observ	ations:					Comment Numbers	
В.	Abnormal Insulation Erosi Tears, Gouges, or Cuts (T Ply Separations or Delami	EARS)?	<u> </u>	yes yes yes	<u> </u>	no no no	1	
D.	Blistering (BLSPT)? Abnormal Liner Pattern (A			yes yes	X	no no	2	

- 1. Scratches and scuff marks from splashdown debris impact 350°-355°-0° full length of segment.
- 2. Liner present normally slightly forward of factory joint to NER inhibitor.

Table B-29
RSRM-7B Forward Center Segment NBR Inhibitor Height Evaluation

Motor No.: RSRM-7B	Date: 1 Decembe	er 1989	
Assessment Engineer(s):	S. Hicken, J. Passman, D. Bar	rtelt	
NER Inhibitor Observation		ves X	Comment Numbers no
B. Severe or Abno	or Separations (PLYSP)? rmal Erosion (INSER)?	yes <u>X</u> yes <u>X</u>	no
Record NBR Inhibitor Me	asurements:		
Degree Location	Radial Distance	Degree Location	Radial Distance
0° 30° 60° 90° 120° 150°	26.5 in. 25.0 in. 27.5 in. 25.5 in. 24.0 in. 26.0 in.	180° 210° 240° 270° 300° 330°	26.0 in. 27.0 in. 24.5 in. 24.0 in. 24.5 in. 24.5 in.
Max. inhibitor he			

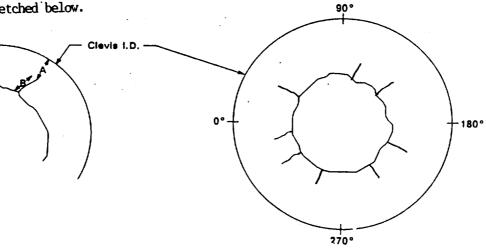
Table B-30 RSRM-7B Forward Center Segment NBR Inhibitor Tear Evaluation

Motor No.: RSRM-7B	Date: 1 December 1989					
Assessment Engineer(s): S. Hicken, J. Passman, D. Bartelt						
NBR Inhibitor Description	Comment Numbers					
<ul><li>A. Radial Tears &gt; 3 in. Long (TEAR</li><li>B. Circumferential tears?</li><li>C. Tears exhibiting charring or er</li></ul>	See Below					

## Record NBR Inhibitor Tear Measurements (if applicable, for radial tears > 3 in. long or circ. tears):

Degree Location	Meas. "A"*	Meas. "B"*	Comments (Charring, etc.)
31	$\overline{17.0}$ in.	8.5 in.	
105	17.0 in.	8.0 in.	
136	15.0 in.	9.0 in.	
190	14.5 in.	11.5 in.	
240	18.0 in.	6.5 in.	
291	14.5 in.	9.5 in.	
334	13.5 in.	11.5 in.	
354	17.5 in.	7.5 in.	

\* Measurements "A" and "B" are to measured as shown and sketched below.



### Table B-31 RSRM-7B Forward Center Segment Stress Relief Flap Evaluation

Motor No.: RSRM-7B	Date: 1 December 1989		
Assessment Engineer(s): S. Hicken	, J. Passman, D. Bartelt		
Stress Relief Flap Region Observat	ions:		Comment Numbers
A. Abnormal CF/EPDM or NER Eros B. Tears Gouges, or Cuts (TEARS C. Ply Separations, Delaminatio D. Abnormal/Unusual Missing Mat E. Castable Inhibitor Present?	ns, or Voids (PLYSP)?	yes X no	<u></u>
Record Stress Relief Flap Measure	ments:		
	Axial Dis   11.25   10.0     10.0	in. in. in.	
Record Stress Relief Flap Tear Me	asurements (If Applicable):		
	ement "A"** Measurement		arring, etc.)
the Management MAN is to be	easured from the tip of the taken from the tip of the tar taken from the aft edge of th	ng to the alt edge of the	: rrah.

#### Votes/Comments:

1. Small blisters (closed) in carbon fiber intermittent full circumference.

Table B-32 RSRM-7B Forward Segment Internal Insulation Evaluation

Motor No.: RSRM-7B	Date: 1 December 1989							
Assessment Engineer(s): J. Passman								
Segment Internal Insulat	ion Observations:	Conment Numbers						
R. Tears, Gouges, C	ation Erosion (INSER)?  or Cuts (TEARS)?  s or Delaminations (PLYSP)?  Pattern (ABLNR)?  yes X no yes X no yes X no yes X no							

#### lotes/Comments:

1. Eleven star pattern evident 6-12 in. aft of cylinder to cylinder factory joint.

### Table B-33 RSRM-7B Forward Segment Stress Relief Flap Evaluation

otor No.: RSRM-7B	Date: 1 December	1989				
ssessment Engineer(s): S. Hicker	n, J. Passman, D. Bart	elt				
tress Relief Flap Region Observat	tions:					Comment
tress Retter Flap Region Goserva						Numbers
A. Abnormal CF/EPDM or NBR Eros	sion (INSER)?		yes	<u>X</u>	no	
B. Tears Gouges, or Cuts (TEARS	5)?		yes	<u>X</u> .	no	
C. Ply Separations, Delamination	ons, or Voids (PLYSP)?	·	yes	<u> X</u>	no	1
D. Abnormal/Unusual Missing Mar	terial (MISS)?		yes	X	no	τ
E. Castable Inhibitor Present?			yes	<u> </u>	no	
				•		
ecord Stress Relief Flap Measur	ements:					
tord ottess retree 1 mp						
Degr	~ <del>~</del>	dal Distan				
	0°	3.5 in.	`	II IIAP I	emaining)	
	90° _	3.5 in. 3.5 in.				
	180° 270°	4.0 in.	_			
		7.0 11.0	_			
Max. Missing (If Appl.)  Min. Missing (If Appl.)	<del></del>					
mii. missing (in appro)			<del></del>			
ecord Stress Relief Flap Tear Me	asurements (If Applic	able):				
			ماساسان ۱۲	Commont	s (Charrin	m etc.)
Degree Location Measur	ement "A"** Mea	surement "B		willen	S (CHELLIN	g, etc./
			_			
			_			
			-			
	<del></del>					
			_			
* Axial distance is to be	measured from the tip	of the tang	g to the	aft edge	of the fl	ap.
the Manuscrapt MAN is to be	taken from the tip OI	the tang t	to the a	ttenge o	hr nas rroch	<b>/•</b>
** Measurement "A" is to be	taken from the aft ed	ge of the f	flap to	the forward	ard edge of	the tear

#### Votes/Comments:

1. 210°-214° area of erosion (10 in. meximum). 168° area of erosion (11 in. maximum).

## PHOTOGRAPHS SORTED BY: SEGMENT, PHOTO CODE, JOINT, SEGMENT END, NEGATIVE # FOR RSRM-7B

:g Ber	PHOTO CODE	SEGMENT	JOINT	SEGMENT END	DEG LOC	COMMENT -
, HOUSI	NG					
4-01	00	FXD HOUSING	NOZZLE/CASE JNT	CLEVIS	354.6	O-RING DAMAGE (POLYSULFIDE)
14-02	00	FXD HOUSING	NOZZLE/CASE JNT	CLEVIS	52.2	O-RING DAMAGE (POLYSULFIDE)
14-03	00	FXD HOUSING	NOZZLE/CASE JNT	CLEVIS	354.6	O-RING DAMAGE (POLYSULFIDE)
14-04	00	FXD HOUSING	NOZZLE/CASE JNT	CLEVIS	354.6	O-RING DAMAGE (POLYSULFIDE)
14-05	00	FXD HOUSING	NOZZLE/CASE JNT	CLEVIS	354.6	O-RING DAMAGE (POLYSULFIDE)
)9-01	00	FXD HOUSING	N/A	N/A	0 .	NOZZLE OVERALL
)9-03	00	FXD HOUSING	N/A	N/A	90	NOZZLE OVERALL
<b>39-04</b>	00	FXD HOUSING	N/A	n/A	180	NOZZLE OVERALL
09-05	00	FXD HOUSING	N/A	N/A	270	NOZZLE OVERALL
10-01	00	FXD HOUSING	N/A	N/A	0	NOZZLE OUTER BOOT RING - AFT TIP
10-02	00	FXD HOUSING	N/A	N/A	45	NOZZLE OUTER BOOT RING - AFT TIP
10-03	00	FXD HOUSING	N/A	N/A	90	NOZZLE OUTER BOOT RING - AFT TIP
10-04	00	FXD HOUSING	N/A	N/A	135	NOZZLE OUTER BOOT RING AFT TIP
10-05	00	FXD HOUSING	N/A	N/A	180	NOZZLE OUTER BOOT RING - AFT TIP
10-06	00	FXD HOUSING	N/A	N/A	225	NOZZLE OUTER BOOT RING - AFT TIP
10-07	00	FXD HOUSING	N/A	N/A	270	NOZZLE OUTER BOOT RING - AFT TIP
10-08	00	FXD HOUSING	N/A	N/A	315	NOZZLE OUTER BOOT RING - AFT TIP
T SEG	00	AFT SEG	NOZZLE/CASE JNT	AFT DOME	0-120	NOZZLE BOSS, AFT DOME, AND CYLINDER
,05–06	00	A 1 556	,			REGION-
i05–07	00	AFT SEG	NOZZLE/CASE JNT	AFT DOME	120-240	NOZZLE BOSS, AFT DOME, AND CYLINDER REGION
i05-08	00	AFT SEG	NOZZLE/CASE JNT	AFT DOME	240-0	NOZZLE BOSS, AFT DOME, AND CYLINDER REGION
i06 <u>-</u> 01	00	AFT SEG	NOZZLE/CASE JNT	AFT DOME	183.8	NOZZLE TO CASE JOINT FIXED HOUSING - LACK OF GREASE
i05–02	00	AFT SEG	N/A	AFT DOME	0-120	AFT DOME INSULATION
505-03	00	AFT SEG	N/A	AFT DOME	120-240	AFT DOME INSULATION
30504	00	AFT SEG	N/A	AFT DOME	240-0	AFT DOME INSULATION
30505	00	AFT SEG	N/A	AFT DOME	215	AFT DOME DEBRIS CUT IN CF/EPDM
T CTR	SEG		·	CT SUT C	240-0	CLEVIS, NBR INHIBITOR, AND CYLINDER
191-09	17	AFT CTR SEG	CTR FIELD UNT	CLEVIS	240-0	REGION
491-08	16	AFT CTR SEG	CTR FIELD JNT	CLEVIS	120-240	CLEVIS, NBR INHIBITOR, AND CYLINDER REGION
491-07	15	AFT CTR SEG	CTR FIELD JNT	CLEVIS	0-120	CLEVIS, NBR INHIBITOR, AND CYLINDER REGION
491-05	14	AFT CTR SEG	CTR FIELD JNT	CLEVIS	360	INTERNAL INSULATION, NBR INHIBITOR, AND CYLINDER REGION
			RSRM-7B Insulat	ion Postfire P		
	• •	A		Table B-34	OF POOR	QUALIFY
					-	Page 185

# PHOTOGRAPHS SORTED BY: SEGMENT, PHOTO CODE, JOINT, SEGMENT END, NEGATIVE # FOR RSRM-7B

;g Ber	PHOTO CODE	SEGMENT	JOINT	SEGMENT END	DEG LOC	COMMENT
) CTR S	SEG			TANG	240-0	FLAP, CYLINDER REGION, AND TANG
1-04	13	FWD CTR SEG	CTR FIELD JNT	_	120-240	FLAP, CYLINDER REGION, AND TANG
)1-03	12	FWD CTR SEG	CTR FIELD JNT	TANG	0-120	FLAP, CYLINDER REGION, AND TANG
91-02	11	FWD CTR SEG	CTR FIELD JNT	TANG	360	FLAP, CYLINDER REGION, AND TANG
31-01	10	FWD CTR SEG	CTR FIELD JNT	TANG		CLEVIS, NBR INHIBITOR, AND CYLINDER
90-10	09	FWD CTR SEG	FWD FIELD JNT	CLEVIS	240-0	REGION
9009	08 -	FWD CTR SEG	FWD FIELD JNT	CLEVIS	120-240	CLEVIS, NBR INHIBITOR, AND CYLINDER REGION
90-08	07	FWD CTR SEG	FWD FIELD JNT	CLEVIS	0-120	CLEVIS, NBR INHIBITOR, AND CYLINDER REGION
90-07	06	FWD CTR SEG	FWD FIELD JNT	CLEVIS	360	INTERNAL INSULATION, NBR INHIBITOR, AND CYLINDER REGION
ID SEG						TANG
90-06	05	FWD SEG	FWD FIELD JNT	TANG	240-0	FLAP, CYLINDER REGION, AND TANG
190-05	04	FWD SEG	FWD FIELD JNT	TANG	120-240	FLAP, CYLINDER REGION, AND TANG
190-04	03	FWD SEG	FWD FIELD JNT	TANG	0-120	FLAP, CYLINDER REGION, AND TANG
190-03	(2	FWD SEG	FWD FIELD JNT	TANG	360	INTERNAL INSULATION AND TANG
190-01	01	FWD SEG	FWD FIELD JNT	FWD DOME	360	FORWARD DOME AND CYLINDER REGION
171-02	00	FWD SEG	FWD CYL/CYL FACT JNT	N/A	165	WEATHERSEAL UNBOND
471-04	00	FWD SEG	FWD CYL/CYL FACT JNT	N/A	210	WEATHERSEAL UNBOND
486-08	00	FWD SEG	igniter/case jnt	N/A	360	FORWARD DOME AFTER IGNITER REMOVAL
507-01		FWD SEG	N/A	FWD DOME	090	IGNITER BOOT REMOVED FROM FORWARD DOME
507-02	. 00	FWD SEG	N/A	FWD DOME	90-180	IGNITER BOOT REMOVED FROM FORWARD DOME
507-03	00	FWD SEG	N/A	FWD DOME	180-270	IGNITER BOOT REMOVED FROM FORWARD DOME
507-04	00	FWD SEG	N/A	FWD DOME	270-0	IGNITER BOOT REMOVED FROM FORWARD DOME
507-0	5 00	FWD SEG	N/A	FWD DOME	360	IGNITER BOOT REMOVED FROM FORWARD DOME
496-0	3 00	FWD SEG	N/A	N/A	360	IGNITER BOOT INSULATION
GNITE	R					
486-0	1 00	igniter	N/A	N/A	0	IGNITER
486-0	2 00	igniter	N/A	N/A	180	IGNITER
1486-0	3 00	IGNITER	N/A	N/A	90	IGNITER
1486-0	4 00	IGNITER	N/A	N/A	270	igniter
1486-0		igniter	N/A	N/A	360	IGNITER
1488-0		igniter	N/A	N/A	340	IGNITER CHAMBER FORWARD SURFACE BLOWHOLE
					, •	

# PHOTOGRAPHS SORTED BY: SEGMENT, PHOTO CODE, JOINT, SEGMENT END, NEGATIVE # FOR RSRM-7B

3 BER	PHOTO	SEGMENT	JOINT	Segment End	DEG LOC	COMMENT
8-02	00	IGNITER	N/A	N/A	340	IGNITER ADAPTER FORWARD SURFACE BLOWHOLE
8-03	00	IGNITER	N/A	N/A	340	IGNITER ADAPTER FORWARD SURFACE BLOWHOLE
8-04	00	IGNITER	N/A	N/A	0	IGNITER CHAMBER FORWARD SEAL SURFACE
8-05	00	IGNITER	N/A	N/A	360	IGNITER ADAPTER

END OF REPORT\*\*\*

Я

ORIGINAL PAGE IS OF POOR QUALITY

•		